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LS

3-phase TEFV cage induction motors Aluminium alloy frame - 0.09 to 200 kW

Technical catalogue

3-phase TEFV induction motors LS aluminium alloy frame 0.09 to 200 kW

The LEROY-SOMER range of 3-phase motors



Other LEROY-SOMER motor ranges



Single phase induction motor



D.C. motor (drip-proof or enclosed)



Cast iron motor



VARMECA variable speed motor



3-phase autosynchronous motor

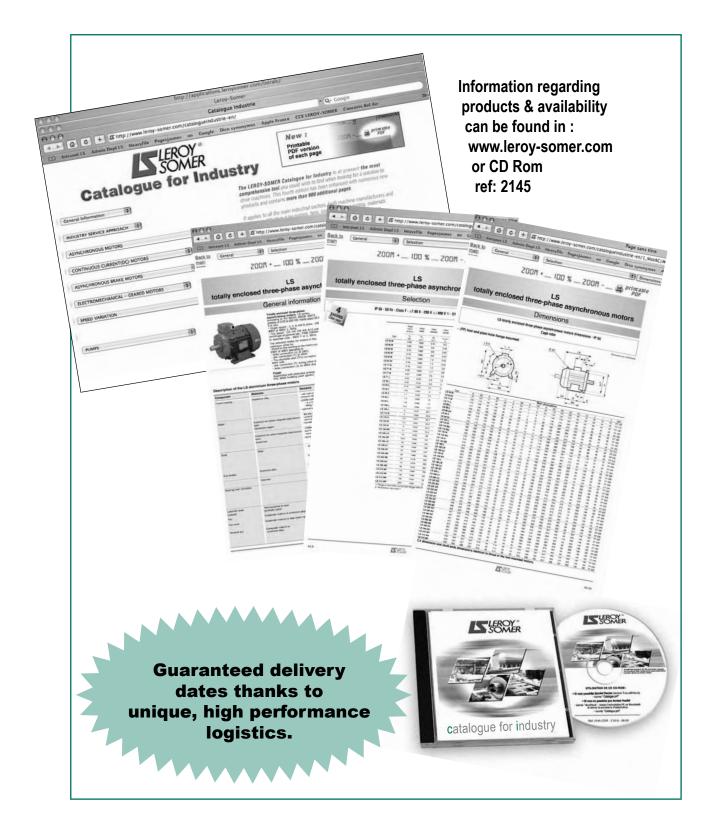


Motor for variable speed drive systems



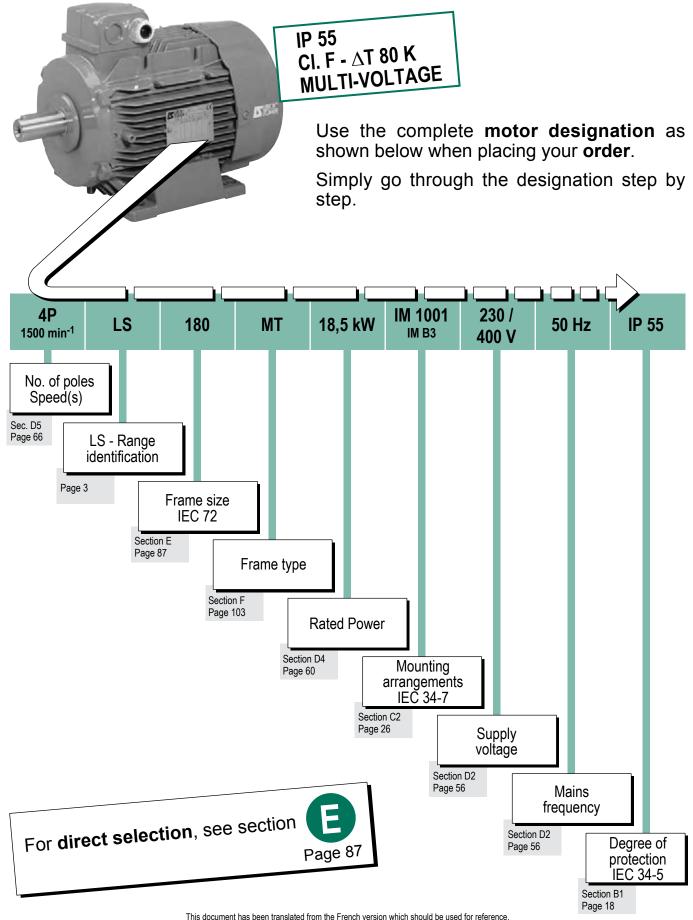
CATALOGUE FOR INDUSTRY

LEROY-SOMER offer their clients the opportunity to fix their own delivery dates, without prior consultation.





3-phase TEFV induction motors LS aluminium alloy frame 0.09 to 200 kW

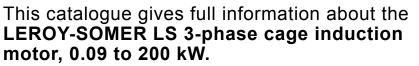


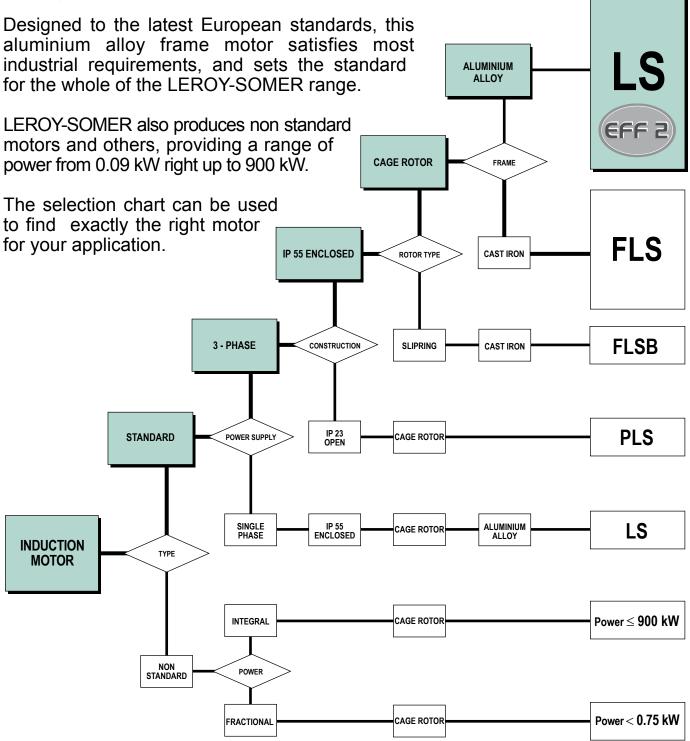
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The descriptions cannot in any way be considered contractual.



3-phase TEFV induction motors LS aluminium alloy frame 0.09 to 200 kW







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A1 - Quality commitment

LEROY-SOMER's quality management system is based on :

- control of procedures right from the initial sales offering until delivery to the customer, including design, manufacturing start-up and production.

- a total quality policy based on making continuous progress in improving operational procedures, involving all departments in the company in order to give customer satisfaction as regards delivery times, conformity and cost. - indicators used to monitor procedure performance.

- corrective actions and advancements with tools such as FMECA, QFD, MAVP, MSP/MSQ and Hoshin type improvement workshops on flows, process re-engineering, plus Lean Manufacturing and Lean Office.

- annual surveys, opinion polls and regular visits to customers in order to ascertain and detect their expectations.

Personnel are trained and take part in the analyses and the actions for continuously improving the procedures.

LEROY-SOMER has entrusted the certification of its expertise to various international organisations.

Certification is granted by independent professional auditors, and recognises the high standards of the **company's quality assurance procedures**. All activities resulting in the final version of the machine have therefore received official **ISO 9001: 2000 certification from the DNV**. Similarly, our environmental approach has enabled us to obtain ISO 14001: 2004 certification.

Products for particular applications or those designed to operate in specific environments are also approved or certified by the following organisations: CETIM, LCIE, DNV, INERIS, EFECTIS, UL, BSRIA, TUV, CCC, GOST, which check their technical performance against the various standards or recommendations.



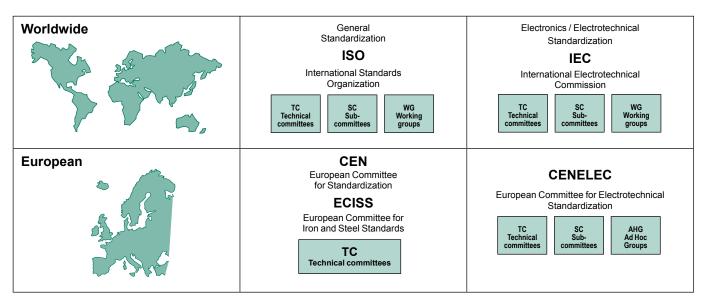
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A2 - Standards and approvals

ORGANIZATION OF STANDARDS AUTHORITIES

International bodies



Country	Initials	Designation
AUSTRALIA	SAA	Standards Association of Australia
BELGIUM	IBN	Institut Belge de Normalisation
CIS (ex-USSR)	GOST	Gosudarstvenne Komitet Standartov
DENMARK	DS	Dansk Standardisieringsraad
FINLAND	SFS	Suomen Standardisoimisliitto
FRANCE	AFNOR including UTE	Association Française de Normalisation including: Union Technique de l'Électricité
GERMANY	DIN/VDE	Verband Deutscher Elektrotechniker
GREAT BRITAIN	BSI	British Standards Institution
ITALY	IEC	Comitato Electtrotechnico Italiano
JAPAN	JIS	Japanese Industrial Standard
NETHERLANDS	NNI	Nederlands Normalisatie - Instituut
NORWAY	NFS	Norges Standardisieringsforbund
SAUDI ARABIA	SASO	Saudi Arabian Standards Organization
SPAIN	UNE	Una Norma Española
SWEDEN	SIS	Standardisieringskommissionen I Sverige
SWITZERLAND	SEV or ASE	Schweizerischer Elektrotechnischer Verein
UNITED STATES	ANSI including NEMA	American National Standards Institute including: National Electrical Manufacturers



A2 - Standards and approvals

Approvals

Certain countries recommend or insist on approval from national organizations.

Approved products must carry the recognized mark on their identification plates.

Country	Initials	Organization
USA	UL	Underwriters Laboratories
CANADA	CSA	Canadian Standards Association
etc.		

Approvals for LEROY-SOMER motors (versions derived from standard construction):

Country	Initials	Certification No.	Application
CANADA	CSA	LR 57 008	Standard adapted range (see section D2.2.3)
USA	UL or 위	E 68554 SA 6704 E 206450	Impregnation systems Stator/rotor assemblies for sealed units Complete motors up to 160 frame size
SAUDIARABIA	SASO		Standard range
FRANCE	LCIE INERIS	Various nos.	Sealing, shocks, safety

For specific approved products, see the relevant documents.

International and national standard equivalents

	International reference standards	National standards				
IEC	Title (summary)	FRANCE	GERMANY	U.K.	ITALY	SWITZERLAND
60034-1	Ratings and operating characteristics	NFEN 60034-1 NFC 51-120 NFC 51-200	DIN/VDE O530	BS 4999	CEI 2.3.VI.	SEV ASE 3009
60034-2	Determination of losses and efficiency	NFEN 60034-2	DIN/EN 60034-2	BS 4999-102		
60034-5	Classification of degrees of protection	NFEN 60034-5	DIN/EN 60034-5	BS EN 60034-5	UNEL B 1781	
60034-6	Cooling methods	NFEN 60034-6	DIN/EN 60034-6	BS EN 60034-6		
60034-7	Mounting arrangements and assembly layouts	NFEN 60034-7	NFEN 60034-7 DIN/EN 60034-7			
60034-8	Terminal markings and direction of rotation	NFC 51 118	DIN/VDE 0530 Teil 8	BS 4999-108		
60034-9	Noise limits	NFEN 60034-9	DIN/EN 60034-9	BS EN 60034-9		
60034-12	Starting characteristics for single-speed motors powered from the mains ≤ 660 V	NFEN 60034-12	0034-12 DIN/EN 60034-12 BS EN 60034-12			SEV ASE 3009-12
60034-14	Mechanical vibration in machines of frame size $>$ 56 mm	NFEN 60034-14	DIN/EN 60034-14	BS EN 60034-14		
60072-1	Dimensions and output powers for machines of between 56 and 400 frame and flanges of between 55 and 1080	NFC 51 104 NFC 51 105	DIN 748 (~) DIN 42672 DIN 42673 BS 4999 DIN 42631 DIN 42676 DIN 42677			
60085	Evaluation and thermal classification of electrical insulation	NFC 26206	DIN/EN 60085	BS 2757		SEV ASE 3584

Note: DIN 748 tolerances do not conform to IEC 60072-1.



A2 - Standards and approvals

A

List of standards quoted in this document

LS motors comply with the standards quoted in this catalogue

Reference		Date	International standards			
IEC 60034-1	EN 60034-1	1999	Electrical rotating machines: ratings and operating characteristics			
IEC 60034-5	EN 60034-5	2000	Electrical rotating machines: classification of degrees of protection provided by casings of rotating machines.			
IEC 60034-6	EN 60034-6	1993	Electrical rotating machines (except traction): cooling methods			
IEC 60034-7	EN 60034-7	2000	Electrical rotating machines (except traction): symbols for mounting positions and assembly layouts			
IEC 60034-8		2001	Electrical rotating machines: terminal markings and direction of rotation			
IEC 60034-9	EN 60034-9	1997	Electrical rotating machines: noise limits			
IEC 60034-12	EN 60034-12	1999	Starting characteristics for single-speed 3-phase cage induction motors for supply voltages less than or equal to 660V.			
IEC 60034-14	EN 60034-14	2004	Electrical rotating machines: mechanical vibrations of certain machines with a frame size above or equal to 56 mm. Measurement, evaluation and limits of vibrational intensity.			
IEC 60038		1999	IEC standard voltages			
IEC 60072-1		1991	Dimensions and power series for electrical rotating machines: designation of casings between 56 and 400 and flanges between 55 and 1080.			
IEC 60085		1984	Evaluation and thermal classification of electrical insulation.			
IEC 60721-2-1		1987	Classification of natural environment conditions. Temperature and humidity.			
IEC 60892		1987	Effects of an imbalance in the voltage system on the characteristics of three-phase squirrel-cage induction motors.			
IEC 61000-2-10/11 and		1999	Electromagnetic compatibility (EMC): environment			
IEC guide 106		1989	Guidelines on the specification of environmental conditions for the determination of operating characteristics of equipment.			
ISO 281		2000	Bearings - Basic dynamic loadings and nominal bearing life			
ISO 1680	EN 21680	1999	Acoustics - Test code for measuring airborne noise emitted by electrical rotating machines: a method for establishing an expert opinion for free field conditions over a reflective surface			
ISO 8821		1999	Mechanical vibration - Balancing. Conventions on shaft keys and related parts			
	EN 50102	1998	Degree of protection provided by the electrical housing against extreme mechanical impacts.			



A3 - Tolerance on main performance parameters

Tolerances for electromechanical characteristics

IEC 60034-1 specifies standard tolerances for electromechanical characteristics.

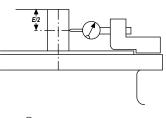
Parameters	Tolerances
Efficiency machines P ≤ 50 kW machines P > 50 kW	– 15% (1 – η) – 10% (1 – η)
Cos φ	– 1/6 (1 – cos φ) (min 0.02 - max 0.07)
Slip $machines P < 1 kW$ machines P $\ge 1 kW$	± 30% ± 20%
Locked rotor torque	- 15%, + 25% of rated torque
Starting current	+ 20%
Run-up torque	- 15% of rated torque
Breakdown torque	- 10% of rated torque > 1.5 $M_{_{\rm N}}$
Moment of inertia	± 10%
Noise	+ 3 dB (A)
Vibration	+ 10% of the guaranteed class

Note: IEC 60034-1 does not specify tolerances for current the tolerance is ± 10% in NEMA-MG1

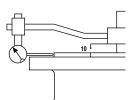
Tolerances and adjustments

The standard tolerances shown below are applicable to the drawing dimensions given in our catalogues. They comply fully with the requirements of IEC standard 60072-1.

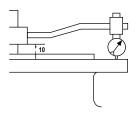
Characteristics	Tolerances
Frame size H ≤ 250 ≥ 280	0, — 0.5 mm 0, — 1 mm
Diameter \varnothing of shaft extension:	
- 11 to 28 mm	j6
- 32 to 48 mm	k6
- 55 mm and over	m6
Diameter N of flange spigot	j6 up to FF 500, js6 for FF 600 and over
Key width	h9
Width of drive shaft keyway (normal keying)	N9
Key depth	
- square section	h9
- rectangular section	h11
① Eccentricity of shaft in flanged motors	
(standard class)	
- diameter > 10 up to 18 mm	0.035 mm
- diameter > 18 up to 30 mm	0.040 mm 0.050 mm
- diameter > 30 up to 50 mm - diameter > 50 up to 80 mm	0.050 mm
- diameter > 80 up to 120 mm	0.070 mm
	0.070 mm
Concentricity of spigot diameter and perpendicularity of mating surface of flange in relation to shaft (standard class) Flange (FF) or Faceplate (FT):	
- F 55 to F 115	0.08 mm
- F 130 to F 265	0.10 mm
- FF 300 to FF 500	0.125 mm
- FF 600 to FF 740	0.16 mm
- FF 940 to FF 1080	0.20 mm



① Eccentricity of shaft in flanged motors



Concentricity of spigot diameter



③ Perpendicularity of mating surface of flange in relation to shaft



A4 - Units of measurement and standard formulae

A4.1 - ELECTRICITY AND ELECTROMAGNETISM

Parameters				Unit		Units and expressions not recommended
Name	French name	Symbol	Definition	SI	Non SI, but accepted	Conversion
Frequency Period	Fréquence	f	$f = \frac{1}{T}$	Hz (hertz)		
Electric current	Courant électrique (intensité de)	1		A (ampere)		
Electric potential Voltage Electromotive force	Potentiel électrique Tension Force électromotrice	V U E		V (volt)		
Phase angle	Déphasage	φ	$U = Um \cos \omega t$ $i = im \cos (\omega t - \varphi)$	rad	° degree	
Power factor	Facteur de puissance	cos φ				
Reactance Resistance	Réactance Résistance	X R	$Z = Z ^{\psi\varphi}$ $= R + jX$ $ Z = \sqrt{R^2 + x^2}$	Ω (ohm)		<i>j</i> is defined as $j^2 = -1$ ω pulsation = 2 π . <i>f</i>
Impedance	Impédance	Ζ	$X = L\omega - \frac{1}{C\omega}$			
Self inductance	Inductance propre (self)	L	$L = \frac{\Phi}{I}$	H (henry)		
Capacitance	Capacité	С	$C = \frac{Q}{V}$	F (farad)		
Quantity of electricity	Charge électrique, Quantité d'électricité	Q	Q = ∫Idt	C (coulomb)	A.h 1 A.h = 3600 C	
Resistivity	Résistivité	ρ	$\rho = \frac{R.S}{I}$	Ω.m		Ω/m
Conductance	Conductance	G	$G = \frac{1}{R}$	S (siemens)		1/Ω=1S
Number of turns (coil) Number of phases Number of pairs of poles	Nombre de tours (spires) de l'enroulement Nombre de phases Nombre de paires de pôles	N m p				
Magnetic field	Champ magnétique	Н		A/m		
Magnetic potential difference Magnetomotive force	Différence de potentiel magnétique Force magnétomotrice Solénation, courant totalisé	Um F, Fm H	$F = \Phi H_s d_s$ H = NI	A		The unit AT (ampere-turns) is incorrect because it treats "turn" as a physical unit
Magnetic induction, Magnetic flux density	Induction magnétique, Densité de flux magnétique	В		T (tesla) = Wb/m ²		(gauss) 1 G = 10⊣ T
Magnetic flux	Flux magnétique, Flux d'induction magnétique	Φ	$\Phi = ff_s Bn ds$	Wb (weber)		(maxwell) 1 max = 10⊸ Wb
Magnetic vector potential	Potentiel vecteur magnétique	A		Wb/m		
Permeability Permeability of vacuum	Perméabilité du milieu Perméabilité du vide	μ = μ _° μ _′	$B = \mu H$ $\mu_{o} = 4\pi 10^{-7} H/m$	H/m		
Permittivity	Permittivité	$\varepsilon = \varepsilon_o \varepsilon_r$	$\varepsilon_o = \frac{1}{36 \pi 10^9} \mathrm{F/m}$	F/m		



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A4 - Units of measurement and standard formulae

A4.2 - THERMODYNAMICS

Parameters	Parameters					Units and expressions not recommended
French name	English name	Symbol	Definition	SI	Non SI, but accepted	Conversion
Temperature Thermodynamic	Température Thermodynamique	Τ		K (kelvin)	temperature Celsius, t, °C T = t + 273.15	°C: Degree Celsius t_{c} : temp. in °C t_{F} : temp. in °F f temperature Fahrenheit °F $t = \frac{f-32}{1,8}$ $t_{C} = \frac{t_{F}-32}{1,8}$
Temperature rise	Ecart de température	ΔT		К	°C.	1 °C = 1 K
Thermal flux density	Densité de flux thermique	q , φ	$q = \frac{\Phi}{A}$	W/m ²		
Thermal conductivity	Conductivité thermique	λ		W/m.K		
Total heat transmission coefficient total heat	Coefficient de transmission thermique globale coefficient	к	$\varphi = K \left(Tr_2 - Tr_1 \right)$	W/m².K		
Thermal capacity	Capacité thermique	С	$C = \frac{dQ}{dT}$	J/K		
Specific thermal capacity	Capacité thermique massique	с	$c = \frac{C}{m}$	J/kg.K		
Internal energy	Energie interne	U		J		

A4.3 - NOISE AND VIBRATION

Parameters				Unit		Units and expressions not recommended
Name	French name	Symbol	Definition	SI	Non SI, but accepted	Conversion
Sound power level	Niveau de puissance acoustique	L _w	$L_{w} = 10 \log(P/P_{o})$ $(P_{o} = 10^{-12} W)$	dB (decibel)		Ig logarithm to base 10 Ig10 = 1
Sound pressure level	Niveau de pression acoustique	L _P	$L_{p} = 20 \text{lg}(P/P_{o})$ $(P_{o} = 2x10^{\circ} Pa)$	dB		

A4.4 - DIMENSIONS

Parameters	Parameters			Unit		Units and expressions not recommended
Name	French name	Symbol	Definition	SI	Non SI, but accepted	Conversion
Angle (plane angle)	Angle (angle plan)	α, β, <i>Τ</i> , φ		rad	degree: ° minute: ' second: "	$180^{\circ} = \pi \text{ rad}$ = 3.14 rad
Length Width Height Radius	Longeur Largeur Hauteur Rayon Longueur curviligne	l b r s		m (metres)	micrometre	cm, dm, dam, hm 1 inch = 1" = 25.4 mm 1 foot = 1' = 304.8 mm μ m micron μ angström: A = 0.10 nm
Area Volume	Aire, superficie Volume	A, S V		m ²	litre: I liter: L	1 square inch = 6.45 10-4 m ² UK gallon = 4.546 10-3 m ³ US gallon = 3.785 10-3 m ³



A4 - Units of measurement and standard formulae

A4.5 - MECHANICS AND MOVEMENT

Parameters				Unit		Units and expressions not recommended	
Name	French name	Symbol	Definition	SI	Non SI, but accepted	Conversion	
Time Period (duration of cycle)	Temps Intervalle de temps, durée Période (durée d'un cycle)	t T		s (second)	minute: min hour: h day: d	Symbols ' and " are reserved for angles minute not written as mn	
Angular velocity Rotational frequency	Vitesse angulaire Pulsation	ω	$\omega = \frac{d\varphi}{dt}$	rad/s			
Angular acceleration	Accélération angulaire	α	$\alpha = \frac{d\omega}{dt}$	rad/s ²			
Speed Velocity	Vitesse Célérité	u, v, w, c	$v = \frac{ds}{dt}$	m/s	1 km/h = 0.277 778 m/s 1 m/min =		
Acceleration	Accélération	а	$a = \frac{dv}{dt}$	m/s²	0.016 6 m/s		
Acceleration of free fall	Accélération de la pesanteur	g=9.81m/s ^e	in Paris				
Speed of rotation	Vitesse de rotation	N		S -1	min₁	tr/mn, RPM, TM	
Weight	Masse	т		kg (kilogram)	tonne: t 1 t = 1000 kg	kilo, kgs, KG 1 pound: 1 lb = 0.4536 kg	
Mass density	Masse volumique	ρ	dm dV	kg/m₃			
Linear density	Masse linéique	ρ _e	dm dL	kg/m			
Surface density	Masse surfacique	ρ _Α	dm dS	kg/m²			
Momentum	Quantité de mouvement	Р	<i>p</i> = <i>m</i> . <i>v</i>	kg. m/s		-	
Moment of inertia	Moment d'inertie	J, I	<i>I</i> = ∑m.r ²	kg.m²		$J = \frac{MD^2}{4}$ kg.m pound per square foot = 1 lb.ft ² = 42.1 x 10 ⁻³ kg.m ²	
Force Weight	Force Poids	F G	G = m.g	N (newton)		kgf = kgp = 9.81 N pound force = IbF = 4.448 N	
Moment of force Torque	Moment d'une force	M T	M = F.r	N.m		mdaN, mkg, m.N 1 mkg = 9.81 N.m 1 ft.lbF = 1.356 N.m 1 in.lbF = 0.113 N.m	
Pressure	Pression	p	$p = \frac{F}{S} = \frac{F}{A}$	Pa (pascal)	bar 1 bar = 10⊧Pa	1 kgf/cm ² = 0.981 bar 1 psi = 6894 N/m ² = 6894 Pa 1 psi = 0.06894 bar 1 atm = 1.013 x 10 ^s Pa	
Normal stress Shear stress,	Contrainte normale Contrainte tangentielle Cission	σ τ		Pa Leroy-Somer usetheMPa=10 [;] Pa		kg/mm², 1 daN/mm² = 10 MPa psi = pound per square inch 1 psi = 6894 Pa	
Friction coefficient	Facteur de frottement	μ				incorrectly = friction cœfficient f	
Work Energy Potential energy Kinetic energy Quantity of heat	Travail Énergie Énergie potentielle Énergie cinétique Quantité de chaleur	W E Ep Ek Q	W = F.I	J (joule)	Wh = 3600 J (watt-hour)	1 N.m = 1 W.s = 1 J 1 kgm = 9.81 J (calorie) 1 cal = 4.18 J 1 Btu = 1055 J (British thermal unit)	
Power	Puissance	P	$P = \frac{W}{t}$	W (watt)		1 ch = 736 W 1 HP = 746 W	
Volumetric flow	Débit volumique	qv	$q_{\rm V} = \frac{dV}{dt}$	m³/s			
Efficiency	Rendement	η		<1		%	
Dynamic viscosity	Viscosité dynamique	η, μ		Pa.s		poise, 1 P = 0.1 Pa.s	
Kinematic viscosity	Viscosité cinématique	ν	$v = \frac{\eta}{\rho}$	m²/s		stokes, 1 St = 10-4 m²/s	



A5 - Unit conversions

Unit	MKSA (IS international system)	AGMA (US system)	
Length	1 m = 3.2808 ft 1 mm = 0.03937 in	1 ft = 0.3048 m 1 in = 25.4 mm	
Weight	1 kg = 2.2046 lb	1 lb = 0.4536 kg	
Torque	1 Nm = 0.7376 lb.ft 1 N.m = 141.6 oz.in	1 lb.ft = 1.356 N.m 1 oz.in = 0.00706 N.m	
Force	1 N = 0.2248 lb	1 lb = 4.448 N	
Moment of inertia	1 kg.m² = 23.73 lb.ft²	1 lb.ft² = 0.04214 kg.m²	
Power	1 kW = 1.341 HP	1 HP = 0.746 kW	
Pressure	1 kPa = 0.14505 psi	1 psi = 6.894 kPa	
Magnetic flux	1 T = 1 Wb / m ² = 6.452 10 ⁴ line / in ²	1 line / in² = 1.550 10-5 Wb / m²	
Magnetic losses	1 W / kg = 0.4536 W / lb	1 W / Ib = 2.204 W / kg	

Multip	les and sub-multiples	
Factor by which the unit is multiplied	Prefix to be placed before the unit name	Symbol to be placed before that of the unit
10 ¹⁸ or 1,000,000,000,000,000,000	exa	Е
10 ¹⁵ or 1,000,000,000,000,000	peta	Р
10 ¹² or 1,000,000,000,000	tera	Т
10° or 1,000,000,000	giga	G
10 ⁶ or 1,000,000	mega	М
10 ³ or 1,000	kilo	k
10 ² or 100	hecto	h
10 ¹ or 10	deca	da
10 ⁻¹ or 0.1	deci	d
10 ⁻² or 0.01	centi	с
10 ⁻³ or 0.001	milli	m
10 ⁻⁶ or 0.000,001	micro	μ
10 ^{.9} or 0.000,000,001	nano	n
10 ⁻¹² or 0.000,000,000,001	pico	p
10 ⁻¹⁵ or 0.000,000,000,000,001	femto	f
10 ⁻¹⁸ or 0.000,000,000,000,000,001	atto	а



Δ

A6 - Standard formulae used in electrical engineering

A6.1 - MECHANICAL FORMULAE

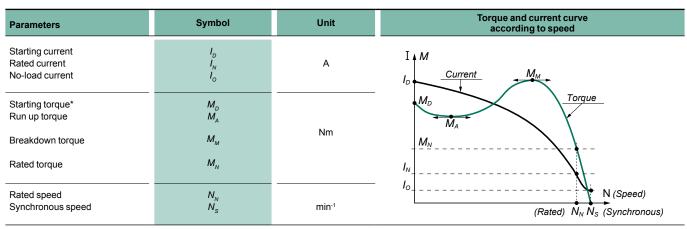
Title	Formula	Unit	Definitions / notes
Force	$F = m \cdot \gamma$	<i>F</i> in N <i>m</i> in kg γ in m/s²	A force <i>F</i> is the product of a mass <i>m</i> by an acceleration γ
Weight	$G = m \cdot g$	G in N <i>m</i> in kg g = 9.81 m/s²	
Moment	M = F · r	<i>M</i> in N.m <i>F</i> in N <i>r</i> in m	The moment M of a force in relation to an axis is the product of that force multiplied by the distance r of the point of application of F in relation to the axis.
Power - Rotation	$P = M \cdot \omega$	P in W M in N.m ω in rad/s	Power <i>P</i> is the quantity of work yielded per unit of time $\omega = 2\pi N/60$ where <i>N</i> is the speed of rotation in min ⁻¹
- Linear	P = F . V	P in W F in N V in m/s	V = linear velocity
Acceleration time	$t = J \cdot \frac{\omega}{M_{\rm a}}$	t in s J in kg.m ² ω in rad/s M_a in Nm	<i>J</i> is the moment of inertia of the system M_a is the moment of acceleration Note: all the calculations refer to a single rotational speed ω where the inertias at speed ω are corrected to speed ω by the following calculation:
			$J_{\omega} = J_{\omega'} \cdot \left(\frac{\omega}{\omega}\right)^2$
Moment of inertia Centre of gravity	$J = m . r^2$		
Solid cylinder around its shaft	$J = m \cdot \frac{r^2}{2}$ $J = m \cdot \frac{r_1^2 + r_2^2}{2}$	J in kg.m² <i>m</i> in kg <i>r</i> in m	
Hollow cylinder around its shaft			т
Inertia of a mass in linear motion	$J = m \cdot \left(\frac{v}{\omega}\right)^2$	J in kg.m ² m in kg v in m/s ω in rad/s	The moment of inertia of a mass in linear motion transformed to a rotating motion.



A6 - Standard formulae used in electrical engineering

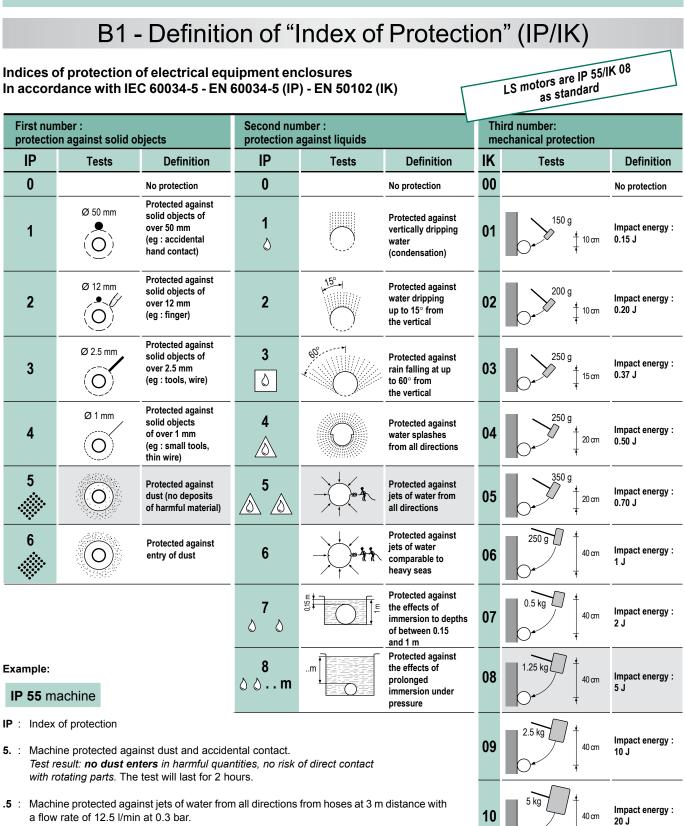
A6.2 - ELECTRICAL FORMULAE

Title	Formula	Unit	Definitions / notes
Accelerating torque	$M_{a} = \frac{M_{D} + 2M_{A} + 2M_{M} + M_{N}}{6} - M_{r}$ General formula: $M_{a} = \frac{1}{N_{N}} \int_{0}^{N_{N}} (M_{mot} - M_{r}) dN$	Nm	Moment of acceleration M_A is the difference between the motor torque M_{mot} (estimated), and the resistive torque M_r . $(M_D, M_A, M_M, M_N$, see curve below) N = instantaneous speed N_N = rated speed
Power required by machine	$P = \frac{M \cdot \omega}{\eta_{A}}$	P in W M in N.m ω in rad/s η _A no unit	$\eta_{\rm A}$ expresses the efficiency of the driven machine. M is the torque required by the driven machine.
Power drawn by the 3-phase motor	$P = \sqrt{3} \cdot U \cdot I \cdot \cos \varphi$	P in W U in V I in A	φ phase angle by which the current lags or leads the voltage. <i>U</i> phase to phase voltage. <i>I</i> line current.
Reactive power absorbed by the motor	$Q = \sqrt{3} \cdot U \cdot I \cdot \sin \varphi$	Q in VAR	
Reactive power supplied by a bank of capacitors	$\mathbf{Q} = \sqrt{3} \cdot \boldsymbol{U}^2 \cdot \boldsymbol{C} \cdot \boldsymbol{\omega}$	U in V C in μ F ω in rad/s	U = voltage at the capacitor terminals C = capacitor capacitance ω = rotational frequency of supply phases (ω = 2 π f)
Apparent power	$S = \sqrt{3} \cdot U \cdot I$ $S = \sqrt{P^2 + Q^2}$	S in VA	
Power supplied by 3-phase motor	$P = \sqrt{3} \cdot U \cdot I \cdot \cos \varphi \cdot \eta$		$\boldsymbol{\eta}$ expresses motor efficiency at the point of operation under consideration.
Slip	$g = \frac{N_{\rm S} - N}{N_{\rm S}}$		Slip is the difference between the actual motor speed N and the synchronous speed N_s
Synchronous speed	$N_{\rm S} = \frac{120.f}{p}$	N _s in min ⁻¹ f in Hz	<i>p</i> = number of poles <i>f</i> = frequency of the power supply



* Torque is the usual term for expressing the moment of a force.





The test will last for 3 minutes.

Test result: no damage from water projected onto the machine.

LEROY* SOMER

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B2 - Environmental limitations

B2.1 - NORMAL OPERATING CONDITIONS

a / According to IEC 60034-1, motors can operate in the following normal conditions:
ambient temperature within the range - 16 and + 40 °C

• altitude less than 1000 m

• atmospheric pressure: 1050 hPa (mbar) = (750 mm Hg)

b / Power correction factor:

For operating conditions outside these limits, apply the power correction coefficient shown in the chart on the right *which maintains the thermal reserve*, as a function of the altitude and ambient temperature.

B2.2 - NORMAL STORAGE CONDITIONS

Machines should be stored at an ambient temperature between -16 and + 40 $^{\circ}$ C and a relative humidity of less than 90%.

For restarting, see commissioning manual.

B2.3 - RELATIVE AND ABSOL-UTE HUMIDITY

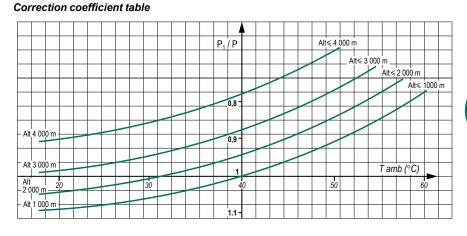
Measuring the humidity:

Humidity is usually measured by the "wet and dry bulb thermometer" method.

Absolute humidity, calculated from the readings taken on the two thermometers, can be determined using the chart on the right. The chart also provides relative humidity figures.

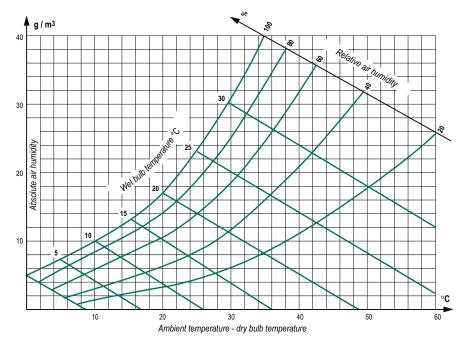
To determine the humidity correctly, a good air flow is required for stable readings, and accurate readings must be taken on the thermometers.

During the construction of aluminium motors, the materials of the various components which are in contact with one another are selected so as to minimise deterioration by galvanic effect. The voltages in the metal combinations used (cast iron-steel; cast ironaluminium; steel-aluminium; steel-tin) are too low to cause deterioration.



Note: the output power can only be corrected upwards once the ability of the motor to start the load has been checked.

In temperate climates, relative humidity is generally between 50 and 70%. For the relationship between relative humidity and motor impregnation, especially where humidity and temperature are high, see table on next page.



B2.4 - DRAIN HOLES

Holes are provided at the lowest points of the enclosure, depending on the operating position (IM etc) to drain off any moisture that may have accumulated inside during cooling of the machine.

The holes may be sealed in various ways: - standard: with plastic plugs,

- on request: with screws, siphon or plastic ventilator.

Under certain special conditions, it is advisable to leave the drain holes permanently open (operating in environments with high levels of condensation).

Opening the holes periodically should be part of the regular maintenance procedure.

B2.5 - DRIP COVERS

For machines operating outdoors, with the drive shaft downwards, drip covers are recommended.

This is an option and should be specified on the order if required.

The dimensions are given in the dimensions tables. (Page 111, section G2).



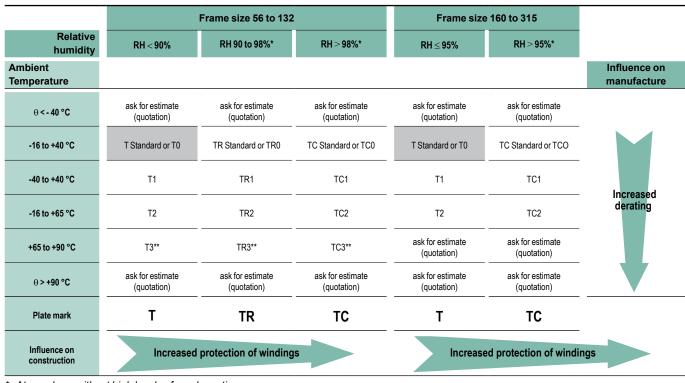
B3 - Impregnation and enhanced protection

B3.1 - NORMAL ATMOSPHERIC PRESSURE (750 mm Hg)

The selection table below can be used to find the method of manufacture best suited to particular environments in which temperature and relative humidity show large degrees of variation (see relative and absolute humidity calculation method, on preceding page). The symbols used refer to permutations of components, materials, impregnation methods and finishes (varnish or paint).

The protection of the winding is generally described by the term «tropicalization».

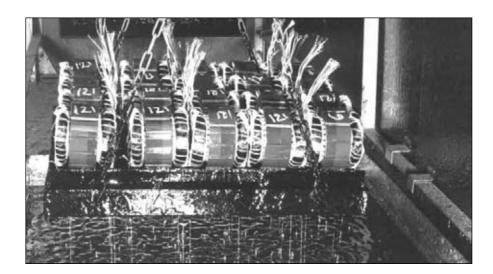
For high humidity environments, we recommend that the windings are pre-heated (see section B4.1).



* Atmosphere without high levels of condensation

** Bearing life calculated for 5000 running hours (section C3, page 28). For longer times, please consult Leroy Somer. For motors of frame size 56 to 71: T3/TR3/TC3 ask for quotation.

Standard manufacture



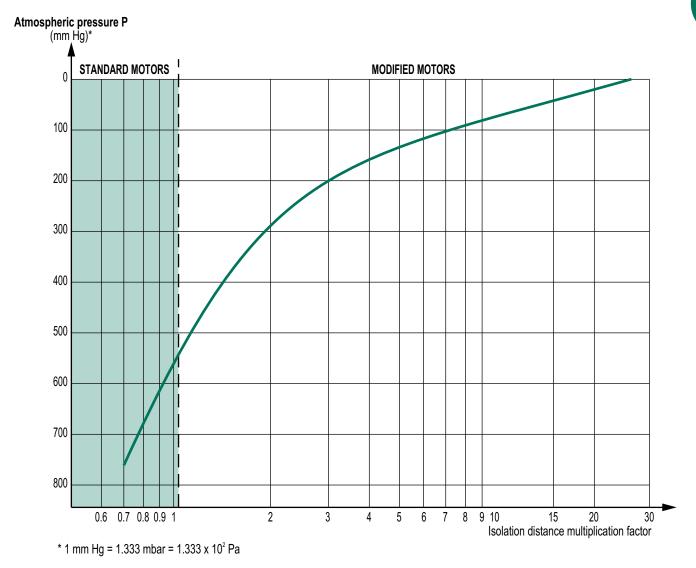


B3 - Impregnation and enhanced protection

B3.2 - INFLUENCE OF ATMOSPHERIC PRESSURE

As atmospheric pressure decreases, air particles rarefy and the environment becomes increasingly conductive.

The curve below shows the increase in isolation distance required, according to atmospheric pressure.



Solutions for permanent applications: offers based on specification

- P > 550 mm Hg: Standard impregnation according to previous table - Possible derating or forced ventilation.

- P > 200 mm Hg: Coating of bearings - Flying leads up to a zone at P ~ 750 mm Hg - Derating to take account of insufficient ventilation - Forced ventilation.

- P < 200 mm Hg: Special manufacture based on specification.

In all cases, these problems should be resolved by a special contract worked out on the basis of a specification.



B4 - Heaters

B4.1 - SPACE HEATERS

Severe climatic conditions, e.g. *T* amb < - 40° C, RH > 95% etc, may require the use of space heaters (fitted to the motor windings) which serve to maintain the average temperature of the motor, provide trouble-free starting, and eliminate problems caused by condensation (loss of insulation).

The heater supply wires are brought out to a terminal block in the motor terminal box. The heaters must be switched off while the motor is running.

Motor type	No. of poles	Power: P(W)
LS 80	2 - 4 - 6 - 8	10
LS 90 to LS 132	2 - 4 - 6 - 8	25
LS 160 MP - LR LS 160 M - L	2 - 4 2 - 6 - 8	25 50
LS 180 to LS 225	2 - 4 - 6 - 8	50
LS 250	2 4 - 6 - 8	50 80
LS 280 to LS 315	2 4 - 6 - 8	80 100

The space heaters use 200/240V, single-phase, 50 or 60 Hz.

B4.2 - D.C. INJECTION

An alternative to the use of space heaters is to inject direct current into two of the phases wired in series from a D.C. voltage source which can give the total power indicated in the table above. This method can only be used on motors of less than 10 kW.

This is easily calculated: if R is the resistance of the windings in series, the D.C. voltage will be given by the equation (Ohm's law):

$$\mathsf{U}_{(\mathsf{V})} = \sqrt{\mathsf{P}_{(\mathsf{W})} \cdot \mathsf{R}_{(\Omega)}}$$

Resistance should be measured with a micro-ohmmeter.



B4.3 - A.C. INJECTION

A single-phase A.C. voltage (from 10 to 15% of rated voltage), can be used between 2 phases placed in series.

This method can be used on the whole LS range.





B5 - External finish

LEROY-SOMER motors are protected with a range of surface finishes. The surfaces receive appropriate special treatments, as shown below.



Preparation of surfaces

SURFACE	PARTS	TREATMENT	
Cast iron	End shields	Shot blasting + Primer	
Steel	Accessories	Phosphatization + Primer	
Steer	Terminal boxes - Fan covers	Electrostatic painting or Epoxy powder	
Aluminium alloy	Housing - Terminal boxes	Shot blasting	
Polymer	Fan covers - Terminal boxes Ventilation grilles	None, but must be free from grease, casting-mould coatings, and dust which would affect paint adhesion	

Definition of atmospheres

An atmosphere is said to be harsh when components are attacked by bases, acids or salts. It is said to be corrosive when components are attacked by oxygen.

Painting systems

PRODUCTS	ATMOSPHERE	SYSTEM	APPLICATIONS	RESISTANCE TO SALINE MIST ISO 9227 standard
	Clean, dry (indoors, rural or industrial)	Ia	1 coat polyurethane finish 20/30 μm	72 hours
	Moderately corrosive: humid, and outdoors (temperate climate)	Ha	1 base coat Epoxy 30/40 μm 1 coat polyurethane finish 20/30 μm	150 hours
LEROY-SOMER Motors	Corrosive: coastal, very humid (tropical climate)	IIIa	1 base coat Epoxy 30/40 μm 1 intermediate coat Epoxy 30/40 μm 1 coat polyurethane finish 20/30 μm	300 hours
	Significant level of chemical attack: frequent contact with bases, acids, alkalines environment - neutral atmosphere (not on contact with chlorinated or sulphurous products)	Шь	1 base coat Epoxy 30/40 μm 1 intermediate coat Epoxy 30/40 μm 1 coat Epoxy finish 25/35 μm	500 hours

System Ia is for moderate climates and System IIa is for general climates as defined in standard IEC 60721-2-1. Exposure to saline mist under the terms of ISO 9227 standard (5% of NaCl at 6 < PH < 7.5 at 35° and 1 bar).

LEROY-SOMER standard paint colour reference:

RAL 6000



B6 - Interference suppression

Airborne interference

Emission

For standard motors, the housing acts as an electromagnetic screening, reducing electromagnetic emissions measured at 0.25 metres from the motor to approximately 5 gauss (5 x 10^{-4} T).

However, electromagnetic emissions may be noticeably reduced by a special construction of aluminium alloy end shields and a stainless steel shaft.

Immunity

The construction of motor housings (especially the finned aluminium alloy frames) isolates external electromagnetic sources to the extent that any field penetrating the casing and magnetic circuit will be too weak to interfere with the operation of the motor.

Power supply interference

The use of electronic systems for starting, speed control or power supply can create harmonics on the supply lines which may interfere with the operation of machines. These phenomena are taken into account in determining the machine dimensions, which act as quenching chokes in this respect.

The IEC 61000 standard, currently in preparation, will define permissible rejection and immunity rates: only then will machines for general distribution (especially single-phase motors and commutator motors) have to be fitted with suppression systems.

Three-phase squirrel cage machines do not in themselves produce interference of this type. Mains connection equipment (contactors) may, however, need interference protection.

Application of Directive 89-336 modified by Directives 92-31 and 93-68 concerning electromagnetic compatibility (EMC).

a - for motors only

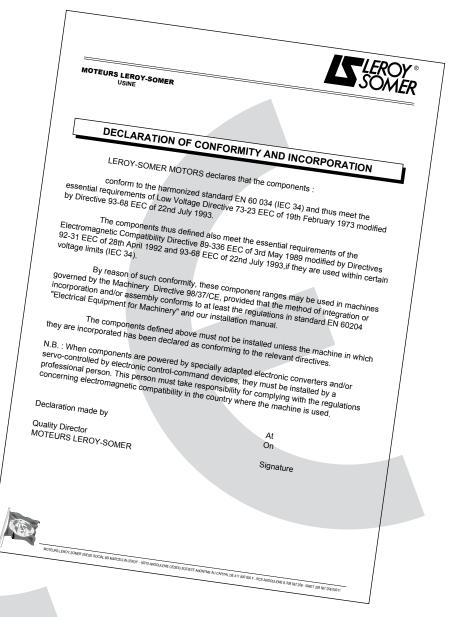
According to amendment 1 of IEC 60034-1, induction motors are not transmitters and do not produce interference (via carried or airborne signals) and therefore conform inherently to the essential requirements of the EMC directives.

b - for motors supplied by inverters (at fixed or variable frequency)

In this case, the motor is only a sub-assembly of a device which the system builder must ensure conforms to the essential requirements of the EMC directives.

Application of the Low Voltage Directive 73-23 EEC modified by Directive 93/68

All motors have been subject to this directive since 1 July 1997. The main requirements concern the protection of people, animals and property against risks caused by operation of the motors (see the commissioning and maintenance manual for precautions to be taken).



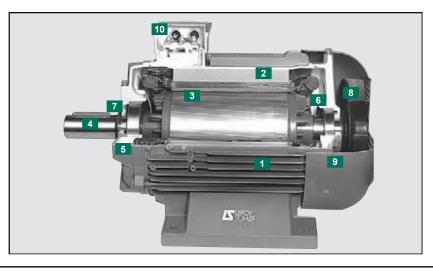
CE product marking

The fact that motors conform to the essential requirements of the Directives is shown by the **CC** mark on their nameplates and/or packaging and documentation.

C1 - Component parts

Description of standard LS 3-phase motors

Component	Materials	Remarks
1 Housing with cooling fins	Aluminium alloy	 with integral or screw-on feet, or without feet 4 or 6 fixing holes for housings with feet lifting rings for frame size ≥ 132 M, optional for 132 S and 112 earth terminal (optional)
2 Stator	Insulated low-carbon magnetic steel laminations Electroplated copper	 low carbon content guarantees long-term lamination pack stability welded packs semi-enclosed slots class F insulation
3 Rotor	Insulated low-carbon magnetic steel laminations Aluminium (A5L)	 - inclined cage bars - rotor cage pressure die-cast in aluminium (or alloy for special applications) - shrink-fitted to shaft - rotor balanced dynamically, 1/2 key
4 Shaft	Steel	 for frame size < 132: shaft end fitted with screw and washer closed keyway for frame size ≥ 132: tapped hole open keyway
5 End shields	Aluminium alloy	- LS 56 - 63 - 71 drive end and non drive end - LS 80 - 90 non drive end
	Cast iron	 LS 80 - 90 drive end (optional for LS 80 and 90 at non drive end) LS 100 to 315 drive end and non drive end
6 Bearings and lubrication		 ball bearings type 2RS 'greased for life' from LS 56 to LS 71 inclusive types ZZ 'greased for life' from LS 80 to LS 180 inclusive semi-protected or open type for frame size 200 open type, regreasable from 225 upwards bearings preloaded at non drive end
7 Labyrinth seal Lipseals	Plastic or steel Synthetic rubber	 lipseal or deflector at drive end for all flange mounted motors lipseal, deflector or labyrinth seal for foot mounted motors
8 Fan	Composite material or aluminium alloy	- 2 directions of rotation: straight blades
9 Fan cover	Composite material or pressed steel	 fitted, on request, with a drip cover for operation in vertical position, shaft end facing down.
10 Terminal box	Composite material or aluminium alloy	 IP 55 can be turned on, opposite side to feet fitted with a terminal block with 6 steel terminals as standard (brass as an option) terminal box supplied fitted with cable glands (without cable glands as an option) 1 earth terminal in each terminal box



C2 - Mounting arrangements

C2.1 - MOUNTING ARRANGEMENTS





IM 3001 (IM B5)



IM 3601 (IM B14)





The various mounting arrangements for machines are defined in IEC 60034-7. Below is an extract from the standard which shows equivalent terms in current use.

Code formulation

IM 1	00 1					
International Foot or flange type	Mounting position Type of shaft extension					
Code I	Code II					
IM B 3	IM 1001					
IM V 5	IM 1011					
IM V 6	IM 1031					
IM B 6	IM 1051					
IM B 7	IM 1061					
IM B 8	IM 1071					
IM B 20	IM 1101					
IM B 15	IM 1201					
IM B 35	IM 2001					
IM V 15	IM 2011					
IM V 36	IM 2031					
IM B 34	IM 2101					
IM B 5	IM 3001					
IM V 1	IM 3011					
IM V 21	IM 3051					
IM V 3	IM 3031					
IM V 4	IM 3211					
IM V 2	IM 3231					
IM B 14	IM 3601					
IM V 18	IM 3611					
IM V 19	IM 3631					
IM B 10	IM 4001					
IM V 10	IM 4011					
IM V 14	IM 4031					
IM V 16	IM 4131					
IM B 9	IM 9101					
IM V 8	IM 9111					
IM V 9	IM 9131					
IM B 30	IM 9201					
IM V 30	IM 9211					
IM V 31	IM 9231					

Codes I and II are interchangeable. It should however be noted that the above code list is not exhaustive and you should therefore refer to IEC 60034-7 for other designations. On the next page you will find the most common mounting arrangements with line drawings and an explanation of the standard symbols used.

Mounting options according to frame size

Some operating positions are prohibited for standard motors. Select the possible configurations for machine installation from the table below. In the case of difficulty, please consult Leroy-Somer.

E						Mounting	positions					
Frame size	IM 1001	IM 1051	IM 1061	IM 1071	IM 1011*	IM 1031	IM 3001	IM 3011*	IM 3031	IM 2001	IM 2011*	IM 2031
80 to 200	•	٠	٠	•	٠	٠	٠	٠	٠	•	٠	•
225 and 250	•	•	•	•	٠	•	о	٠	٠	•	٠	•
280 and 315	•	о	О	О	О	0	0	•	•	•	•	0

• : possible positions.

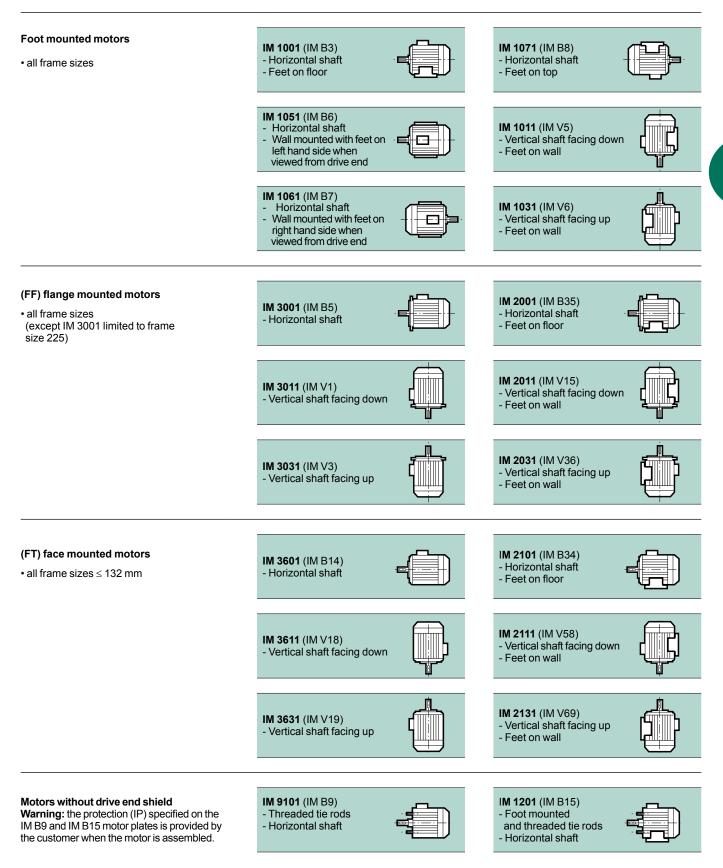
O: please consult Leroy-Somer specifying the coupling method and the axial and radial loads if applicable.

* : the use of a drip cover is recommended for these mounting arrangements.



C2 - Mounting arrangements

C2.2 - MOUNTINGS AND POSITIONS (IEC 60034-7)





C3 - Bearings and lubrication

C3.1 - TYPES OF BALL BEARING AND STANDARD FITTING ARRANGEMENTS

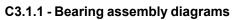
		Horizontal shaft	Vertical shaft		
			Shaft facing down	Shaft facing up	
	Mounting arrangement	B3 / B6 / B7 / B8	V5	V6	
Foot mounted motors	standard mounting	The DE bearing is: - located at DE for frame ≤ 180 - locked at DE for frame ≥ 200	The DE bearing is: - located at DE for frame ≤ 180 - locked at DE for frame ≥ 200	The DE bearing is: - locked at DE for frame \ge 100	
	on request	DE bearing locked	DE bearing locked		
	Mounting arrangement	B5 / B35 / B14 / B34	V1 / V15 / V18 / V58	V3 / V36 / V19 / V69	
Flange mounted (or foot and flange) motors	standard mounting	The DE bearing is locked	The DE bearing is locked	The DE bearing is locked	

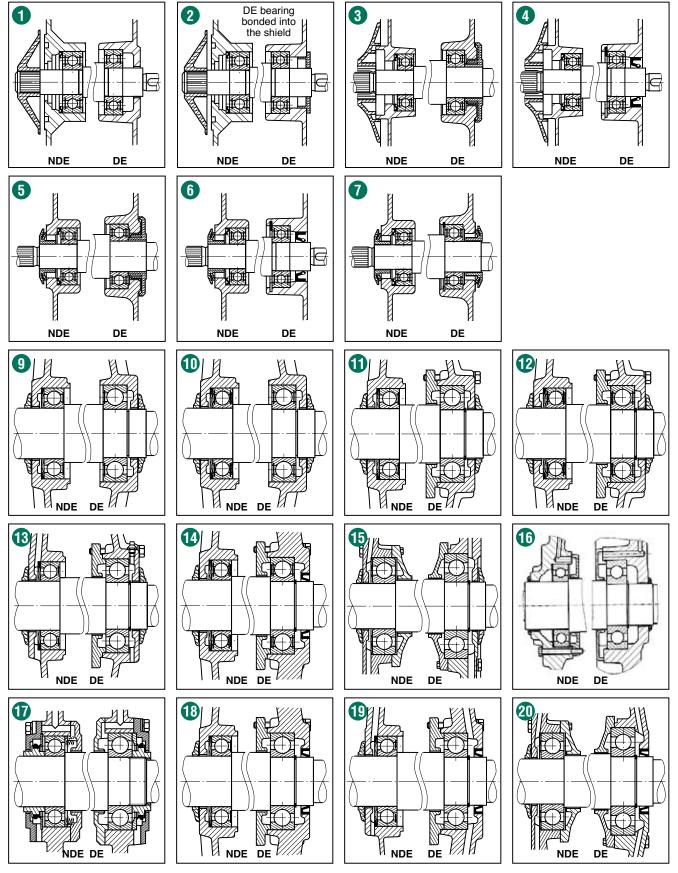
Important: When ordering, state correct mounting type and position (see section C1).

Me	otor			Standard	mounting	
			Non drive end		Assembly diag	ram reference
Frame/Type	LEROY-SOMER Designation	No. of poles	bearing (N.D.E.)	Drive end bearing (D.E.)	Foot mounted motors	Flange mounted (or foot and flange) motors
56 L	LS 56 L	2;4;6;8	6201 2RS C3	6201 2RS C3	0	2
63 M	LS 63 M	2;4;6;8	6201 2RS C3	6202 2RS C3	0	2
71 M	LS 71 M	2;4;6;8	6201 2RS C3	6202 2RS C3	0	2
80 L	LS 80 L	2;4	6203 ZZ CN	6204 ZZ C3	3	4
80 L	LS 80 L	6;8	6203 CN	6204 ZZ C3	5	6
90 S/L	LS 90 S - SL - L	2;4	6204 ZZ C3	6205 ZZ C3	3	4
90 L	LS 90 S - SL - L	6;8	6204 ZZ C3	6205 ZZ C3	5	6
100 L	LS 100 L	2;4;6;8	6205 ZZ C3	6206 ZZ C3	5	6
112 M	LS 112 M - MG - MR	2;4;6;8	6205 ZZ C3	6206 ZZ C3	5	6
112 M	LS 112 MU	2;4;6;8	6206 ZZ C3	6206 ZZ C3	5	6
132 S	LS 132 S	2;4;6;8	6206 ZZ C3	6208 ZZ C3	5	6
132 M	LS 132 M - SM	2;4;6;8	6207 ZZ C3	6308 ZZ C3	5	6
160 M	LS 160 MP	2;4	6208 ZZ C3	6309 ZZ C3	0	0
160 M	LS 160 M	6;8	6210 ZZ C3	6309 ZZ C3	10 (12 for V6)	14
160 L	LS 160 LR	4	6308 ZZ C3	6309 ZZ C3	0	7
160 L	LS 160 L	2;6;8	6210 ZZ C3	6309 ZZ C3	10 (12 for V6)	14
160 L	LS 160 LU	2-speed	6210 ZZ C3	6309 ZZ C3	10 (12 for V6)	1
180 M	LS 180 MT	2;4	6210 ZZ C3	6310 ZZ C3	10 (12 for V6)	14
180 L	LS 180 LR	4	6210 ZZ C3	6310 ZZ C3	10 (12 for V6)	1
180 L	LS 180 L	6;8	6212 Z C3	6310 Z C3	9 (11 for V6)	18
180 L	LS 180 LU	2-speed	6212 Z C3	6310 Z C3	9 (11 for V6)	18
200 L	LS 200 LT	2;4;6	6212 Z C3	6312 C3	1	18
200 L	LS 200 L	2;6;8	6214 Z C3	6312 C3	1	18
200 L	LS 200 LU	2-speed	6312 C3	6312 C3	15	20
225 S	LS 225 ST	4;8	6214 Z C3	6313 C3	13	19
225 M	LS 225 MT	2	6214 Z C3	6313 C3	13	19
225 M	LS 225 MR	2;4;6;8	6312 C3	6313 C3	15	20
225 M	LS 225 MG	2-speed	6216 C3	6314 C3	16	10
250 M	LS 250 MZ	2	6312 C3	6313 C3	15	20
250 M	LS 250 ME	4;6;8	6216 C3	6314 C3	16	10
280 S	LS 280 SC - MC	2	6216 C3	6314 C3	16	16
280 S	LS 280 SC	4;6;8	6216 C3	6316 C3	16	10
280 S	LS 280 SK - MK	2-speed	6317 C3	6317 C3	1	0
280 M	LS 280 MD	4;8	6218 C3	6316 C3	16	16
315 S	LS 315 SP	2	6317 C3	6317 C3	1	1
315 S	LS 315 SP	4;6;8	6317 C3	6320 C3	1	0
315 M	LS 315 MP - MR	2	6317 C3	6317 C3	1	0
315 M	LS 315 MP - MR	4;6;8	6317 C3	6320 C3	1	1



C3 - Bearings and lubrication







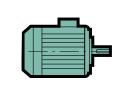
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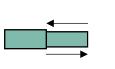
C3 - Bearings and lubrication

C3.2 - AXIAL LOADS

C3.2.1 - Permissible axial load (in daN) on main shaft extension for standard bearing assembly

Horizontal motor





Nominal lifetime L_{10h} of bearings: 25,000 hours

	Motor		oles 00 min ^{.1}		oles 00 min ^{.1}		oles 00 min ^{.1}	8 p N = 75	oles 10 min ^{.1}
Frame		\rightarrow		\rightarrow	←	\rightarrow		\rightarrow	←
size	Туре	IM B3 / B6 IM B7 / B8 IM B5 / B35 IM B14 / B34	IM B3 / B6 IM B7 / B8 IM B5 / B35 IM B14 / B34	IM B3 / B6 IM B7 / B8 IM B5 / B35 IM B14 / B34	IM B3 / B6 IM B7 / B8 IM B5 / B35 IM B14 / B34	IM B3 / B6 IM B7 / B8 IM B5 / B35 IM B14 / B34	IM B3 / B6 IM B7 / B8 IM B5 / B35 IM B14 / B34	IM B3 / B6 IM B7 / B8 IM B5 / B35 IM B14 / B34	IM B3 / B6 IM B7 / B8 IM B5 / B35 IM B14 / B34
56	LS 56 L	7	(28)*	14	(35)*	17	(38)*	18	(39)*
63	LS 63 M	13	(34)*	18	(39)*	26	(47)*	32	(53)*
71	L\$ 71 L	13	(34)*	18	(39)*	26	(47)*	32	(53)*
80	LS 80 L	23	(61)*	37	(75)*	45	(83)*	55	(93)*
90	LS 90 SR	19	(69)*	35	(85)*	44	(94)*	55	(105)*
90	LS 90 S	19	(69)*	35	(85)*	44	(94)*	55	(105)*
90	LS 90 L	19	(69)*	35	(85)*	44	(94)*	55	(105)*
100	LS 100 L	34	(90)*	57	(113)*	68	(124)*	83	(139)*
112	LS 112 M*	32	(88)*	46	(102)*	63	(119)*	78	(134)*
132	L\$ 132 \$	59	(137)*	92	(170)*	114	(192)*	-	-
132	LS 132 M	86	(188)*	125	(227)*	159	(261)*	192	(294)*
160	LS 160 M	-		-	-	237	(337)*	268	(368)*
160	LS 160 MP	147	(227)*	197	(277)*	-		-	-
160	LS 160 LR	-		188	(278)*	-	-	-	-
160	LS 160 L	131	(231)*	-	-	219	(319)*	249	(349)*
180	LS 180 MT	159	(259)*	207	(307)*	-		-	-
180	LS 180 LR	-	-	193	(293)*	-	-	-	-
180	LS 180 L			-		270	(318)*	318	(366)*
200	LS 200 LT	255	303	312	360	372	420	-	-
200	LS 200 L	247	313	-		366	432	455	521
225	LS 225 ST	-	-	366	432	-	-	501	567
225	LS 225 MT	278	344	-		-		-	
225	LS 225 MR	-	-	350	413	370	433	477	540
250	LS 250 MZ	275	338	-		-	-	-	-
250	LS 250 ME	-	-	392	462	451	521	523	593
280	LS 280 SC	294	364	464	534	538	608	627	697
280	LS 280 MC	291	361	-	-	524	594	-	-
280	LS 280 MD			437	507	-		569	657
315	LS 315 SP	500	320	790	610	864	684	1012	832
315	LS 315 MP	487	307	762	582	821	641	-	-
315	LS 315 MR	472	292	743	563	761	581	935	755

()* The axial loads shown above for IM B3 / B6 / B7 / B8 with frame size < 180 are the permissible axial loads for locked DE bearings (non-standard assembly, special order).

 * Also applies to LS 112 MG and MU.

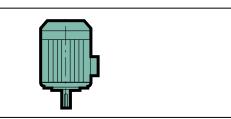


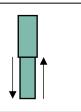
C3 - Bearings and lubrication

C3.2.1 - Permissible axial load (in daN) on main shaft extension for standard bearing assembly

Vertical motor Shaft facing down

Nominal lifetime L_{10h} of bearings: 25,000 hours





	Motor	2 po N = 300	oles)0 min [.] 1		oles 00 min [.] 1		oles 00 min ^{.1}	8 pc N = 75	oles 0 min ^{.1}
Frame size	Туре	IM V5 IM V1 / V15	IM V5 IM V1 / V15	IM V5 IM V1 / V15	IM V5 IM V1 / V15	IM V5 IM V1 / V15	IM V5 IM V1 / V15	IM V5 IM V1 / V15	IM V5 IM V1 / V15
		IM V18 / V58	IM V18 / V69	IM V18 / V69	IM V18 / V69	IM V18 / V69	IM V18 / V69	IM V18 / V69	IM V18 / V69
56	LS 56 L	6	(24)*	13	(36)*	16	(39)*	19	(40)*
63	LS 63 M	11	(36)*	16	(41)*	24	(49)*	30	(55)*
71	LS 71 L	11	(36)*	16	(41)*	24	(49)*	30	(55)*
80	LS 80 L	22	(63)*	35	(79)*	42	(89)*	52	(99)*
90	LS 90 SR	17	(73)*	31	(91)*	41	(100)*	52	(111)*
90	LS 90 S	17	(73)*	31	(91)*	41	(100)*	52	(111)*
90	LS 90 L	17	(73)*	31	(91)*	41	(100)*	52	(111)*
100	LS 100 L	32	(94)*	54	(119)*	64	(131)*	79	(146)*
112	LS 112 M*	29	(93)*	41	(111)*	57	(129)*	72	(144)*
132	LS 132 S	51	(149)*	83	(185)*	105	(207)*	-	-
132	LS 132 M	73	(207)*	110	(251)*	140	(291)*	176	(321)*
160	LS 160 M	-	-	-	-	213	(376)*	245	(408)*
160	LS 160 MP	129	(245)*	177	(297)*	-		-	-
160	LS 160 LR		-	165	(301)*	-	-	-	
160	LS 160 L	111	(261)*	-	-	191	(370)*	224	(397)*
180	LS 180 MT	136	(293)*	182	(353)*	-	-	-	-
180	LS 180 LR	-	-	166	(345)*	-	-	-	-
180	LS 180 L	-	-	-	-	232	(385)*	279	(438)*
200	LS 200 LT	222	352	276	429	329	504	-	-
200	LS 200 L	209	370	-	-	314	521	403	606
225	LS 225 ST	-	-	314	517	-	-	443	670
225	LS 225 MT	236	408	-	-	-	-	-	-
225	LS 225 MR	-	-	292	514	310	553	414	661
250	LS 250 MZ	225	414	-	-		-	-	
250	LS 250 ME	-	-	311	607	363	687	424	778
280	LS 280 SC	224	481	360	707	436	795	511	904
280	LS 280 MC	209	492	-	-	406	804	-	
280	LS 280 MD		-	315	718	-	-	439	908
315	LS 315 SP	344	544	601	896	657	1018	805	1167
315	LS 315 MP	317	561	553	916	591	1034	-	
315	LS 315 MR	278	586	506	949	508	1044	678	1215

()* The axial loads shown above for IM V5 with frame size ≤ 180 are the permissible axial loads for locked DE bearings (non-standard assembly, special order).

 * Also applies to LS 112 MG and MU.



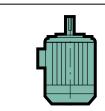
31

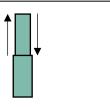
C3 - Bearings and lubrication

C3.2.1 - Permissible axial load (in daN) on main shaft extension for standard bearing assembly

Vertical motor Shaft facing up

Nominal lifetime L_™ of bearings: 25,000 hours





	Motor		oles 00 min ^{.1}		oles 00 min ^{.1}		oles 00 min ^{.1}		oles i0 min ^{.1}
Frame size	Туре	\downarrow	1	Ļ	Î	Ļ	1	Ļ	Î
3126		IM V6 IM V3 / V36 IM V19 / V69	IM V6 IM V3 / V36 IM V19 / V69	IM V6 IM V3 / V36 IM V19 / V69	IM V6 IM V3 / V36 IM V19 / V69	IM V6 IM V3 / V36 IM V19 / V69	IM V6 IM V3 / V36 IM V19 / V69	IM V6 IM V3 / V36 IM V19 / V69	IM V6 IM V3 / V36 IM V19 / V69
56	LS 56 L	8	27	15	34	18	39	18	38
63	LS 63 M	15	32	20	37	28	45	34	51
71	L\$ 71 L	15	32	20	37	28	45	34	51
80	LS 80 L	60	25	73	41	80	51	90	61
90	LS 90 SR	67	23	81	41	91	50	102	61
90	LS 90 S	67	23	81	41	91	50	102	61
90	LS 90 L	67	23	81	41	91	50	102	61
100	LS 100 L	88	38	110	63	120	75	135	90
112	LS 112 M*	85	37	97	55	113	73	128	88
132	LS 132 S	129	71	161	107	183	129	<u> </u>	
132	LS 132 M	175	105	212	149	242	189	278	219
160	LS 160 M	-	-	-	-	313	276	345	308
160	LS 160 MP	209	165	257	217	-	-	-	-
160	LS 160 LR		-	(255)*	211	-	-	-	-
160	LS 160 L	211	161	-	-	291	270	324	297
180	LS 180 MT	236	193	282	253	-	-	-	-
180	LS 180 LR	-	-	266	245	-		-	-
180	LS 180 L	-	-	-	-	280	337	327	390
200	LS 200 LT	270	304	324	381	377	456	-	-
200	LS 200 L	275	304			380	455	469	540
225	LS 225 ST	-	-	380	451	-	-	509	604
225	LS 225 MT	302	342			-			
225	LS 225 MR	-	-	355	451	373	490	477	598
250	LS 250 MZ	288	351			-			
250	LS 250 ME	-	-	381	537	433	617	494	708
280	LS 280 SC	294	411	430	637	506	725	834	581
280	LS 280 MC	279	422	-	-	476	734	-	-
280	LS 280 MD	· ·		385	648	-		820	527
315	LS 315 SP	164	724	421	1076	477	1198	625	1347
315	LS 315 MP	137	741	373	1096	411	1214		
315	LS 315 MR	98	766	326	1129	328	1224	498	1395

* Also applies to LS 112 MG and MU.



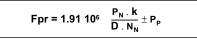
C3 - Bearings and lubrication

C3.3 - RADIAL LOADS C3.3.1 - Permissible radial load on main shaft extension

In pulley and belt couplings, the drive shaft carrying the pulley is subjected to a radial force Fpr applied at a distance X (mm) from the shoulder of the shaft extension (length E).

• Radial force applied to drive shaft extension: Fpr

The radial force Fpr expressed in daN applied to the shaft extension is found by the formula.



where:

- $P_{_{N}}$ = rated motor power (kW)
- D = external diameter of the drive pulley (mm) N_{N} = rated speed of the motor (min⁻¹)

k = factor depending on the type of transmission

 $P_{P_{P}}$ = weight of the pulley (daN)

The weight of the pulley is positive when it acts in the same direction as the tension force in the belt (and negative when it acts in the opposite direction).

Range of values for factor k(*)

- toothed belts	k١	= 1 t	o 1	.5
- V-belts	k۶	= 2 t	o 2	.5
- flat belts				

 • with tensioner
 k = 2.5 to 3

 • without tensioner
 k = 3 to 4

(*) A more accurate figure for factor k can be obtained from the transmission suppliers.

• Permission radial force on the drive shaft extension

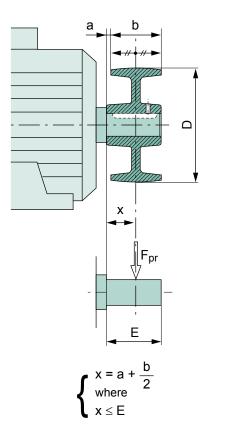
The charts on the following pages indicate, for each type of motor, the radial force $F_{\rm \tiny R}$ at a distance X permissible on the drive end shaft extension, for a bearing life $L_{\rm ton}$ of 25,000 hours.

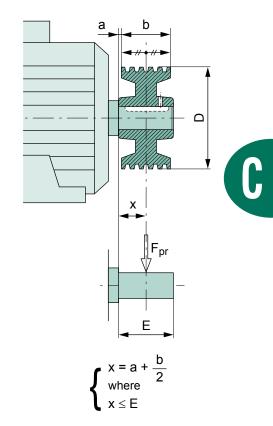
Note: For frame sizes \geq 315 M, the selection charts are applicable for a motor installed with the shaft horizontal.

• Change in bearing life depending on the radial load factor

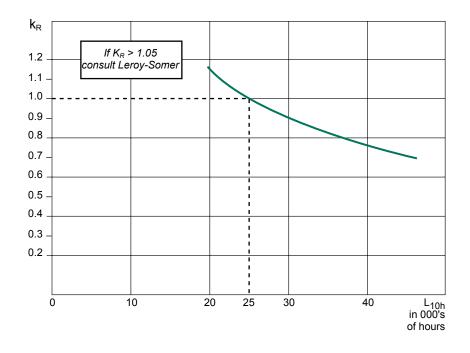
For a radial load Fpr (Fpr \neq F_R), applied at distance X, the bearing life L_{10b} changes, at a first approximation, in the ratio k_R, (k_R = Fpr / F_R) as shown in the chart opposite, for standard assemblies.

If the load factor $k_{\rm \tiny R}$ is greater than 1.05, you should consult our technical department, stating mounting position and direction of force before opting for a special assembly.





Change in bearing life L_{m} depending on the radial load factor k_{p} for standard assemblies.

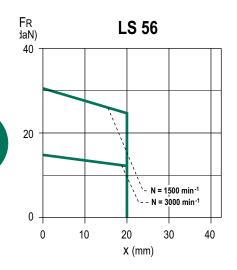


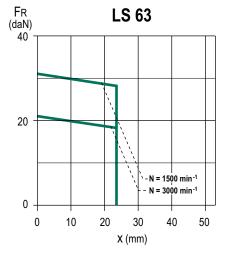


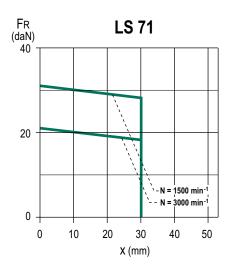
C3 - Bearings and lubrication

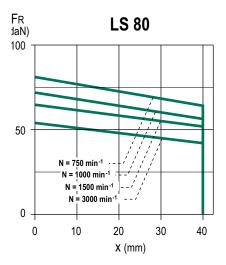
C3.3.2 - Standard mounting

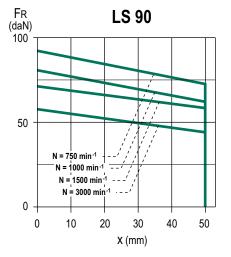
Permissible radial load on main shaft extension with a bearing life L_{10h} of 25,000 hours.

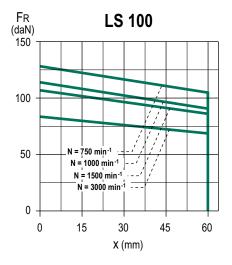


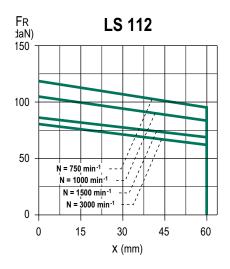


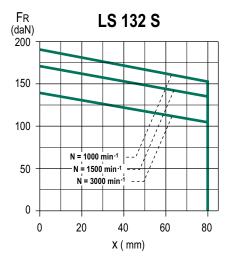


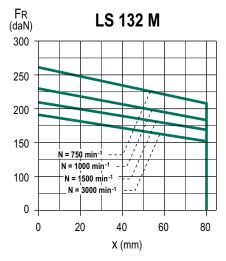










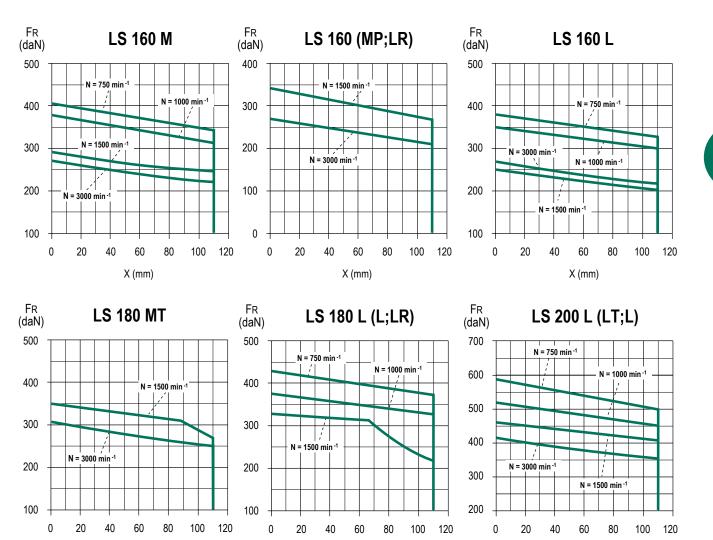


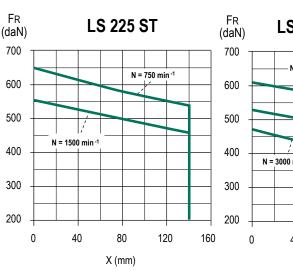
LEROY® SOMER

C3 - Bearings and lubrication

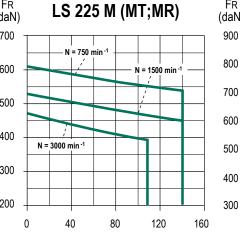
C3.3.2 - Standard assembly

Permissible radial load on main shaft extension with a bearing life $L_{_{10h}}$ of 25,000 hours.





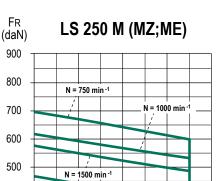
X (mm)



X (mm)

SOMER

X (mm)



80

X (mm)

120

160

N = 3000 min ⁻¹

40

0

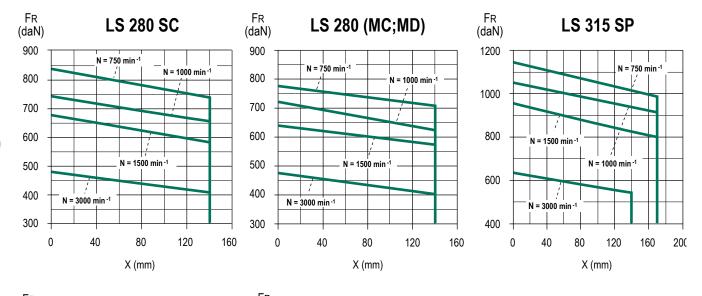
X (mm)

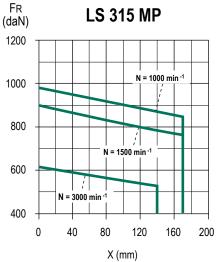


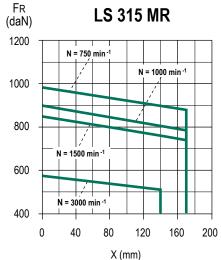
C3 - Bearings and lubrication

C3.3.2 - Standard assembly

Permissible radial load on main shaft extension with a bearing life $L_{_{10h}}$ of 25,000 hours.









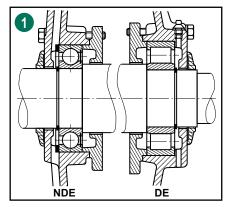
C3 - Bearings and lubrication

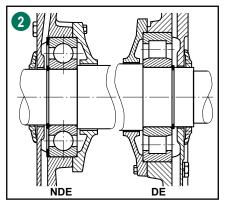
C3.4 - TYPES AND SPECIAL FITTING ARRANGEMENTS FOR DE ROLLER BEARINGS

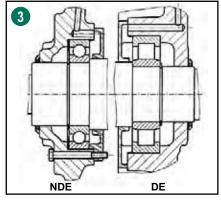
Motor			Standard mounting				
-	LEROY-SOMER	No. Sector	Non drive end	Drive end	Assembly dia	gram reference	
Frame size	Designation	No. of poles	bearing (N.D.E.)	bearing (D.E.)	Foot mounted motors	Flange mounted (or foot and flange) motors	
160	LS 160 M/L	6;8	6210 Z C3	NU 309	1	6	
160	LS 160 LU	*	6210 Z C3	NU 309	1	5	
180	LS 180 MT	4	6210 Z C3	NU 310	1	5	
180	LS 180 LR	4	6210 Z C3	NU 310	1	5	
180	LS 180 L	6;8	6212 Z C3	NU 310	1	5	
180	LS 180 LU	*	6212 Z C3	NU 310	1	5	
200	LS 200 LT	4;6	6212 Z C3	NU 312	1	6	
200	LS 200 L	6;8	6214 Z C3	NU 312	1	5	
200	LS 200 LU	*	6312 C3	NU 312	1	6	
225	LS 225 ST	4;8	6214 Z C3	NU 313	1	5	
225	LS 225 MR	4;6;8	6312 C3	NU 313	2	6	
225	LS 225 MG	*	6216 C3	NU 314	3	3	
250	LS 250 ME	4	6216 C3	NU 314	3	3	
280	LS 280 SC	4	6216 C3	NU 316	3	3	
280	LS 280 MD	4	6218 C3	NU 316	3	3	
280	LS 280 SK - MK	*	6317 C3	NU 317	4	4	
315	LS 315 SP - MP - MR	4;6;8	6317 C3	NU 320	4	4	

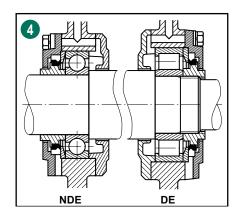
* 2-speed motors (excluding 2-pole motors).

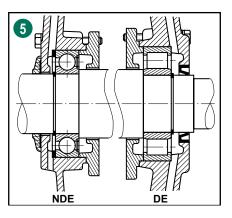
C3.4.1 - Bearing assembly diagrams

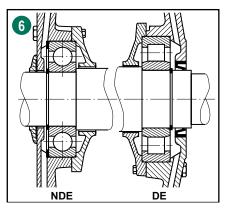












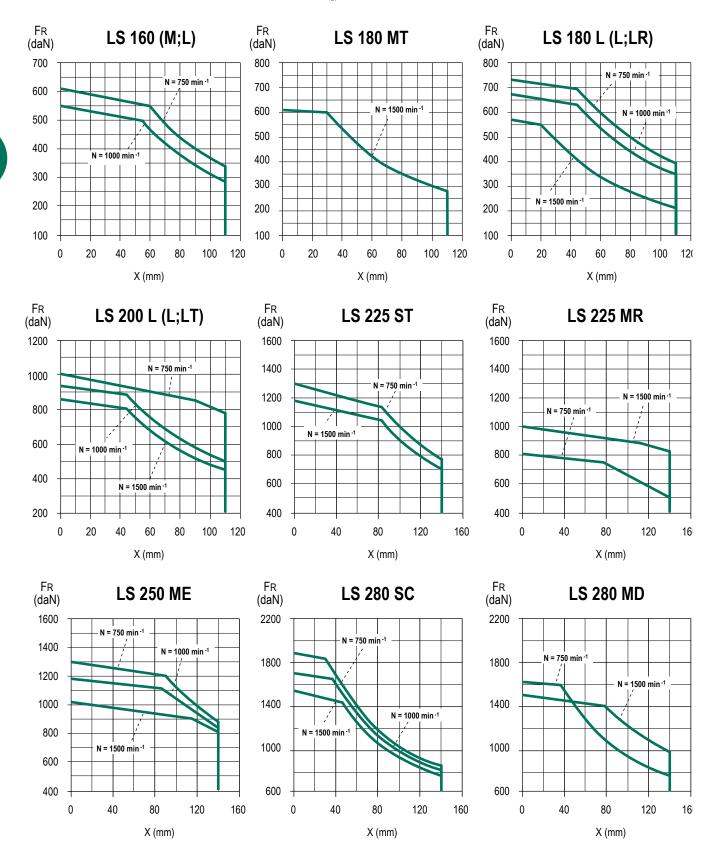




C3 - Bearings and lubrication

C3.4.2 - Special fitting arrangements

Permissible radial load on main shaft extension with a bearing life $L_{_{10h}}$ of 25,000 hours.

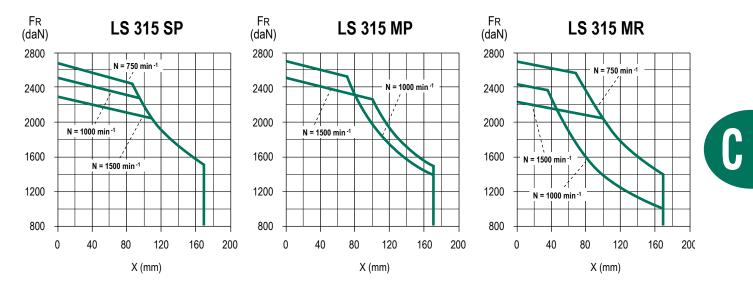




C3 - Bearings and lubrication

C3.4.2 - Special fitting arrangements

Permissible radial load on main shaft extension with a bearing life $L_{_{10h}}$ of 25,000 hours.





C3 - Bearings and lubrication

C3.5 - BEARINGS AND BEARING LIFE

Definitions

Load ratings

- Basic static load C_o:

This is the load for which permanent deformation at point of contact between a bearing race and the ball (or roller) with the heaviest load reaches 0.01% of the diameter of the ball (or roller).

- Basic dynamic load C:

This is the load (constant in intensity and direction) for which the nominal lifetime of the bearing will reach 1 million revolutions.

The static load rating C_{\circ} and dynamic load rating C are obtained for each bearing by following the method in ISO 281.

Lifetime

The lifetime of a bearing is the number of revolutions (or number of operating hours at a constant speed) that the bearing can accomplish before the first signs of fatigue (spalling) begin to appear on a ring, ball or roller.

- Nominal lifetime L10h

According to the ISO recommendations, the nominal lifetime is the length of time completed or exceeded by 90% of apparently identical bearings operating under the conditions specified by the manufacturer.

Note: The majority of bearings last much longer than the nominal lifetime; the average lifetime achieved or exceeded by 50% of bearings is around 5 times longer than the nominal lifetime.

Determination of nominal lifetime Constant load and speed of rotation

The nominal lifetime of a bearing expressed in operating hours L_{ron} , the basic dynamic load C expressed in daN and the applied loads (radial load F_r and axial load F_s) are related by the following equation:

$$L_{10h} = \frac{1000000}{60 \cdot N} \cdot \left(\frac{C}{P}\right)^{p}$$

where N = speed of rotation (min⁻¹)

P (P = X F_r + Y F_a): equivalent dynamic load (F_r, F_a, P in daN)

 p: an index which depends on the type of contact between the races and balls (or rollers)

p = 3 for ball bearings

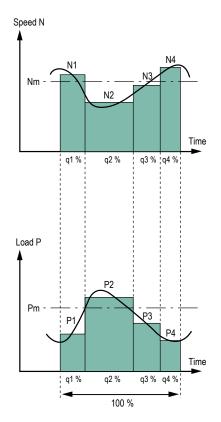
p = 10/3 for roller bearings

The formulae that give Equivalent Dynamic Load (values of factors X and Y) for different types of bearing may be obtained from their respective manufacturers.

Variable load and speed of rotation

For bearings with periodically variable load and speed, the nominal lifetime is established using the equation:

$$L_{10h} = \frac{1000000}{60 \cdot N_m} \cdot \left(\frac{C}{P_m}\right)^p$$



N_m: average speed of rotation

$$N_m = N_1 \cdot \frac{q_1}{100} + N_2 \cdot \frac{q_2}{100} + \dots (min^{-1})$$

P_m: average equivalent dynamic load

$$\mathbf{P}_{m} = \mathbf{P}_{N} \left[\mathbf{P}_{1}^{\mathbf{P}} \cdot \left(\frac{\mathbf{N}_{1}}{\mathbf{N}_{m}} \right) \cdot \frac{\mathbf{q}_{1}}{100} + \mathbf{P}_{2}^{\mathbf{P}} \cdot \left(\frac{\mathbf{N}_{2}}{\mathbf{N}_{m}} \right) \cdot \frac{\mathbf{q}_{2}}{100} + \dots \right] (daN)$$

with q_1 , q_2 , etc as a %

Nominal lifetime L_{100} is applicable to bearings made of bearing steel and normal operating conditions (lubricating film present, no contamination, correctly fitted, etc). Situations and data differing from these conditions will lead to either a reduction or an increase in lifetime compared to the nominal lifetime.

Corrected nominal lifetime

If the ISO recommendations (DIN ISO 281) are used, improvements to bearing steel, manufacturing processes and the effects of operating conditions may be integrated in the nominal lifetime calculation.

The theoretical pre-fatigue lifetime ${\rm L}_{\rm \tiny nah}$ is thus calculated using the formula:

$$L_{nah} = a_1 a_2 a_3 L_{10h}$$

where:

a,: failure probability factor

 a_2 : factor for the characteristics and tempering of the steel

a_s: factor for the operating conditions (lubricant quality, temperature, speed of rotation, etc)

Under normal operating conditions for LS motors, the corrected nominal lifetime, calculated with a failure probability factor a1 = 1 (L_{toah}), is longer than the nominal lifetime L_{toa} .



C3 - Bearings and lubrication

C3.6 - LUBRICATION AND MAINTENANCE OF BEARINGS Role of the lubricant

The principal role of the lubricant is to avoid direct contact between the metal parts in motion: balls or rollers, slip-rings, cages, etc. It also protects the bearing against wear and corrosion.

The quantity of lubricant needed by a bearing is normally quite small. There should be enough to provide good lubrication without undesirable overheating. As well as lubrication itself and the operating temperature, the amount of lubricant should be judged by considerations such as sealing and heat dissipation.

The lubricating power of a grease or an oil lessens with time owing to mechanical constraints and straightforward ageing. Used or contaminated lubricants should therefore be replaced or topped up with new lubricant at regular intervals.

Bearings can be lubricated with grease, oil or, in certain cases, with a solid lubricant.

C1.2.1 - Lubricating with grease

A lubricating grease can be defined as a product of semi-fluid consistency obtained by the dispersion of a thickening agent in a lubricating fluid and which may contain several additives to give it particular properties.

Composition of a grease				
Base oil: 85 to 97%				
Thickener: 3 to 15%				
Additives: 0 to 12%				

The base oil lubricates

The oil making up the grease **is of prime importance**. It is the oil that lubricates the moving parts by coating them with a protective film which prevents direct contact. The thickness of the lubricating film is directly linked to the viscosity of the oil, and the viscosity itself depends on temperature. The two main types used to make grease are mineral oils and synthetic oils. Mineral oils are suitable for normal applications in a range of temperatures from -30° to +150°C. Synthetic oils have the advantage of being effective in severe conditions (extreme variations of temperature, harsh chemical environments, etc).

The thickener gives the grease consistency

The more thickener a grease contains, the 'harder' it will be. Grease consistency varies with the temperature. In falling temperatures, the grease hardens progressively, and the opposite happens when temperatures rise. The consistency of a grease can be quantified using the NLGI (National Lubricating Grease Institute) classification. There are 9 NLGI grades, from 000 for the softest greases up to 6 for the hardest. Consistency is expressed by the depth to which a cone may be driven into a grease maintained at 25 °C.

If we only consider the chemical nature of the thickener, lubricating greases fall into three major categories:

• conventional greases with a metallic soap base (calcium, sodium, aluminium, lithium). Lithium soaps have several advantages over other metallic soaps: a high melting point (180° to 200°), good mechanical stability and good water resistant properties.

• greases with a complex soap base The main advantage of this type of soap is a very high melting point (over 250°C).

• soapless greases. The thickener is an inorganic compound, such as clay. Their main property is the absence of a melting point, which makes them practically non-liquefying.

Additives improve some properties of greases

Additives fall into two types, depending on whether or not they are soluble in the base oil.

The most common insoluble additives graphite, molybdenum disulphide, talc, mica, etc, improve the friction characteristics between metal surfaces. They are therefore used in applications where heavy pressure occurs.

The soluble additives are the same as those used in lubricating oils: antioxidants, anti-rust agents, etc.

C3.6.2 - Grease life

The lifetime of a lubricating grease depends on:

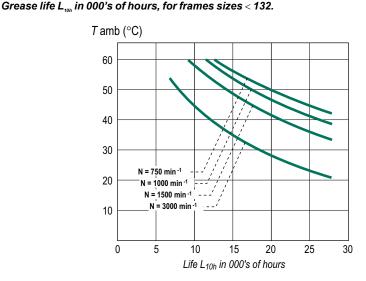
- the characteristics of the grease (type of soap and base oil, etc)

- service stress (type and size of bearing, speed of rotation, operating temperature, etc)

- contamination

C3.6.2.1 - Permanently greased bearings

For motors from 56 frame to 132 frame, the type and size of the bearings make for long grease life and therefore lubrication for the lifetime of the machine. The grease life L_{10h} according to speed of rotation and ambient temperature is shown on the chart opposite.



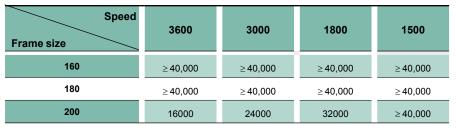


C3 - Bearings and lubrication

C3.6.2.2 - Bearings without grease nipples

Motors of frame sizes 160 and 180 with permanently greased bearings and motors of frame size 200 with bearings, factory lubricated with a complex lithium soap grease that has an operating range of -20° C to $+150^{\circ}$ C, are not fitted with grease nipples.

Lubricant lifetime (L10h) under normal operating conditions is given in the table below for a machine with horizontal shaft operating at 50 Hz and 60 Hz in ambient temperatures of 25°C or less.



Note: On request, motors of frame size 90 to 200 mm can be fitted with grease nipples, and motors of frame sizes 225 and 250 can be supplied without grease nipples.

C3.6.2.3 - Bearings with grease nipples

The chart opposite shows the regreasing intervals, depending on the type of motor, for standard bearing assemblies of frame size \geq 160 fitted with grease nipples, operating at an ambient temperature of 25°C on a horizontal shaft machine.

The chart opposite is valid for LS motors lubricated with ESSO UNIREX N3 grease, which is used as standard.

C3.6.2.4 - Special construction and environment

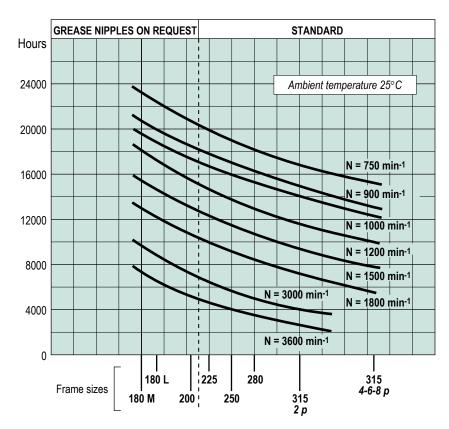
For vertical shaft machines operating at an ambient 25°C, the regreasing intervals will be approximately 80% of those shown on the chart.

Motors operating at an ambient 40°C need more frequent lubrication. The intervals between greasing will be about half of those shown on the chart.

Note: the quality and quantity of grease and the regreasing interval are shown on the machine identification plate.

For special assemblies (motors fitted with DE roller bearings or other types), machines of frame size \geq 160 have bearings with grease nipples. Instructions for bearing maintenance are given on the identification plates on these machines.

Regreasing intervals according to frame size and speed of rotation (for standard bearing assemblies).





3-phase TEFV induction motors LS aluminium alloy frame Construction LS motors are of standard configuration IC 411 C4 - Cooling New designation for the IC (International IC 4 A 1 A 1 Cooling) coded cooling method in the IEC Circulation mode for secondary fluid (1: self-circulating) 60034-6 standard. Secondary fluid (A : air) The standard allows for two designations Circulation method for primary fluid (1: self-circulating) ٠ (general formula and simplified formula) as Primary fluid (A: air) shown in the example opposite. Circuit layout (4: machine surface-cooled) Note: the letter A may be omitted if this will not lead to confusion. This contracted formula becomes the simplified formula.

Coolant

Circuit layout

Simplified form: IC 411.

Character- istic number	Designation	Description
O (1)	Free circulation	The coolant enters and leaves the machine <i>freely</i> . It is taken from and returned to the fluid round the machine.
1 (1)	Machine with an intake pipe	The coolant is taken up elsewhere than from the fluid round the machine, brought into the machine through an <i>intake pipe</i> and emptied into the fluid round the machine.
2 (1)	Machine with an outlet pipe	The coolant is taken up from the fluid round the machine, brought away from the machine by an <i>outlet pipe</i> and does not go back into the fluid round the machine.
3 (1)	Machine with two pipes (intake and outlet)	The coolant is taken up elsewhere than from the fluid round the machine, brought to the machine through an <i>intake pipe</i> , then taken away from the machine through an <i>outlet pipe</i> and does not go back into the fluid round the machine.
4	Surface cooled machine using the fluid round the machine	The primary coolant circulates in a closed circuit, transferring its heat to a secondary coolant (the one surrounding the machine) through the machine casing. The casing surface is either smooth or finned to improve heat transmission.
5 (2)	Built-in heat exchanger (using the surrounding environment)	The primary coolant circulates in a <i>closed</i> circuit, transferring its heat to a secondary coolant (the one surrounding the machine) in an integral heat exchanger inside the machine.
6(2)	Machine-mounted heat exchanger (using the surrounding environment)	The primary coolant circulates in a closed circuit, transferring its heat to a secondary coolant (the one surrounding the machine) in a heat exchanger that forms an independent unit, mounted on the machine.
7 (2)	Built-in heat exchanger (not using the surrounding environment)	The primary coolant circulates in a closed circuit, transferring its heat to a secondary coolant (which is not the one round the machine) in an integral heat exchanger inside the machine.
8 (2)	Machine-mounted heat exchanger (not using the surrounding environment)	The primary coolant circulates in a closed circuit, transferring its heat to a secondary coolant (which is not the one round the machine) in a heat exchanger that forms an independent unit, mounted on the machine.
9 (2)(3)	Separate heat exchanger (using/not using the surrounding environment)	The primary coolant circulates in a closed circuit, transferring its heat to the secondary fluid in a heat exchanger that forms an independent unit, away from the machine.

Character- istic letter	Type of fluid
А	Air
F	Freon
Н	Hydrogen
Ν	Nitrogen
С	Carbon dioxide
W	Water
U	Oil
S	Any other fluid (must be identified separately)
Y	The fluid has not yet been selected (used temporarily)

Method of circulation

Character- istic number	Designation	Description
0	Free circulation	The circulation of the coolant is due only to differences in temperature. Ventilation caused by the rotor is negligible.
1	Self-circulating	The circulation of the coolant depends on the rotational speed of the main machine, and is caused by the action of the rotor alone, or a device mounted directly on it.
2, 3, 4		Not yet defined.
5 (4)	Built-in, independent device	The coolant is circulated by a built-in device which is powered independently of the rotational speed of the main machine.
6 (4)	Independent device mounted on the machine	The coolant is circulated by a device mounted on the machine which is powered independently of the rotational speed of the main machine.
7 (4)	Entirely separate independent device or using the pressure of the coolant circulation system	The coolant is circulated by a separate electrical or mechanical device, independent and not mounted on the machine, or by the pressure in the coolant circulation system.
8 (4)	Relative displacement	The circulation of the coolant is produced by the relative movement between the machine and the coolant, either by displacement of the machine in relation to the coolant, or by the flow of the surrounding coolant.
9	Any other device	The coolant is circulated using a method other than those defined above: it must be described in full.

(1) Filters or labyrinths for dust removal or noise protection can be fitted inside the casing or in the ducting. The first designation numbers 0 to 3 also apply to machines in which the coolant is taken up at the outlet of a watercooler designed to lower the temperature of the ambient air or recirculated through a watercooler so as not to increase the ambient temperature.

(2) The nature of the heat exchanger elements is not specified (smooth or finned tubes, corrugated surfaces, etc).

(3) A separate heat exchanger can be installed near to or at a distance from the machine. A secondary gas coolant may or may not be the surrounding medium.

(4) Use of such a device does not exclude the ventilating action of the rotor or the existence of an additional fan mounted directly on the rotor.



C4 - Cooling

C4.1 - STANDARD CODES

IC 01	Self-cooling open machine. Fan mounted on the shaft.	
IC 410	Enclosed machine, surface-cooled by natural convection and radiation. No external fan.	
IC 411	Enclosed machine. Smooth or finned ventilated casing. External shaft-mounted fan.	
IC 416 A*	Enclosed machine. Smooth or finned enclosed casing. External motorized axial (A) fan supplied with the machine.	
IC 416 R*	Enclosed machine. Smooth or finned enclosed casing. External motorized radial (R) fan supplied with the machine.	
IC 418	Enclosed machine. Smooth or finned casing. No external fan. Ventilation provided by air flow coming from the driven system.	

* Features not within manufacturer's standard range.

Application of cooling systems to the LEROY-SOMER range

Frame size	IC 410/IC 418	IC 411	IC 416 A	IC 416 R	
56	•	0			
63	•	o			
71	•	0	•		
80	•	o	•		
90	•	o	•	Please consult Leroy-Somer	
100	•	O	•	Please consult Leroy-Somer	
112	•	o	•	Please consult Leroy-Somer	
132	•	0	•	Please consult Leroy-Somer	
160	•	o	•	Please consult Leroy-Somer	
180	•	0	•	Please consult Leroy-Somer	
200	•	• •	•	Please consult Leroy-Somer	
225	•	0	•	Please consult Leroy-Somer	
250	•	o	•	Please consult Leroy-Somer	
280	•	0	•	Please consult Leroy-Somer	
315	•	o	•	Please consult Leroy-Somer	

• : possible. O : standard construction

Other cooling systems may be fitted as options:

- complete immersion of motor in oil.

- circulation of water inside housing for frame sizes \leq 132

- sealed motor submerged in water for frame sizes \leq 132



C4.2 - VENTILATION

C4.2.1 - Motor ventilation

In compliance with IEC 60034-6, the motors in this catalogue are cooled using method IC 411, ie. «surface-cooled machine using the ambient air circulating round the machine».

Cooling is achieved by a fan mounted at the NDE of the motor, inside a fan cover which acts as a safety guard (control conforming to IEC 60034-5). The fan draws the air through the grille in the cover and sends it along the housing fins, giving an identical heat balance in either direction of rotation (except for 2-pole motors of frame size 315).

Note: Obstruction - even accidental - of the fan cover grille (grille clogged or placed against a wall) has an adverse effect on the motor cooling process.

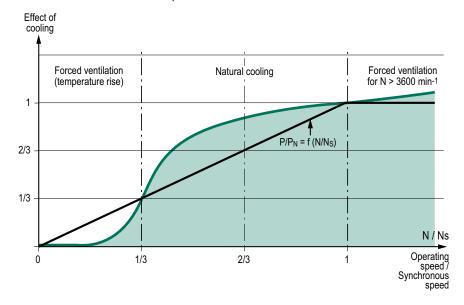
C4 - Cooling

Cooling of variable speed motors

Special precautions need to be taken when standard induction motors are being used with variable speed, powered by an inverter or voltage controller.

In prolonged operation at low speed, cooling efficiency is lost. It is therefore advisable to install forced ventilation that will produce a constant flow independent of the motor speed.

In prolonged operation at high speed, the fan may make excessive noise. It is again advisable to install a forced ventilation system.



C4.2.2 - Non-ventilated applications in continuous operation

Motors can be supplied without fans. Dimensions will depend on the application.

a) IC 418 cooling system

Placed in the air flow from a fan, these motors are capable of achieving their power rating if the speed of the air between the housing fins and the overall flow rate of the air between the fins comply with the figures in the table opposite.

	2 poles		4 poles		6 poles and above	
Frame size	flow rate m³/h	speed m/s	flow rate m³/h	speed m/s	flow rate m³/h	speed m/s
56	37	8	16	3.5	9	2
63	50	7.5	23	4	13	2
71	82	7.5	39	4.5	24	2
80	120	7.5	60	4	40	2.5
90	200	11.5	75	5.5	60	3.5
100	300	15	130	7.5	95	5
112	460	18	200	9	140	6
132	570	21	300	10.5	220	7
160	800	21	400	11	500	9
180	900	21	600	13	550	10
200	1100	23	800	14	700	10
225	1200	24	900	15	800	13
250	1600	25	1400	17	1400	13
280	1800	25	1500	18	1500	15
315	3000	25	2000	20	2000	15

These air flows are valid for normal working conditions as described in section B2.1.



C4 - Cooling

a) IC 410 cooling system

Used for general applications without cooling, these motors will provide the output powers given in the table below (if this is the case, their internal design is adapted to the power provided, for an ambient temperature of 40° C and a temperature rise corresponding to insulation class F).

Non ventilated three-phase induction motors - 50 Hz - IC 410 (temperature rise class F)

Power kW	No. of poles 2 poles	No. of poles 4 poles	No. of poles 6 poles	No. of poles 8 poles
0.18	LS 71 L	LS 71 L	LS 80 L	LS 90 L
0.25	LS 71 L	LS 80 L	LS 80 L	LS 90 L
0.37	LS 80 L	LS 80 L	LS 90 L	LS 100 L
0.55	LS 80 L	LS 90 S	LS 90 L	LS 100 L
0.75	LS 80 L	LS 90 L	LS 100 L	LS 112 MG
0.9	LS 90 L	LS 90 L	LS 100 L	LS 112 MG
1.1	LS 90 L	LS 100 L	LS 112 MG	LS 132 SM
1.5	LS 100 L	LS 100 L	LS 112 MG	LS 132 M
1.85	LS 100 L	LS 112 MG	LS 132 M	LS 160 M
2.2	LS 112 MG	LS 112 MG	LS 132 M	LS 160 M
3	LS 132 SM	LS 132 SM	LS 160 M	LS 160 M
3.7	LS 132 SM	LS 132 M	LS 160 M	LS 160 L
4	LS 132 M	LS 132 M	LS 160 L	LS 160 L
5.5	LS 160 L	LS 160 LR	LS 160 L	LS 180 L
7.5	LS 180 MT	LS 180 MT	LS 180 L	LS 200 L
11	LS 200 L	LS 200 LT	LS 200 L	LS 225 MR
15	LS 225 MR	LS 225 ST	LS 225 MR	LS 250 MK
18.5	LS 250 MZ	LS 225 MR	LS 250 ME	LS 280 SC
22	LS 280 SC	LS 250 ME	LS 280 SC	LS 280 MD
30	LS 280 MC	LS 280 SC	LS 315 SP	LS 315 SP
37	LS 315 SP	LS 280 MD	LS 315 SP	LS 315 MP
45	LS 315 MP	LS 315 SP	LS 315 MP	-
55	LS 315 MR	LS 315 MR	LS 315 MR	-

Dimensions: see pages 105 to 109



C5 - Mains connection

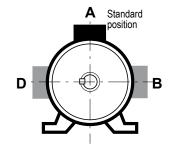
C5.1 - TERMINAL BOX

Placed as standard on the top of the motor near the drive end, the terminal box has IP 55 protection and is fitted with a cable gland (see table in C5.2).

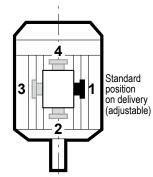
The standard position of the cable gland is on the right, seen from the drive end, but, owing to the symmetrical construction of the box, it can be placed in any of the 4 directions (except position **2** on flange-mounted motors).

If required, the terminal box may be fitted in a different position (on the left or right as seen from the drive end, and at the DE or NDE of the motor housing).

Positions of the terminal box in relation to the drive end (motor in IM 1001 position)

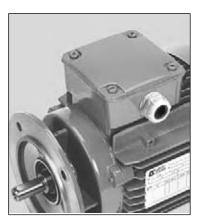


Positions of the cable gland in relation to the drive end





Position 2 not recommended and it is not possible on standard (FF) flange-mounted motor



Terminal box for 71 frame



Terminal box for 80 to 112 frame



Terminal box for 200 to 315 frame

C5.1.1 - Flying leads

According to specification, motors can be supplied with flying leads or multicore cables. Please state cable characteristics (type and supplier, cross-section, length, number of conductors), connection method (on stator coil end turns, or on a separate panel), and the cable gland position required.



SOMER







C5 - Mains connection

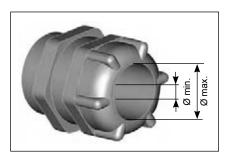
C5.2 - TABLE OF TERMINAL BOXES AND CABLE GLANDS FOR RATED SUPPLY VOLTAGE OF 400V (according to EN 50262)

Frame size	Terminal box	Single-sp	eed motor	Two-spe	ed motor	Cable gland
Frame size	material	D.O.L. starting	Y∆ starting	2 windings	1 winding	for accessories: PTO/PTF/etc
56	Plastic	ISO 16	-	2 x ISO 16	ISO 16	ISO 16
63	Plastic	ISO 16	-	2 x ISO 16	ISO 16	ISO 16
71	Plastic	ISO 16	-	2 x ISO 16	ISO 16	ISO 16
80	Plastic	ISO 20	-	2 x ISO 20	ISO 20	ISO 16
90	Plastic	ISO 20	-	2 x ISO 20	ISO 20	ISO 16
100	Plastic	ISO 20*	ISO 20*	2 x ISO 20*	ISO 20*	ISO 16
112 / 132 S	Plastic	ISO 20*	ISO 20*	2 x ISO 20*	ISO 20*	ISO 16
132 M	Aluminium alloy	ISO 25	ISO 25	2 x ISO 25	ISO 25*	ISO 16
160**	Aluminium alloy	2 x ISO 25	2 x ISO 25	2 x ISO 25	2 x ISO 25	ISO 16
180**	Aluminium alloy	2 - 4p 2 x ISO 32 6 - 8p 2 x ISO 25	2 x ISO 25	2 x ISO 32	2 x ISO 32	ISO 16
200**	Aluminium alloy	2 x ISO 32	6 - 8p 2 x ISO 32 2 - 4 - 6p 2 x ISO 25	2 x ISO 40	2 x ISO 40	ISO 16
225**	Aluminium alloy	2 - 4p 2 x ISO 40 6 - 8p 2 x ISO 32	2 x ISO 32	2 x ISO 40	2 x ISO 40	ISO 16
250**	Aluminium alloy	2-4-6p 2xISO40 8p 2xISO32	2 x ISO 32	2 x ISO 50	2 x ISO 50	ISO 16
280**	Aluminium alloy	2 - 4p 2 x ISO 50 6 - 8p 2 x ISO 40	2-4p 2xISO40 6-8p 2xISO32	2 x ISO 50	2 x ISO 50	ISO 16
315 SP/MP**	Aluminium alloy	2 - 4p 2 x ISO 63 6 - 8p 2 x ISO 50	2-4p 2 x ISO 50 6-8p 2 x ISO 40	2 x ISO 63	2 x ISO 63	ISO 16
315 MR**	Aluminium alloy	2 - 4p 2 x ISO 63 6p 2 x ISO 63	2-4p 2 x ISO 63 6p 2 x ISO 50	-	-	ISO 16

* As an option, ISO 20 and ISO 25 cable glands may be replaced by ISO 25 and ISO 32 respectively (to comply with standard DIN 42925). ** From 160 to 315 : the number and type of cable glands are provided for information only depending on the application.

Tightening capacity of cable glands

Time of apple gland	Tightening capacity			
Type of cable gland	Min. cable Ø (mm)	Max. cable Ø (mm)		
ISO 16	5	10		
ISO 20	9.5	15		
ISO 25	13	19		
ISO 32	15	25		
ISO 40	21	32		
ISO 50	26	38		
ISO 63	31	44		



Standard cable gland material = polyamide (brass on request).

On request, the terminal boxes can be supplied with drill holes, without cable glands.



C5 - Mains connection

C5.3 - TERMINAL BLOCKS - DIRECTION OF ROTATION

Standard motors are fitted with a block of six terminals complying with standard NFC 51 120, with the terminal markings complying with IEC 60034-8 (or NFEN 60034-8).

When the motor is running in U1, V1, W1 or 1U, 1V, 1W from a direct mains supply L1, L2, L3, it turns clockwise when viewed from the drive shaft end.

If any two of the phases are changed over, the motor will run in an anti-clockwise direction (make sure that the motor has been designed to run in both directions).

If the motor is fitted with accessories (thermal protection or space heater), these must be connected on screw dominos with labelled wires.

	Single-speed three-phase motor					
Motor type	D.O.L. sta	rting	Y / ∆ starting			
	Number of poles	Terminals	Number of poles	Terminals		
LS 56 to 71	2 - 4 - 6 - 8	M4				
LS 80 to 132 S	2 - 4 - 6 - 8	M5	2 - 4 - 6 - 8	M5		
LS 132 M to 160	2 - 4 - 6 - 8	M6	2 - 4 - 6 - 8	M6		
LS 180	2 - 4 6 - 8	M8 M6	2 - 4 - 6 - 8	M6		
LS 200	2 - 4 - 6 - 8	M8	6 - 8 2 - 4 - 6	M8 M6		
LS 225	2 - 4 6 - 8	M10 M8	2 - 4 - 6 - 8	M8		
LS 250	2 - 4 - 6 8	M10 M8	2 - 4 - 6 - 8	M10 M8		
LS 280	2 - 4 6 - 8	M12 M10	2 - 4 6 - 8	M10 M8		
LS 315	2 - 4 6 - 8	M16 M12	2 - 4 6 - 8	M12 M10		

Tightening torque for the nuts on the terminal blocks.

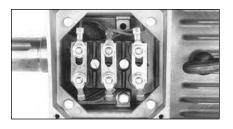
Terminal	M4	M5	M6	M8	M10	M12	M16
Torque N.m	2	3.2	5	10	20	35	65

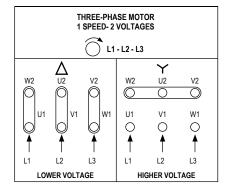
C5.4 - WIRING DIAGRAMS

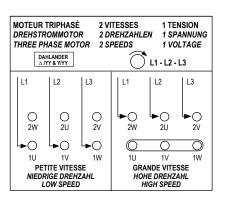
All standard motors are supplied with a wiring diagram in the terminal box.

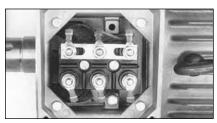
The diagrams normally used are shown opposite.

On the following pages are outline diagrams with internal and external connections.









C5.5 - EARTH TERMINAL*

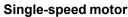
This is situated inside the terminal box. It is a threaded stud with a hexagonal nut (and a terminal washer for frame sizes \leq 132) or a TORX T25 recessed head screw (for motors LS 56, 63 and 71), and will take cables with cross-sections at least as large as the cross-section of the phase conductors.

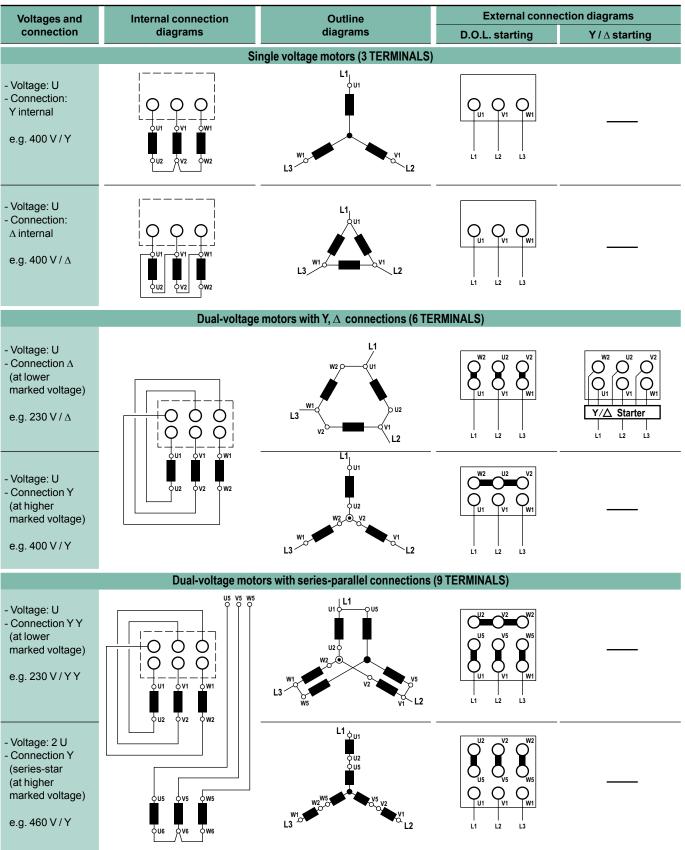
It is indicated by the sign: $\underline{-}$ in the terminal box moulding.

On request, a second earth terminal can be fitted on one of the feet or on one of the cooling fins.



C6 - Motor connections

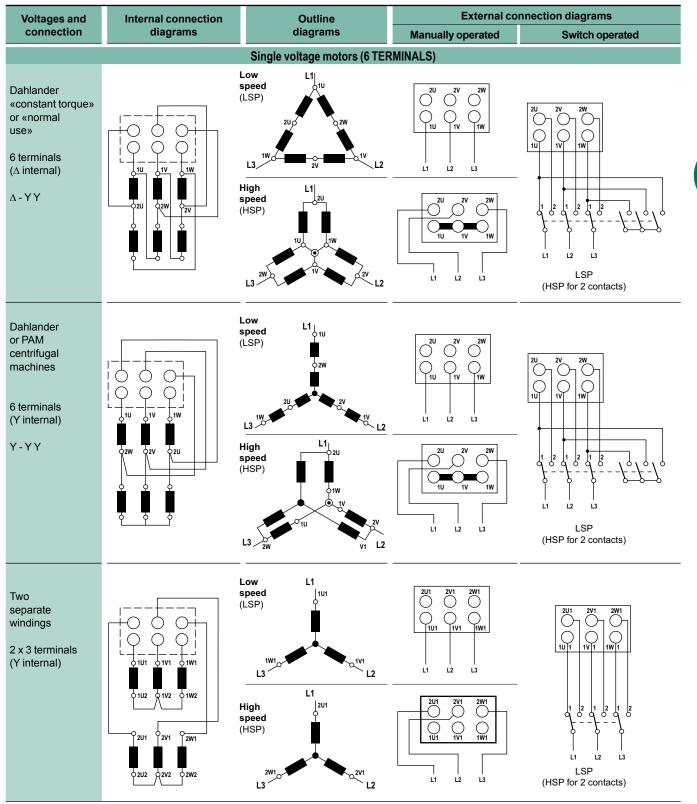






C6 - Motor connections

Two-speed motors

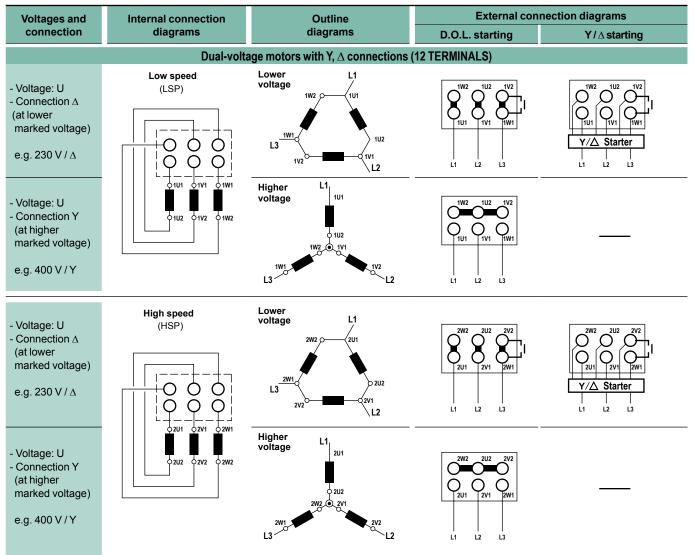


Note: the standardized markings appear on the cables coming from the stator windings.



C6 - Motor connections

Two-speed motors



It is advisable to open the unused circuit (for the speed not in use) to avoid induced currents.

0 : safety switch open when machine runs at the second speed.



D1 - Duty cycle - Definitions

Typical duty cycles (according to IEC 60034-1)

The typical duty cycles are described below: 1 - Continuous duty - Type S1

Operation at constant load of sufficient duration for thermal equilibrium to be reached (see figure 1).

2 - Short-time duty - Type S2

Operation at constant load during a given time, less than that required for thermal equilibrium to be reached, followed by a rest and de-energized period of sufficient duration to re-establish machine temperatures within 2 K of the coolant (see figure 2).

3 - Intermittent periodic duty - Type S3

A sequence of identical duty cycles, each consisting of a period of operation at constant load and a rest and de-energized period (see figure 3). Here, the cycle is such that the starting current does not significantly affect the temperature rise (see figure 3).

4 - Intermittent periodic duty with starting - Type S4

A sequence of identical duty cycles, each consisting of a significant starting period, a period of operation at constant load and a rest and de-energized period (see figure 4).

5 - Intermittent periodic duty with electrical braking - Type S5

A sequence of periodic duty cycles, each consisting of a starting period, a period of operation at constant load, a period of rapid electrical braking and a rest and de-energized period (see figure 5).

6 - Periodic continuous duty with intermittent load - Type S6

A sequence of identical duty cycles, each consisting of a period of operation at constant load and a period of operation at no load. There is no rest and de-energized period (see figure 6).

7 - Periodic continuous duty with electrical braking - Type S7

A sequence of identical duty cycles, each consisting of a starting period, a period of operation at constant load and a period of electrical braking. There is no rest and deenergized period (see figure 7).

8 - Periodic continuous duty with related changes of load and speed - Type S8

A sequence of identical duty cycles, each consisting of a period of operation at constant load corresponding to a predetermined rotation speed, followed by one or more periods of operation at other constant loads corresponding to different rotation speeds (in induction motors, this can be done by changing the number of poles). There is no rest and deenergized period (see figure 8).

9 - Duty with non-periodic variations in load and speed - Type S9

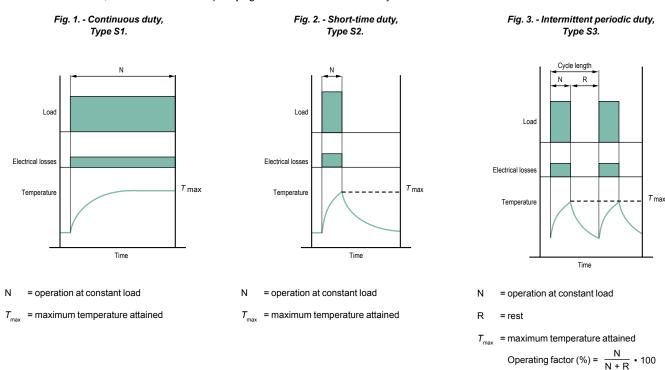
This is a duty in which the load and speed generally vary non-periodically within the permissible operating range. This duty frequently includes applied overloads which may be much higher than the full load or loads (see figure 9).

Note - For this type of duty, the appropriate full load values must be used as the basis for calculating overload.

10 - Operation at discrete constant loads - Type S10

This duty consists of a maximum of 4 discrete load values (or equivalent loads), each value being applied for sufficient time for the machine to reach thermal equilibrium. The minimum load during a load cycle may be zero (no-load operation or rest and deenergized period) (see figure 10).

Note: In section D4.6, there is a method for specifying machines in intermittent duty.





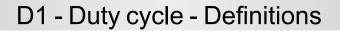
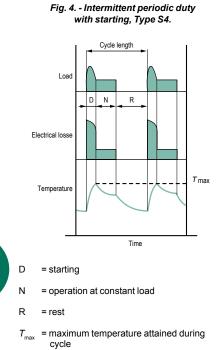
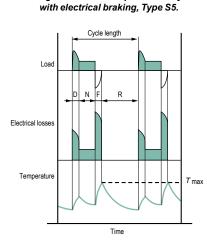


Fig. 5. - Intermittent periodic duty



Operating factor (%) = $\frac{D + N}{N + R + D} \cdot 100$

Fig. 7. - Periodic continuous duty with electrical braking, Type S7.



- D = starting
- N = operation at constant load
 - = electrical braking
- R = rest

F

 $T_{\rm max}$ = maximum temperature attained during cycle

Operating factor (%) = $\frac{D + N + F}{D + N + F + R} \cdot 100$

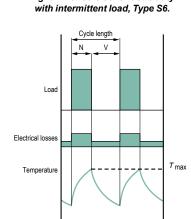
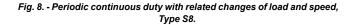


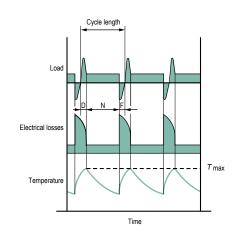
Fig. 6. - Periodic continuous duty

- N = operation at constant load
- V = no-load operation
- $T_{\rm max}$ = maximum temperature attained during cycle

Time

Operating factor (%) = $\frac{N}{N+V} \cdot 100$

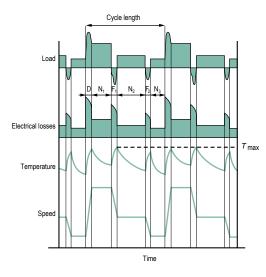




D = starting

- N = operation at constant load
- F = electrical braking
- $T_{\rm max}$ = maximum temperature attained during cycle

Operating factor = 1



F1F2 = electrical braking

D = starting

N1N2N3 = operation at constant loads.

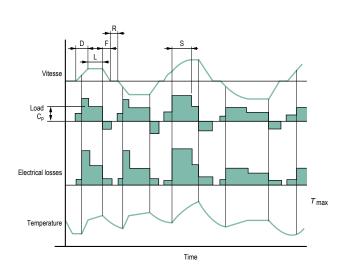
T_{max} = maximum temperature attained during cycle

 $\begin{array}{rl} \text{Operating factor} = & \frac{D+N_1}{D+N_1+F_1+N_2+F_2+N_3} & 100 \ \% \\ \\ & \frac{F_1+N_2}{D+N_1+F_1+N_2+F_2+N_3} & 100 \ \% \\ \\ & \frac{F_2+N_3}{D+N_1+F_1+N_2+F_2+N_3} & 100 \ \% \end{array}$



D1 - Duty cycle - Definitions

Fig. 9. - Duty with non-periodic variations in load and speed, Type S9.



D

L

F

R

S

C_D

 $T_{\rm max}$

= starting

= rest

= full load

= operation at variable loads

= electrical braking

= operation at overload

= maximum temperature attained.

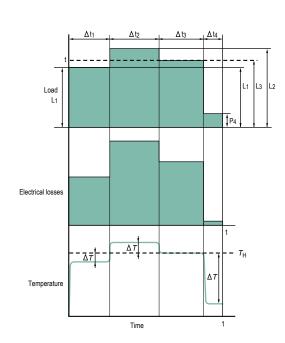


Fig. 10 - Duty at discrete constant loads, Type S10.

D

- L = load
- N = power rating for duty type S1
- p = p / $\frac{L}{N}$ = reduced load
- t = time
- $T_{_{D}}$ = total cycle time
- t_i = discrete period within a cycle
- $\Delta t_i = t_i / T_p$ = relative duration of period within a cycle
- Pu = electrical losses
- H_N = temperature at rated power for duty type S1
- ΔH_i = increase or decrease in temperature rise at the ith period of a cycle

Power is determined according to duty cycle. See section D4.6.



D2 - Supply voltage

D2.1 - REGULATIONS AND STANDARDS

The statement by the electricity consultative committee dated 25th June 1982, and the 6th edition (1983) of publication No. 38 of the International Electrotechnical Committee (IEC) have laid down time scales for the harmonisation of standard voltages in Europe.

Since 1998, voltages at the point of delivery have to be maintained between the following extreme values:

- Single-phase current: 207 to 244 V
- Three-phase current: 358 to 423 V

The IEC 60038 standard gives the European reference voltage as 230 / 400 V three-phase and 230 V single-phase, with a tolerance of +6% to -10% until 2003 and ±10% from then on.

The tolerances usually permitted for power supply sources are indicated below:

• Maximum line drop between customer delivery point and customer usage point: 4%.

• Variation in frequency around nominal frequency:

- continuous state : ±1%
- transient state : ±2%
- Three-phase mains phase-balance error:

 zero-sequence component and/or negative phase sequence component compared to positive phase sequence component: < 2%
 Harmonics:

- relative harmonic content: <10%

- individual harmonic voltages: to be established

Surges and transient power cuts: to be established

The motors in this catalogue are designed for use on the European power supply of 230 / 400 V \pm 10% - 50 Hz.

This means that the same motor can operate on the following existing supplies: - 220 / 380 V \pm 5%

- 230 / 400 V ±5% and ±10%
- 240 / 415 V ± 5%
- 2407 415 V 1 570

and is therefore suitable for a large number of countries worldwide where for example it is possible to extend them to some 60 Hz supplies:

-265 / 460 V ± 10%

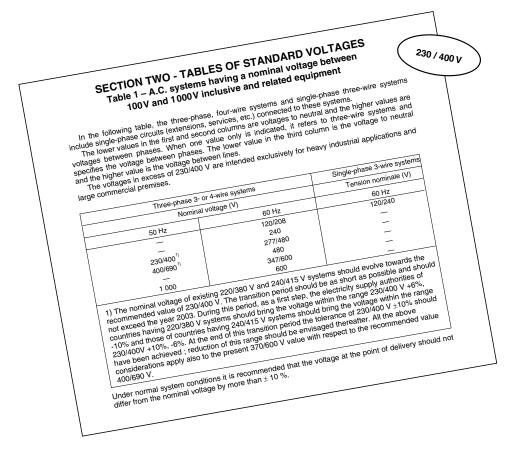
From 2008, 380 and 415 V - 50 Hz voltage supplies must be eliminated.





56

D2 - Supply voltage



D2.2 - EFFECTS ON MOTOR PERFORMANCE

D2.2.1 - Voltage range

The characteristics of motors will of course vary with a corresponding variation in voltage of $\pm 10\%$ around the rated value.

An approximation of these variations is given in the table opposite (precise values for each motor can be supplied on request).

	Voltage variation as a %							
	Un-10% Un-5% Un Un+5% Un+10%							
Torque curve	0.81	0.90	1	1.10	1.21			
Slip	1.23	1.11	1	0.91	0.83			
Rated current	1.10	1.05	1	0.98	0.98			
Rated efficiency	0.97	0.98	1	1.00	0.98			
Rated power factor (Cos ϕ)	1.03	1.02	1	0.97	0.94			
Starting current	0.90	0.95	1	1.05	1.10			
Nominal temperature rise	1.18	1.05*	1	1*	1.10			
P (Watt) no-load	0.85	0.92	1	1.12	1.25			
Q (reactive V A) no-load	0.81	0.9	1	1.1	1.21			

* According to standard IEC 60034-1, the additional temperature rise must not exceed 10 K with ±5% of UN.



D2 - Supply voltage

D2.2.2 - Simultaneous variation of voltage and frequency

Within the tolerances defined in IEC guide 106 (see section D2.1), machine input and performance are unaffected if the variations are of the same polarity and the voltage/ frequency ratio U/f remains constant.

If this is not the case, variations in performance are significant and require the machine specification to be changed.

Variation in main motor parameters (approx.) within the limits defined in IEC Guide 106.

U _{/f}	Pu	М	Ν	Cos φ	Efficiency	
Constant	Pu <mark>f</mark>	М	$N \frac{f'}{f}$	$\cos \phi \\ \text{unchanged}$	Efficiency unchanged	
Variable	$Pu\left(\frac{u'/u}{f/f'}\right)^2$	$M\left(\frac{u'/u}{f/f'}\right)^2$	$N \frac{f'}{f}$	Depends on level of saturation of machine		

M = minimum and maximum values of starting torque.

D2.2.3 - Use of 400V - 50 Hz motors on 460V - 60 Hz supplies

For a rated power at 60 Hz 20% greater than the rated power at 50 Hz, the main characteristics are modified according to the following variations, which necessitate replating of the motor:

- Efficiency increases by 0.5 - 3% - Power factor increases by 0.5 - 3%

- -Rated current decreases by 0 5%
- $-I_{\rm D}/I_{\rm N}$ increases by around 10%
- -Slip and rated torque M_N , M_D / M_N ,

adjusted.

changed and become:

 $M_{\rm M}/M_{\rm N}$ remain more or less constant

VERY IMPORTANT NOTE:

The motors defined in this catalogue which can be used with a 60 Hz supply, will NOT CONFORM with CSA or UL standards. To conform with these standards, a different type of construction is needed.

D2.2.4 - Use on supplies with U' voltages different from the voltages in the characteristics tables

D2.2.5 - Phase voltage imbalance

The phase imbalance for voltage is calculated as follows:

e = 100 x	maximum difference in voltage compared to average voltage value
	average voltage value

% voltage Imbalance

The effect on motor performance is summarized in the table opposite.

If this imbalance is known before the motor is purchased, it is advisable, in order to

D2.2.6 - Phase current imbalance

Voltage imbalances induce current imbalances. Natural lack of symmetry due to manufacture also induces current imbalances.

The chart opposite shows the ratios in which the negative phase component is equal to 5% (and 3%) of the positive phase components in three-phase current supplies without zero components (neutral absent or not connected).

Inside the curve, the negative phase component is lower than 5% (and 3%).

establish the type of motor required, to apply the derating specified in standard IEC 60892, illustrated on the graph opposite.

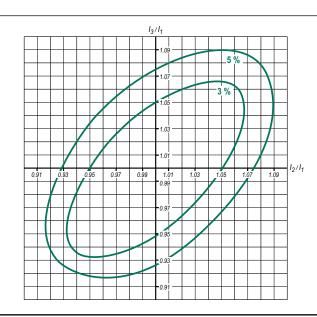
In this case, the machine windings should be

As a result, only the current values will be

5
5
07.5
25
1.28









D3 - Insulation class - Temperature rise and thermal reserve

Insulation class

The machines in this catalogue have been designed with a class ${\sf F}$ insulation system for the windings.

Class F allows for temperature rises of 105 K (measured by the resistance variation method) and maximum temperatures at the hot spots in the machine of 155 $^{\circ}$ C (Ref. IEC 60085 and IEC 60034-1).

Complete impregnation with tropicalized varnish of thermal class 180°C gives protection against attacks from the environment, such as: 90% relative humidity, interference, etc.

For special constructions, the winding is class H and impregnated with special varnishes which enable it to operate in conditions of high temperatures with relative air humidity of up to 100%.

Temperature rise (ΔT^*) and maximum temperatures at hot spots (T_{max}) for insulation classes (IEC 60034 - 1).

	∆ 7 *	T _{max}
Class B	80 K	130°C
Class F	105 K	155°C
Class H	125 K	180°C

 * Measured using the winding resistance variation method.

The insulation of the windings is monitored in two ways:

a - Dielectric inspection which involves checking the leakage current, at an applied voltage of (2U + 1000) V, in conditions complying with standard IEC 60034-1 (systematic test).

b - Monitoring the insulation resistance between the windings and between the windings and the earth (sampling test) at a D.C. voltage of 500V or 1000V.

Temperature rise and thermal reserve

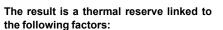
LEROY-SOMER motors are built to have a maximum winding temperature rise of 80 K under normal operating conditions (ambient temperature 40 °C, altitude below 1000 m, rated voltage and frequency, rated load).

Running at the voltage limit (± 10% of $U_{_N}$) will induce overheating of less than 15 K.

In IEC 60034-1 and 60034-2, temperature rise $(\Delta\theta)$ is calculated using the winding resistance variation method, with the formula:

$$\Delta T = \frac{R_2 - R_1}{R_1} (235 + T_1) + (T_1 - T_2)$$

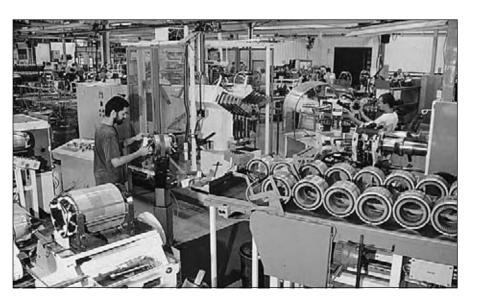
- R_1 : cold resistance measured at ambient temperature T_1
- R₂: stabilized hot resistance measured at ambient temperature T₂
- 235 : coefficient for a copper winding (for an aluminium winding, the coefficient is 225)



• a difference of 25 K between the nominal temperature rise (Un, fn, Pn) and the permissible temperature rise (105 K) for class F insulation.

• a difference of over 20 K at the voltage limits (Un \pm 10%) between the actual temperature rise and the permissible temperature rise.







D4 - Power - Torque - Efficiency - Power Factor (Cosφ)

D4.1 - DEFINITIONS

The output power (Pu) at the motor shaft is linked to the torque (M) by the equation:

Pu = M.ω

where Pu is in W, M is in N.m, ω is in rad/s and where ω is expressed as a function of the speed of rotation in min⁻¹ by the equation: $\omega = 2\pi$.N/60

The active power (P) drawn from the mains is expressed as a function of the apparent

power (S) and the reactive power (Q) by the equation:

$$S = \sqrt{P^2 + Q^2}$$

(S in VA, P in W and Q in VAR)

The power P is linked to the output power Pu by the equation:

 $P = \frac{Pu}{P}$

where η is the efficiency of the machine.

The output power Pu at the motor shaft is expressed as a function of the phase-to-phase mains voltage (U in Volts), of the line current absorbed (I in Amps) by the equation:

Pu = U.I. $\sqrt{3} \cdot \cos \varphi \cdot \eta$

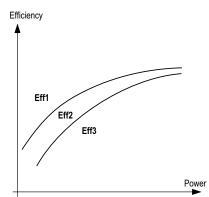
where $\mbox{cos} \phi$ is the power factor found from the ratio:

$$\cos\varphi = \frac{P}{S}$$

D4.2 - EFFICIENCY

In accordance with the agreements signed at the RIO and BUENOS AIRES INTERNATIONAL CONFERENCES, the new generation of motors with aluminium or cast iron frame has been designed to improve efficiency by reducing atmospheric pollution (carbon dioxide).

The improvement in efficiency of low voltage industrial motors (representing around 50% of installed power in industry) has had a large impact on energy consumption.



3 levels of efficiency Eff. 1-2-3 have been defined in a European agreement for 2 and 4-pole motors from 1.1 to 90 kW and this catalogue presents the reference range of LS Eff 2 motors.

Level Eff 3 in version LS is gradually being phased out of the LEROY-SOMER offer. The Eff 1 level range is available on request.

The European recommendation for measuring efficiency recommends testing using the separate losses method (in accordance with IEC 60034-2) on motors not fitted with bearing seals.



The advantages of improvement in efficiency:

Motor characteristics	Effects on the motor	Customer benefits
Increase in efficiency and in power factor.	Increase in specific output power.	Lower operating costs. Longer service life (x2 or 3). Better return on investment.
Noise reduction.		Improved working conditions.
Vibration reduction.		Quiet operation and longer service life of driven controls.
Temperature reduction.	Longer service life of fragile components (insulation system components, greased bearings).	Reduction in operating incidents and reduced maintenance costs.
	Increase in the capacity of instantaneous or extended overloads.	Wider field of applications (voltages, altitude, ambient temperature, etc).

D4.3 - INFLUENCE OF LOAD ON η AND POWER FACTOR COS ϕ See the selection data in section E.

Overrating motors in a number of applications causes them to operate at about 3/4 load, resulting in optimum motor efficiency.



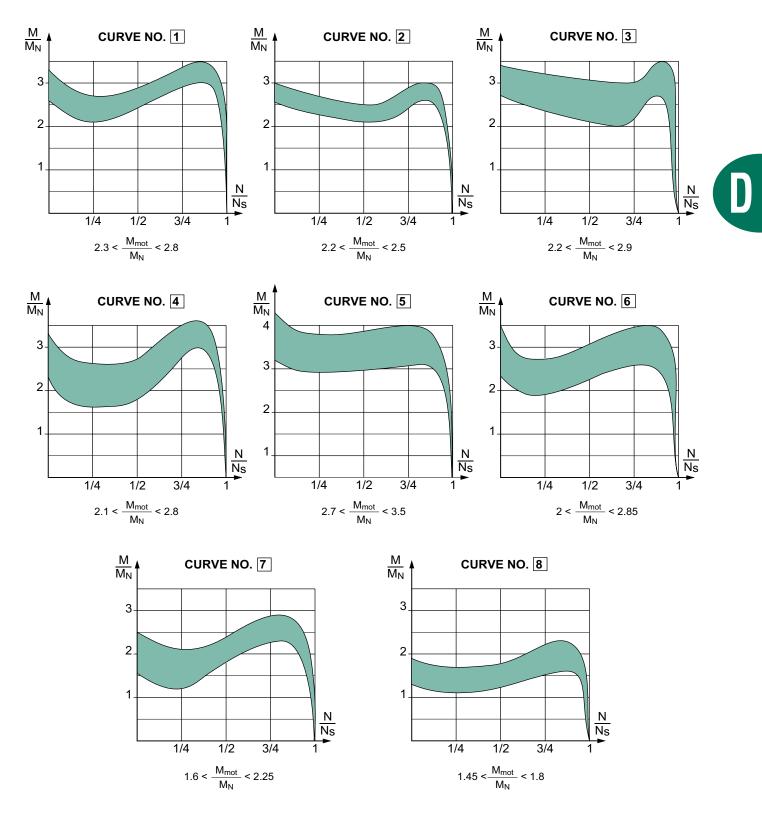
D4 - Power - Torque - Efficiency - Power Factor (Cosφ)

D4.4 - TORQUE-SPEED CHARACTERISTICS

Below are torque/speed curves that correspond to a range of typical cases (different sizes of motor, no. of poles, etc). M_{mot} is the average starting torque of the motor.

To find the accelerating torque, subtract the average load resistive torque from the average starting torque of the motor.

The curve numbers refer back to the electromagnetic characteristic selection tables in section E.





D4 - Power - Torque - Efficiency - Power Factor (Cosφ)

D4.5 - CALCULATION OF ACCELERATING TORQUE AND STARTING TIME

Acceleration time can be calculated using a simplified formula:

$$t_d = \frac{\pi}{30} \frac{N \cdot J_N}{M_a}$$
, where z

 $t_{\rm a}$: is the acceleration time in seconds $J_{\rm N}$ = moment of inertia in kg.m² of the motor plus the load corrected, if necessary, to the speed of the shaft that develops the torque $M_{\rm a}$

N: speed to be achieved in min-1

 M_a or M_{acc} = the average accelerating torque in N.m (average torque developed by the motor during starting, reduced by the average resistive torque during the same period). In general, for centrifugal machines, a very good approximation can be written as follows:

Here again is the formula by which the

moment of inertia of the driven machine

turning at speed N' is equalized with the

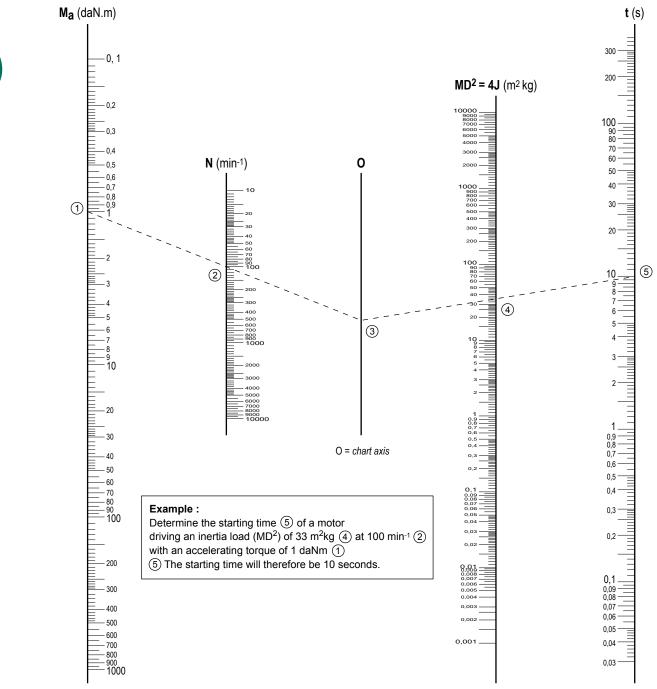
 $\mathbf{J}_{\mathbf{N}} = \mathbf{J}_{\mathbf{N}'} \cdot \left(\frac{\mathbf{N}'}{\mathbf{N}}\right)^2$

speed N of the motor.

$$M_{a} = \frac{M_{D} + 2M_{A} + 2M_{M} + M_{N}}{6} - M_{a}$$

The chart below may also be used:





LEROY*

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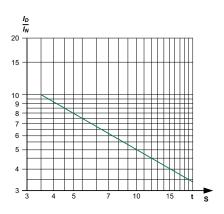
D4 - Power - Torque - Efficiency - Power Factor (Cosφ)

Starting times and locked rotor times

The starting times calculated using the chart on the previous page must remain within the limits of the graph opposite which defines maximum starting times in relation to the starting current.

The rated motor power is also defined by the equation in section D4.6.1 according to the number of (equivalent) starts per hour. Three successive cold starts and two consecutive warm starts are allowed.

Permissible motor starting time in relation to the ratio I_D/I_N for cold starts



D

The table below gives locked rotor times at full voltage (exceptional operation, e.g. incident on the transmission) for the motor when warm and when cold:

	2 p	oles	4 pc	oles	6 pc	6 poles		8 poles	
Туре	t (cold) s	t (warm) s							
LS 56	10	4	15	6	-	-	-	-	
LS 63	10	3.5	15	5	20	8	-	-	
LS 71	10	3.5	15	5	20	8	30	11	
LS 80	8	3	12	6	16	8	18	9	
LS 90	6	3	9	5	18	9	30	11	
LS 100	5	2.5	8	4	20	7	30	11	
LS 112	5	2.5	5	2.5	11	5	25	9	
LS 132	5	2.5	5	2.5	9	4	20	5	
LS 160	9	3	15	5	20	8	25	10	
LS 180	10	3.5	15	5	20	8	25	10	
LS 200	12	4	15	5	20	8	25	10	
LS 225	12	4	16	5	20	8	25	10	
LS 250	13	4.5	17	6	20	8	25	10	
LS 280	15	5	18	6	20	8	25	10	
LS 315	15	5	18	6	20	8	25	10	



D4 - Power - Torque - Efficiency - Power Factor (Cosφ)

D4.6 - RATED POWER PN IN **RELATION TO DUTY CYCLE**

D4.6.1 - General rules for standard motors

 $P_{n} = \sqrt{\frac{n + t_{d} \times [I_{D}/I_{n} \times P]^{2} + (3600 - n \times t_{d})P^{2}u \times fdm}$ 3600

Iterative calculation where:

t _d (s)	starting	time	of	motor	with
	power P(w)			
n	number of	of (eauiv	alent) starts	

- number of (equivalent) starts per hour
- OF operating factor (decimal)
- $I_{\rm D}/I_{\rm n}$ starting current of motor with
- power P P., (w) output power of motor
- during the duty cycle using OF (in decimal), operating factor rated power of motor P (w)
 - selected for the calculation

Note: n and OF are defined in section D4.6.2

Sp = specification

S1	OF = 1; n ≤ 6						
S2	; n = 1 length of operation determined by Sp						
S3	OF according ; n ~ 0 (temperature rise not to Sp affected by starting)						
S4	OF according ; n according to Sp; t _o , P _u , to Sp P according to Sp (replace n with 4n in the above formula)						
S5	OF according ; n = n starts to Sp + 3 n brakings = 4 n; $t_a P_a$, P acc. to Sp (replace n with 4n in the above formula)						
S6	$P = \sqrt{\frac{\Sigma(P^2_i \cdot t_i)}{\Sigma t_i}}$						
S7	same formula as S5 but OF = 1						
S8	at high speed, same formula as S1 at low speed, same formula as S5						
S9	S8 duty formula after complete description of cycle with OF on each speed						
S10	same formula as S6						
In ad	ddition, see the warning regarding						

precautions to be taken. Variations in voltage and/or frequency greater than standard should also be taken into account. The application should also be taken into account (general at constant torque, centrifugal at quadratic torque etc).

D4.6.2 - Determination of the power in intermittent duty cycles for adapted motors

rms power in intermittent duty

This is the rated power absorbed by the driven machine, usually defined by the manufacturer.

If the power absorbed by the machine varies during a cycle, the rms power P is calculated using the equation:

$$\mathsf{P} = \sqrt{\frac{\sum_{i=1}^{n} (\mathsf{P}_{i}^{2} \cdot t_{i})}{\sum_{i=1}^{n} t_{i}}} = \sqrt{\frac{\mathsf{P}_{1}^{2} \cdot t_{1} + \mathsf{P}_{2}^{2} \cdot t_{2}^{\dots} + \mathsf{P}_{n}^{2} \cdot t_{n}}{t_{1} + t_{2} + \cdots t_{n}}}$$

if, during the working time the absorbed power is:

- P₁ for period t₁
- P_2 for period t_2
- P_n for period t_n

Power values lower than 0.5 $\rm P_{_N}$ are replaced by 0.5 $\rm P_{_N}$ in the calculation of rms power P (no-load operation is a special case).

Additionally, it is also necessary to check that for a particular motor of power P_N . • the actual starting time is at most equal to 5

seconds

· the maximum output of the cycle does not exceed twice the rated output power P

· there is still sufficient accelerating torque during the starting period

Load factor (LF)

Expressed as a percentage, this is the ratio of the period of operating time with a load during the cycle to the total duration of the cycle where the motor is energized.

Operating factor (OF)

Expressed as a percentage, this is the ratio of the motor power-up time during the cycle to the total cycle time, provided that the total cycle time is less than 10 minutes.

Starting class

Class: $n = n_D + k.n_F + k'.n_I$

 $n_{\rm p}$ is the number of complete starts per hour n_r is the number of times electrical braking is applied per hour

«Electrical braking» means any braking directly involving the stator winding or the rotor winding:

 Regenerative braking (with frequency controller, multipole motor, etc)

Reverse-current braking (the most commonly used)

· D.C. injection braking

ni is the number of impulses (incomplete starts up to one-third of maximum speed) per hour

k and k' are constants determined as follows:

	k	k'
Cage induction motors	3	0.5

- Reversing the direction of rotation involves braking (usually electrical) and starting.

Braking with LEROY-SOMER electromechanical brakes, as with any other brakes that are independent of the motor, does not constitute electrical braking in the sense described above.

Calculating derating

- Input criteria (load)
- rms power during the cycle = P
- Moment of inertia corrected
- to speed of motor = Je
- Operating factor = OF
- Class of starts per hour = n - Resistive torque during starting = Mr

- · Selection in catalogue
- Motor power rating P_N
- Starting current I, cosφ - Moment of inertia of rotor J.
- Average starting torque M
- Efficiency at $P_N(\eta_{PN})$ and at $P(\eta_P)$

Calculations - Starting time:

$$t_{\rm r} = \frac{\pi}{2} \cdot N \cdot \frac{(J_{\rm e} + J_{\rm r})}{(J_{\rm e} + J_{\rm r})}$$

$$t_d = \frac{1}{30} \cdot N \cdot \frac{1}{M_{mot} - M_r}$$

- Cumulative starting time per hour:

nx t

- Energy to be dissipated per hour during starts = sum of the energy dissipated in the rotor (= inertia acceleration energy) and the energy dissipated in the stator during the cumulative starting time per hour:

$$\mathsf{E}_{\mathsf{d}} = \frac{1}{2} (\mathsf{J}_{\mathsf{e}} + \mathsf{J}_{\mathsf{r}}) \left(\frac{\pi \cdot \mathsf{N}}{30}\right)^2 \mathsf{x} \mathsf{n} + \mathsf{n} \mathsf{x} \mathsf{t}_{\mathsf{d}} \sqrt{3} \mathsf{U} \mathsf{I}_{\mathsf{d}} \mathsf{cos} \varphi_{\mathsf{d}}$$

- Energy to be dissipated during operation

 $E_f = P. (1 - \eta_p) . [(OF) x 3600 - n x t_d]$ - Energy that the motor can dissipate at rated power with the Operating Factor for

Intermittent Duty.

 $E_m = (OF) 3600 \cdot P_N \cdot (1 - \eta_{PN})$ (The heat dissipated when the motor is at rest can be ignored).

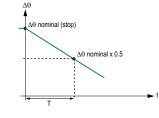
Dimensioning is correct if the following relationship is verified =

$$E_m \ge E_{d+}E_f$$

If the sum of $E_d + E_f$ is lower than 0.75 E_m , check whether a motor with the next lowest power would be more suitable.

D4.6.3 - Equivalent thermal constant

The equivalent thermal constant enables the machine cooling time to be predetermined.



Thermal constant = $\frac{T}{\ln 2}$ = 1.44 T

Cooling curve $\Delta \theta = f(t)$

where $\Delta \theta$ = temperature rise in S1 duty

- T = time required for nomina
 - temperature rise to reach half its value
 - t = time
 - In = natural logarithm

D4.6.4 - Transient overload after operating in type S1 duty cycle

At rated voltage and frequency, the motors can withstand an overload of:

- 1.20 for an OF = 50%
- 1.40 for an OF = 10%

However, it is necessary to ensure that the maximum torque is much greater than 1.5 times the rated torgue corresponding to the overload.



D4 - Power - Torque - Efficiency - Power Factor (Cosφ)

D4.7 - OPERATION OF A 3-PHASE MOTOR FROM A SINGLE-PHASE POWER SUPPLY (STEINMETZ CONNECTION)

It is possible to run three-phase motors from a single-phase power supply under certain conditions:

- a low-power (ie. low kW) motor, wound for 230/400 V 50 Hz
- single-phase supply 220/230 V 50 Hz
- derated for power
- loss of thermal reserve

- starting torque approx. 1.5 times the rated torque

Only 4-pole motors have suitable characteristics (starting current, power factor and efficiency, both for the supply and the machine lifetime).

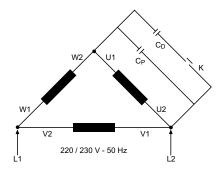
Please consult Leroy-Somer about machines for other speeds.



Table of characteristics

Motor type	P _{3-ph} kW	P _{1-ph} kW	C _D μ F - 150V	C թ μ F - 220V	Efficiency %	Cos φ	ا amp for 230V	Ι _D amp for 230V
LS 80 L	0.55	0.37	120	30	80	0.91	2.2	11.5
LS 80 L	0.75	0.55	225	32	80	0.91	3.3	18
LS 90 L	1.1	0.75	300	47	79	0.99	4.2	25
LS 90 L	1.5	1.1	500	75	81	0.97	6.1	38
LS 100 L	2.2	1.5	560	90	80	0.98	8.3	45
LS 100 L	3	2.2	650	140	80	0.98	12.2	60
LS 112 M	4	3	1100	250	83	0.92	17	90

Circuit diagram

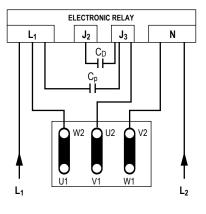


Cp : permanent capacitor

CD : starting capacitor

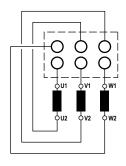
K : circuit breaker relay contact for starting capacitors

External wiring diagram



Note: to change the direction of rotation, connect W_2 to N V_2 to L₁

Internal wiring diagram





D5 - Speed of rotation

D5.1 - SINGLE FIXED SPEED MOTOR

The great majority of applications only require a single fixed speed. If this applies to you, you should opt for a 1500 min⁻¹ or possibly 3000 min⁻¹ motor (50 Hz supply) which are the ones most frequently used.

However, even with fixed speeds there are two types of application which fall outside the standard speed range of 750 to 3000 min⁻¹.

D5.1.1 - High speed motor

High speed motors, operating at speeds of over 3000 min⁻¹, obtained by using supplies with fixed frequencies other than 50 Hz, for example 100, 200 or 400 Hz: the motor will run at a synchronous speed N such that:

 $N = \frac{120}{p} \cdot f$

(N is in min⁻¹; f is the frequency of the supply in Hz; p is the number of motor poles). Motors of this type have to be specially designed, taking into account the following important points:

- the wave form of the high frequency supply (type of harmonics and total harmonic distortion)

- increased magnetic losses in relation to frequency and harmonics
- mechanical properties of rotors

- bearing properties, lubrication, lifetime, temperature rises, reduced currents

- ventilation, noise levels, vibrations

- starting current, motor torque, load inertia

It should also be noted that high speed applications are limited to smaller machines: the higher the speed, the smaller the machine must be.

D5.1.2 - Low speed motor

Low speed motors, running at under 750 min⁻¹. Low speeds are obtained either by using a supply with a fixed frequency of under 50 Hz, or by using more than 8 poles with a 50 Hz supply. Motors of this type also have to be specially designed to deal with the problems involved in this type of application, such as:

- resistive torque and driven inertia

and in the manufacture:

- ventilation

The most widely used fixed frequency (50 Hz) low speeds are 600 min⁻¹ (10-pole motor), 500 min⁻¹ (12-pole motor) and 375 min⁻¹ (16-pole motor).

The table below shows available power for each type of motor used in Type S1 duty, with a power supply of $U_N \pm 5\%$, and a temperature rise of 100 K for a class F construction (quadratic torque application):

Туре	10 p	12 p	16 p
LS 80 L	0.15	0.12	-
LS 90 S	0.25	0.17	0.07
LS 90 L	0.37	0.25	0.11
LS 100 L	0.5	0.37	0.17
LS 112 MG	0.9	0.75	0.25
LS 132 SM	1.1	0.9	0.5
LS 132 M	2.2	1.5	0.75
LS 160 M	4	2.2	1.1
LS 160 L	-	3	-
LS 160 LU	5.5	-	1.7
LS 180 L	7.5	4	2.2 - 3
LS 180 LU	-	5.5	-
LS 200 L	9	7.5	4
LS 200 LU	11 - 13 and 15	9	5.5
LS 225 MG	18.5	11 - 13 and 15	7.5
LS 225 MH	22	18.5	9

D5.2 - MULTIPLE FIXED SPEEDS MOTOR

Some applications require operation at two or three fixed speeds. These can be obtained by changing the poles in a multi-speed motor. There are a large number of solutions, but we shall only look at the following:

D5.2.1 - Motor with single winding

Motors with a single winding (Dahlander connection [speed ratio: 2:1]) or PAM (any speed ratio):

Internal connection of stator windings is used for specific applications:

 $\begin{array}{c} \mbox{centrifugal} \\ \mbox{applications} \end{array} \left\{ \begin{array}{c} \mbox{Dahlander } Y - Y \mbox{ or } \Delta - \Delta \\ \mbox{PAM - Y} \end{array} \right.$

other applications - Dahlander Δ - Y In general, these motors are designed for D.O.L. starting from the mains supply and are single-voltage.

The most common speed ratios are:

- 3000 / 1500 min⁻¹ (2 / 4 poles)
- 1500 / 750 min⁻¹ (4 / 8 poles)

Recommendation for using motors with PAM winding

The following precautions should be taken when connecting PAM 2-speed motors operated in parallel on a single installation to the mains supply:

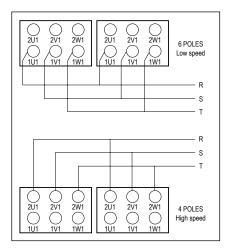
1 - All motors should be of the same construction and come from the same supplier.

2 - The sequence of the R, S, T phases of the supply should be marked.

3 - Terminals with the same name [(1U1, 1V1, 1W1), (2U1, 2V1, 2W1)] on each motor should be connected together on a single-phase.

Note: If one of the motors rotates in a different direction to the others, this motor should be returned to the factory to bring it into conformity.

Example: 2 motors with 4/6 poles operating in parallel.



D5.2.2 - Motor with separate windings

Motors with two separate windings. Different starts are obtained depending on the winding connections on the terminal block:

2 x 3 terminals: Direct-On-Line (D.O.L.) starting

2 x 6 terminals: Y I Δ starting possible

In the first case, these motors will be single-voltage; in the second, they may be either dual-voltage or ~Y / Δ starting single-voltage motors.

The most common speed ratios

are:

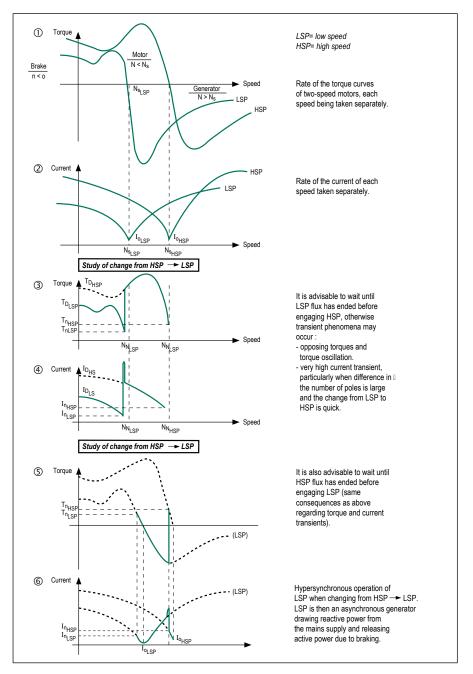
- 3000 / 750 min⁻¹ (2/ 8 poles)
- 1500 / 1000 min-1 (4/6 poles)



D5 - Speed of rotation

D5.2.3 - Behaviour of two-speed motors

Each speed of a multi-speed motor behaves like a complete motor (curves \mathbb{O} and \mathbb{O}) with operation as a brake, a motor and an asynchronous generator, depending on the quadrant.



The above curves 3 to 6 explain how the torques and currents develop when the motor changes from low speed to high speed and vice versa.

Note: The greater the difference between the number of poles, the more likelihood of:

- significant current peak at LSP

- long braking time and risk of temperature rise at LSP
- high level of hypersynchronous noise

Some of these phenomena can be aggravated if the driven inertia is high.

The rated power is determined according to the criteria in section D4.6.1 for each of the two speeds (see type S8 duty).

Manufacturers' recommendations should be followed regarding devices for connecting to the mains supply and protection, using equipment which has already been examined and for which the problems of transient current peaks have been resolved.

D5.2.4 - Operating rules

A few common sense rules need to be applied to get the best out of a two-speed motor:

- Avoid large differences in the number of poles (for example 2/12p, 2/16p, 4/20p, etc): the torque drop at high speed occurs at a speed greater than the synchronous speed at low speed. The motor may start to «crawl» and never reach its higher speed rating.

- It is better to start the motor at the lower speed: this effectively eliminates the high speed torque drop, thus reducing the starting time. It will also limit current surge.

- As well as taking the precaution advised in the previous paragraph, current surge can be limited using the advice given in section D8 on «starting». Do bear in mind, though, that not all two-speed motors can be started using the suggested types of starting.

- An important precaution for motors with two separate windings, if the normal connection is a delta, is to "open" the delta for the speed not in use to avoid inducing circulating currents which can create opposing torques and harmful temperature rises.

D5.2.5 - 2-speed motors with connected windings

For ventilation applications, we manufacture 2-speed motors by connecting the windings on a single-speed motor:

- High speed by delta connection at full voltage.

- Low speed by star connection at full voltage.

The second speed is obtained because the motor is seriously desaturated (voltage divided by 1.732 at the phase terminals) and the rotor is experiencing a great deal of slip: as a result, there is a significant rotor temperature rise – since all the Joule losses due to the slip are dissipated in it – and risks of significant overheating – by conduction – in the windings if essential derating precautions have not been taken.

In fact, equilibrium is achieved for both speed and temperature rise by means of the following principles:

- The power varies in the same way as the speed power three.

- The slip varies as a function of the output and the temperature rise.



D5 - Speed of rotation

- The choice of alloy for the rotor squirrel cage depends on the required output speeds.

When the power absorbed by the fan varies for reasons not related to the selected operating principle – for example, dirt on the fan blades, temperature of the air flow, variation of power supply frequency or voltage, etc. – the temperature rise in the rotor varies and allows speed equilibrium to be regained without making any adjustments (unless the variations exceed the maximum motor torque in the relevant connection).

The immediate consequence of these random conditions is to define the motor according to its load (driven inertia, power, speeds, etc) and to optimize the choice using real tests. The number of poles chosen for these applications should be four poles or more, and the power rating less than 7.5 kW with 4 poles. We do not offer actual motor ranges, but will undertake development work in a technical partnership.

D5.2.6 - Special cases

Motors with more than two speeds have to be specially designed, as, in the majority of cases, the precise nature of the load must be specified.

D5.3 - VARIABLE SPEEDS

Improvements in manufacturing processes have led to the introduction of variable speed control.

Two different processes can be used on motors:

- slip variation at fixed frequency

- supply frequency variation

D5.3.1 - Slip variation at fixed frequency

On a motor of a given build, slip other than the rated slip can be obtained by either increasing the load or decreasing the supply voltage.

As an increase in slip is accompanied by increased rotor losses, special rotors have now been designed for use in motors for very specific applications.

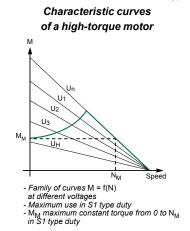
The most common application is the hightorque motor with a high-resistance rotor, used with variable voltage, providing constant torque within a specified range of speeds. These motors have to be specially designed.

The family of curves below shows the variation in motor torque in relation to the supply voltage $U_N > U_1 > U_2$, etc.

The green curve shows the maximum torque available in relation to speed for a maximum temperature rise for the insulation class in Type S1 duty (normally with forced ventilation).

The dotted curve shows the maximum constant torque available in Type S1 duty in the speed range 0 to $N_{\rm M}$.

The available powers and torques of these motors in Type S1 duty are much lower than those of standard motors of the same type.



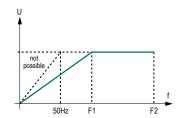
D5.3.2 - Frequency variation

In induction motors, variations of speed within a wide range are obtained using a power supply with variable frequency and voltage.

As a general rule, the frequency inverter delivers a proportional voltage and frequency up to a value F_{1} , which depends on the manufacturer, and a fixed voltage up to a maximum frequency value of F_{2} .

In these conditions, the motor output is proportional to the frequency up to the value F_1 (F_1 = frequency where the U/f ratio

changes), and then constant up to the value $\mathrm{F_{2}}$

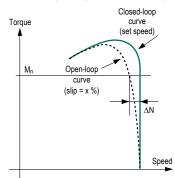


In practice, certain adjustments have to be made. At low frequency, to maintain significant torque, the inverter provides greater saturation of the motor (and thus a higher U value); the value of F1 is itself made variable so as to widen the range of use at constant torque (or at proportional power).

In addition, forced ventilation enhances motor cooling at low speeds and reduces noises levels at high speeds.

In applications where accurate speed regulation is required, the variable speed drive can be used with closed-loop feedback by fitting a speed detector (D.C. tacho, A.C. tacho or encoder)

which will send a signal to the inverter to change its U/f ratio and so regulate the speed at the level required (see curve below).



Using induction motors at high speeds (over about 4000 min⁻¹) can be risky. The cage may be damaged, bearing life impaired, as well as vibration and high-frequency saturation leading to heavy losses and significant temperature rises, etc. An in-depth mechanical and electrical design exercise is needed for all machines required to operate at speeds of over 4000 min⁻¹.

High-speed motors often need to be adapted to suit their application, and this work may include:

- fitting a speed detector (D.C. tacho, A.C. tacho or encoder)

- fitting forced ventilation
- fitting a brake or decelerator



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D5 - Speed of rotation

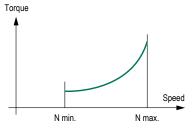
Applications and choice of solutions

There are three main types of load:

a - Centrifugal machines

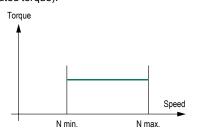
The output torque varies as the square of the

speed. The torque required for acceleration is low (about 20% of rated torque).



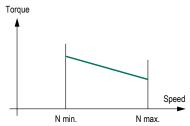
b - Constant torque applications

The output torque remains constant throughout the speed range. The torque required for acceleration may be high, depending on the machine (higher than the rated torque).



c - Constant power applications

The output torque decreases as the speed increases. The torque required for acceleration is at most equal to the rated torque.



These applications involve a choice of motordrives based on the following criteria:

- Centrifugal machines: torque or power at the maximum operating speed.

- Applications with constant torque: range of operating speeds and output torques.

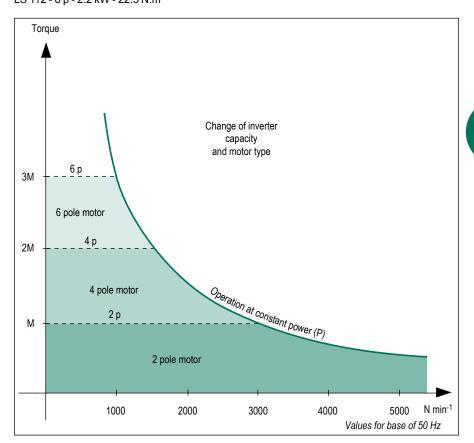
- Applications with constant power: range of operating speeds and torque at the minimum operating speed.

Choice of inverter/motor combination

The curve below expresses the output torque of a 2, 4 or 6 pole motor supplied by a drive with power P where F_1 is 50 Hz (point at which U/f ratio changes).

For a frequency inverter with power P_N operating at constant power P within a determined range of speeds, it is possible to optimize the choice of motor and its number of poles to give a maximum amount of torque.

Example 1: the UMV - 3.5 T inverter (drive) can supply the following motors: LS 90 - 2 p - 2.2 kW - 7.5 N.m LS 100 - 4 p - 2.2 kW - 15 N.m LS 112 - 6 p - 2.2 kW - 22.5 N.m



The choice of the motor and inverter combination will therefore depend on the application.







D5 - Speed of rotation

Extreme operating conditions and other points

Coupling motors

For this type of application, we strongly recommend a Y connection for the windings to reduce the effects of disconnection from the mains supply.

Transient overloads

Drives are designed to withstand transient overload peaks of 180% or overloads of 150% for 60 seconds (maximum once every ten minutes). If the overload is greater, the system will automatically shut down.

Starting torque and current

The specific U/f ratio (with Boost for frequencies lower than 25 Hz), the torque available when the motor is switched on can be adjusted to a value higher than the rated value.

Adjusting the switching frequency

This optimizes motor noise levels by adapting the wave form to the specific type of use.

Electrical protection

The system all have integrated features to protect them against: - overload (over-current)

- under-voltage and over-voltage
- short-circuit
- earth fault

Note: All the above faults are shown on an LCD screen, as are settings, speed and current ranges, etc.

Mechanical speed limits for standard motors when the frequency is varied (min⁻¹)

With increasingly extensive frequency ranges, frequency inverters can, in theory, control a motor at a higher speed than its rated speed. However, the bearings and type of balancing of the standard rotor dictate a maximum mechanical speed which cannot be exceeded without endangering the service life of the motor (please consult Leroy-Somer for each application).

Choice of motor

There are two possibilities:

a - The frequency inverter is not supplied by LEROY-SOMER

All the motors in this catalogue can be used with a frequency inverter. Depending on the application, motors will need to be derated by around 10% to maintain all the characteristics described in this catalogue.

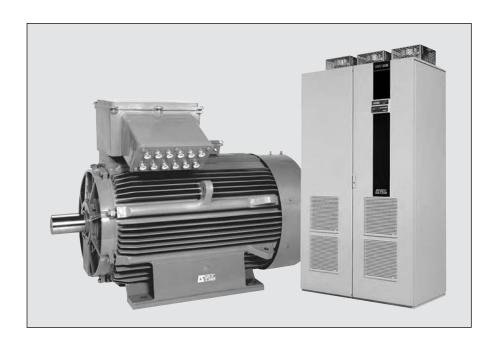
To avoid changes in frame size due to derating within the standard range, LEROY-SOMER has developed a range of adapted motors with standardized dimensions. What is more, the improved efficiency of this range means that the motors can be used with an electronic drive without derating.

b - The frequency inverter is supplied by LEROY-SOMER

LEROY-SOMER has developed a range of optimized motors together with a range of frequency inverters.

As these two ranges have been specifically designed for use in combination, excellent performance is guaranteed.

There is a special catalogue devoted to this product line (LSMV Motors).





D6 - Noise and vibration

D6.1 - MOTOR NOISE LEVELS D6.1.1 - Noise emitted by rotating machines

In a compressible medium, the mechanical vibrations of an elastic body create pressure waves which are characterized by their amplitude and frequency. The pressure waves constitute an audible noise if they have a frequency of between 16 and 16000 Hz.

Noise is measured by a microphone linked to a frequency analyser. Measurements are taken in an anechoic chamber on machines at no-load, and a sound pressure level Lp or a sound power level Lw can then be established. Measurement can also be carried out in situ on machines which may be on-load, using an acoustic intensity meter which can differentiate between sound sources and identify the sound emissions from the machine.

The concept of noise is linked to hearing. The auditory sensation is determined by integrating weighted frequency components with isosonic curves (giving a sensation of constant sound level) according to their intensity. The weighting is carried out on sound meters using filters whose bandwidth takes into account, to a certain extent, the physiology of the human ear:

Filter A: used for low and medium noise levels. High attenuation, narrow bandwidth. *Filter B:* used for very high noise levels. Wide bandwidth.

Filter C: very low attenuation over the whole of the audible frequency range.

Filter A is used most frequently for sound levels emitted by rotating machinery. It is this filter which has been used to establish the standardized characteristics. A few basic definitions:

The unit of reference is the bel, and the sub-multiple decibel dB is used here.

Sound pressure level in dB

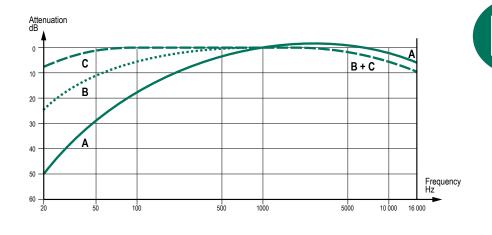
$$L_p = 20\log_{10}\left(\frac{P}{P_0}\right) \text{ avec } p_0 = 2.10^{-5} \text{ Pa}$$

Sound power level in dB

$$L_W = 10log_{10} \left(\frac{P}{P_0}\right)$$
 avec $p_0 = 10^{-12} W$

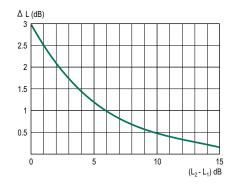
Sound intensity level in dB

$$L_{W} = 10 \log_{10} \left(\frac{l}{l_{0}} \right)$$
 avec $l_{0} = 10^{-12} \text{ W/m}^{2}$



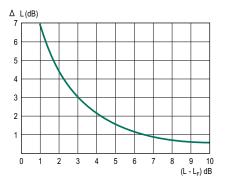
Correction of measurements

For differences of less than 10 dB between 2 sound sources or where there is background noise, corrections can be made by addition or subtraction using the rules below.



Addition of levels

If L_1 and L_2 are the separately measured levels ($L_2 \ge L_1$), the resulting sound level L_R will be obtained by the formula: $L_R = L_2 + \Delta L$ ΔL is found by using the curve above.



Subtraction of levels*

This is most commonly used to eliminate background noise from measurements taken in a «noisy" environment.

If L is the measured level and L_F the background noise level, the actual sound level L_R will be obtained by the calculation: L_p = L - Δ L

 ΔL is found by using the curve above.

*This method is the one normally used for measuring sound power and pressure levels. It is also an integral part of sound intensity measurement.



D6 - Noise and vibration

Under IEC 60034-9, the guaranteed values are given for a machine operating at noload under normal supply conditions (IEC 60034-1), in the actual operating position,

or sometimes in the direction of rotation as specified in the design.

This being the case, standardized sound power level limits are shown for the values

obtained for the machines described in this catalogue. (Measurements were taken in conformity with standard ISO 1680).

Weighted sound level [dB(A)] of motors in position IM 1001 with a 50 Hz supply

Expressed as sound power level (Lw) according to the standard, the level of sound is also shown as sound pressure level (Lp) in the table below:

		2 poles			4 poles			6 poles			8 poles	
Motor type	IEC 60034-9	LS	LS									
	Power Lw	νA	Pressure LpA	Power Lv	νA	Pressure LpA	Power Lv	/A	Pressure LpA	Power Lv	vA	Pressure LpA
LS 56 L	-	62	54	-	55	47	-	-	-	-	-	-
LS 63 M	-	65	57	-	58	49	-	57	48	-	-	-
LS 71 L	-	70	62	-	58	49	-	60	52	-	48	40
LS 80 L	81	69	61	-	55	47	-	49	41	-	49	41
LS 90 S	81	74	66	71	57	49	-	59	51	-	51	43
LS 90 L	81	74	66	71	57	49	71	59	51	-	51	43
LS 100 L	86	75	66	76	57	48	71	59	50	71	52	43
LS 112 M	86	75	66	76	58	49	71	60	51	71	58	49
LS 132 S	91	81	72	81	67	58	76	64	55	71	60	51
LS 132 M	91	81	72	81	71	62	76	64	55	76	63	54
LS 160 M	91	82	72	88	72	62	80	66	56	76	76	66
LS 160 L	94	82	72	88	72	62	80	66	56	80	76	66
LS 180 M	96	82	72	88	74	64	-	-	-	-	-	-
LS 180 L	-	-	-	91	75	64	84	71	60	80	79	68
LS 200 L	96	84	73	91	75	64	84	73	62	84	75	65
LS 225 S	98	84	73	94	75	64		-		84	75	65
LS 225 M	98	84	73	94	75	64	87	74	63	84	75	65
LS 250 M	100	87	76	94	77	66	87	76	65	89	74	63
LS 280 S	100	89	79	97	80	69	90	76	65	89	74	63
LS 280 M	100	90	79	97	80	69	90	76	65	89	74	63
LS 315 S	100	95	83	97	82	70	94	85	73	89	86	74
LS 315 M	103	95	83	101	82	70	94	86	74	92	86	74
LS 315 MR	103	95	83	101	86	74	94	86	74	-	-	-

The maximum tolerance for these values is + 3 dB(A).

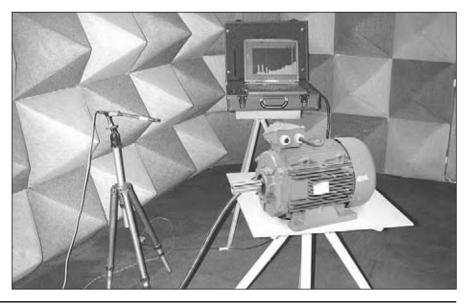
In compliance with standards IEC 60034-9 and NFEN ISO 4871, uncertainty on machine installations is established using the formula: $L_p = L + k$

where 1.5 < k < 6 dB depending on whether laboratory or control measurements are being used.

The noise levels of these motors with a 60 Hz supply with proportional voltage are increased by about 2 dB(A) with 8 poles, to about 6 dB(A) with 2 poles.

D6.1.2 - Noise levels for machines at full load

Sound power levels, when at full load, are usually higher than those when at no-load. The maximum increase at full load to be added to the declared values at no-load is between 2 and 8 dB(A). (Addition to standard IEC 60034.9).





D6 - Noise and vibration

The LS machines in this catalogue have level A, half-key balancing

D6.2 - VIBRATION LEVELS -BALANCING

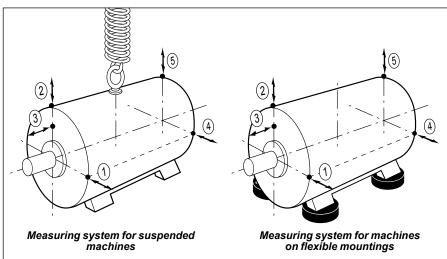
Inaccuracies due to construction (magnetic, mechanical and air-flow) lead to sinusoidal (or pseudo sinusoidal) vibrations over a wide range of frequencies. Other sources of vibration can also affect motor operation: such as poor mounting, incorrect drive coupling, end shield misalignment, etc. We shall first of all look at the vibrations emitted at the operating frequency, corresponding to an unbalanced load whose amplitude swamps all other frequencies and on which the dynamic balancing of the mass in rotation has a decisive effect.

Under standard ISO 8821, rotating machines can be balanced with or without a key or with a half-key on the shaft extension.

Standard ISO 8821 requires the balancing method to be marked on the shaft extension as follows:

- half-key balancing: letter H
- full key balancing: letter F
- no-key balancing: letter N

The machines in this catalogue have level A balancing - Level B balancing is available on request.



The measurement points quoted in the standards are the ones indicated in the drawings above.

At each point, the results should be lower than those given in the tables below for each balancing class and only the highest value is to be taken as the « vibration level».

Measured parameters

The vibration speed can be chosen as the variable to be measured. This is the speed at which the machine moves either side of its static position. It is measured in mm/s.

As the vibratory movements are complex and non-harmonic, it is the quadratic average (rms value) of the speed of vibration which is used to express the vibration level.

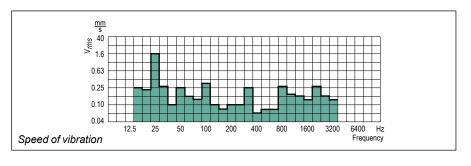
Other variables that could also be measured are the vibratory displacement amplitude (in μm) or vibratory acceleration (in m/s²).

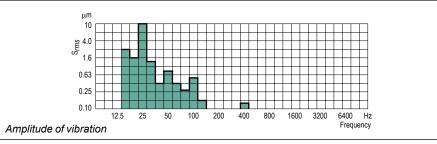
If the vibratory displacement is measured against frequency, the measured value decreases with the frequency: highfrequency vibrations are not taken into account.

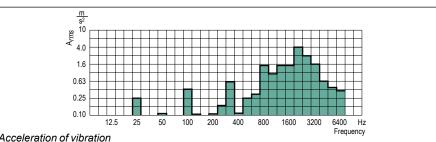
If the vibratory acceleration is measured, the with measured value increases the low-frequency vibrations frequency: (unbalanced loads) cannot be measured.

The rms speed of vibration is the variable chosen by the standards.

However, if preferred, the table of vibration amplitudes may still be used (for measuring sinusoidal and similar vibrations).







Acceleration of vibration



D6 - Noise and vibration

MAXIMUM VIBRATION MAGNITUDE LIMITS, FOR DISPLACEMENT, SPEED AND ACCELERATION IN RMS VALUES FOR FRAME SIZE H (IEC 60034-14)

Vibration level	Frame size <i>H</i> (mm)								
	56 < <i>H</i> ≤ 132			132 < <i>H</i> ≤ 280			H > 280		
	Displa- cement µm	Speed mm/s	Accelera- tion m/s ²	Displa- cement µm	Speed mm/s	Accelera- tion m/s ²	Displa- cement µm	Speed mm/s	Accelera- tion m/s ²
Α	25	1.6	2.5	35	2.2	3.5	45	2.8	4.4
В	11	0.7	1.1	18	1.1	1.7	29	1.8	2.8

For large machines and special requirements with regard to vibration, balancing can be carried out in situ (finished assembly).

Prior consultation is essential, as the machine dimensions may be modified by the addition to the drive ends of the balancing disks required in this situation.





D7 - Performance

D7.1 - THERMAL PROTECTION

Motors are protected by a manual or automatic overcurrent relay, placed between the isolating switch and the motor. This relay may in turn be protected by fuses. These protection devices provide total protection of the motor against non-transient overloads. If a shorter reaction time is required, or if you want to detect transient overloads, or to monitor temperature rises at «hot spots» in the motor or at strategic points in the installation for maintenance purposes, it would be advisable to install heat sensors.

The various types are shown in the table below, with a description of each. It must be emphasized that sensors cannot be used to carry out direct adjustments to the motor operating cycles.

Туре	Symbol	Operating principle	Operating curve	Cut-off (A)	Protection provided	Mounting Number of devices*
Normally closed thermostat	РТО	bimetallic strip, indirectly heated, with normally closed (NC) contact		2.5A at 250V with cos $\phi0.4$	general surveillance for non-transient overloads	2 or 3 in series
Normally open thermostat	PTF	bimetallic strip, indirectly heated, with normally open (NO) contact	F NRT	2.5 A at 250 V with cos φ 0.4	general surveillance for non-transient overloads	2 or 3 in parallel
Positive temperature coefficient thermistor	PTC	Variable non-linear resistor with indirect heating		0	general surveillance for transient overloads	3 in series
Thermocouples	T (T < 150 °C) Copper Constantan K (T < 1000 °C) Copper Copper-Nickel	Peltier effect		0	continuous surveillance at hot spots	1 per hot spot
Platinum resistance thermometer	PT 100	Variable linear resistor with indirect heating	R	0	high accuracy continuous surveillance at key hot spots	1 per hot spot

Built-in indirect thermal protection

- NRT : nominal running temperature.

- The NRTs are chosen according to the position of the sensor in the motor and the temperature rise class.

* The number of devices relates to the winding protection.

Fitting thermal protection

- PTO or PTF, in the control circuits

PTC, with relay, in the control circuits
 PT 100 or Thermocouples, with reading equipment or recorder, in the control board of the installation for continuous surveillance.

Alarm and early warning

All protective equipment may be backed up by another type of protection (with different NRTs). The first device will then act as an «early warning» (light or sound signals given without shutting down the power circuits), and the second device will be the actual alarm (shutting down the power circuits).

Built-in direct thermal protection

For low rated currents, bimetallic strip-type protection may be used. The line current passes through the strip, which shuts down or restores the supply circuit as necessary. The design of this type of protection allows for manual or automatic reset.



D7 - Performance

D7.2 - POWER FACTOR ($COS\phi$) CORRECTION

To help improve current supply in the power lines, electricity supply distributors now ask their customers to have loads with a Power Factor ($\cos \phi$) as near as possible to 1 or at least higher than 0.93.

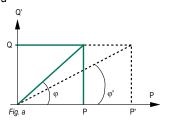
To create the magnetic field, induction motors absorb reactive power (Q) and introduce a Power Factor which may be quite different from the one recommended by electricity supply distributors.

There are, however, several ways of correcting the Power Factor:

a/ by changing the active power

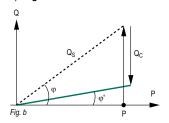
- increase active energy consumption (space heaters, lighting, etc)

- use synchronous machines (cos ϕ = 1). Fig. a



b/ by changing the reactive power

- provide capacitive reactive compensation for the generally inductive reactive drop in the installation (power lines and induction motors). *Fig. b*



The need for Power Factor correction is not linked to faults in design or manufacture. Instead of the two procedures outlined above, it may be easier to use the chart opposite to calculate the compensating reactive power.

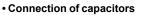
• Calculating the compensating reactive power

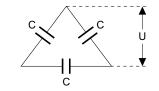
$$Q = \frac{Pu}{\eta} (tg\phi - tg\phi')$$

where Pu active output power

η motor efficiency

tg ϕ and tg ϕ' phase angle error before and after connection





The capacitor values are given by the following formula (in three-phase):

 $Q = U^2 C \omega \cdot \sqrt{3}$

U voltage of the mains with an angular velocity of the phases:

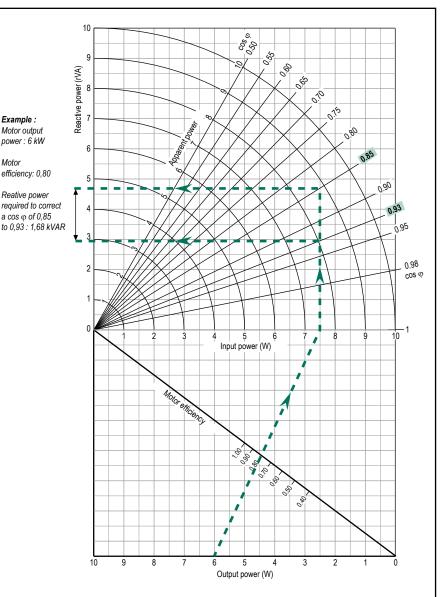
 ω ($\omega = 2 \pi \cdot f$)

IMPORTANT:

The use of capacitors on motor terminals can cause certain problems:

- in hypersynchronous braking, the motor operates as a self-excited generator and high peak voltages will occur across the mains connected terminals

- in the event of micro-cuts, reactive energy is released which will excite the motor. When the supply is restored, high transient voltages may occur.



For increased accuracy when using the chart, multiply the horizontal scale and the vertical scale by the same factor. The result should be divided by the same factor.

Chart for finding the reactive power required for power factor improvement.



D7 - Performance

D7.3 - MOTORS OPERATING IN PARALLEL

Motors connected to the same mechanical shaft

A mechanical shaft can be operated by two or more separate motors:

a) If the motors are of the same type, the total power consumption on the line is equally distributed between the motors (to within the different slip variations).

b) If the motors are of different types, the power is distributed according to the steady speed of the whole unit. So, a small motor with high slip, placed on the same line as a large motor with minimal slip, will run at more or less the same speed as the large motor and therefore only provide a small proportion of the rated power.

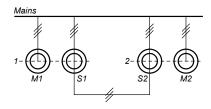


Motors coupled to independent shafts which must rotate at the same speed:

electrical shaft

To avoid deformation problems in large machines (gantry cranes, for example), separately sited mechanical shafts have to be synchronized to rotate at the same speed, whatever their loads.

We can then draw the follow diagram, called an electrical shaft :



1 - 2 : mechanical shafts to be synchronized

M1 - M2: drive motors, normally cage induction motors, providing the average torque on each line.

S1 - S2: synchronizing slipring motors, coupled to the drive motors M1 and M2, whose rotor circuits are linked phase-tophase. These motors have the dimensions required for providing the synchronization power defined in the application specification.

Note: There is a simplified version of this diagram, in which motors M1 and M2 are absent and motors S1 and S2 carry out both functions. In this case both rotors output into a single rheostat for minimum slip operation, which will enable any desynchronization (out-of-step) to be detected and the necessary speed compensation to be made.

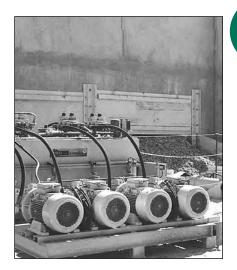
For a given power, machine dimensions will have to be large enough to be able to supply sufficient motor and synchronization torque, and minimize losses due to rotor slip.

Motors in parallel on the same supply controlled by a single switch

Example: drying tunnel with several fans.

As manufacturing inaccuracies in the windings can occur, it is best to check the order of the motor and line phases before starting, and not to use motors with different internal connections so as to avoid circulating currents which might destroy complete installations.

All equipotential neutral connections must be excluded.





D8 - Starting methods for cage induction motors

The two essential parameters for starting cage induction motors are:

- starting torque
- starting current

These two parameters and the resistive torque determine the starting time.

These three characteristics arise from the construction of cage induction motors. Depending on the driven load, it may be necessary to adjust these values to avoid torque impulse on the load or current surges in the supply. There are essentially five different types of supply, which are:

- D.O.L. starting
- star/delta starting
- soft starting with
- auto-transformer
- soft starting with resistors
- electronic starting

The tables on the next few pages give the electrical outline diagrams, the effect on the characteristic curves, and a comparison of the respective advantages of each mode.

D8.1 - MOTORS WITH ASSOCI-ATED ELECTRONICS

«Electronic» starting modes control the voltage at the motor terminals throughout the entire starting phase, giving very gradual smooth starting.

«Unistart» electronic soft starter

This electronic starter enables three-phase induction motors to be started smoothly by controlling their acceleration.

Characteristics:

- P < 2.2 kW 380V-415V 50/60 Hz
- P < 1.5 kW 230V 50/60 Hz
- Ramp from 0.5 to 10 s
- Starting torque adjustable from 0 to 100%.

«Digistart» electronic soft starter

- 10 models from 9 to 500 kW
- Supply: 220 to 690 V 50/60 Hz

- Advantages:

- · Protects both itself and the motor over the whole power range.
- · Can be used on all motors without derating
- Fault signalling
- Simple digital programming
- · Keypad or remote control



Hyper control

Hyper Control is an electronic system which is placed between the multi-speed motor and the low-speed power supply contactor, and is used to manage torque when changing from one speed to another.

6 power ratings

RATINGS	HC.1.22.400	HC.3.22.400	HC.4.8.9.400
Low speed motor power		0.06 to 3.9 kW	
Three-phase mains supply voltage		400 V +10% -10%	
RATINGS	HC.1.22.230	HC.3.22.230	HC.4.8.9.230

RATINGS	HC.1.22.230	HC.3.22.230	HC.4.8.9.230		
Low speed motor power	0.035 to 2.25 kW				
Three-phase mains supply voltage	230 V +10% -10%				
Mains frequency	50 / 60 Hz ±5%				
Protection	IP 20				
Housing in composite material					

D8.2 - VARIABLE SPEED MOTOR

· These motors (VARMECA type) are designed and developed with built-in electronics.

- Characteristics:
- 0.75 < P ≤ 7.5 kW*
- 50/60 Hz
- 360 < speed < 2400 min⁻¹
- for 4-pole motors
- Cos φ = 1
- Constant torque * other power ranges on request

Starting on variable speed drive

One of the advantages of variable speed drives is that loads can be started without a current surge on the mains supply, since starting is always performed with no voltage or frequency at the motor terminals.



VARMECA

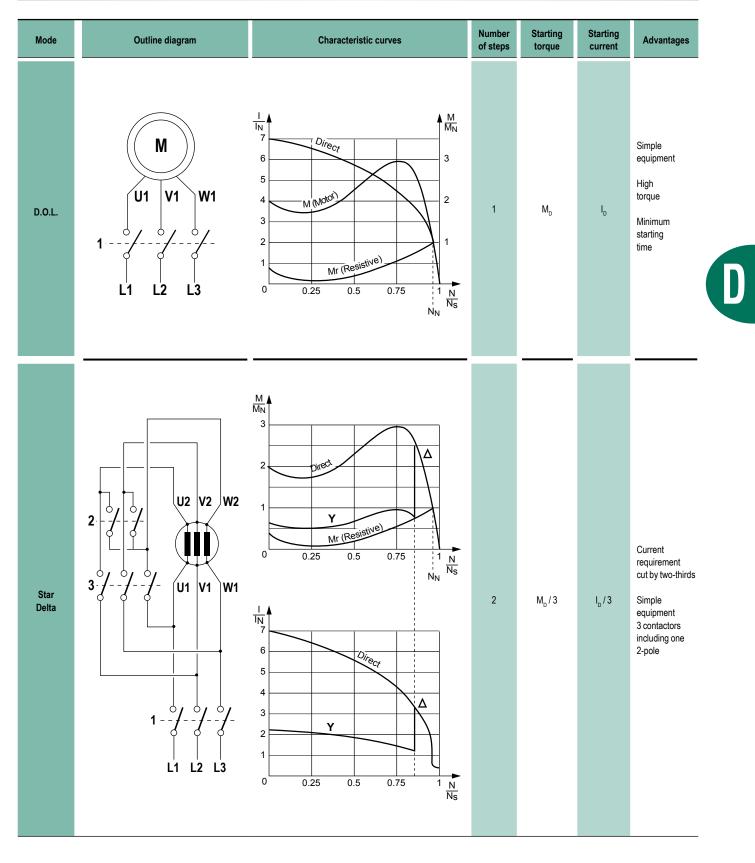


UNISTART



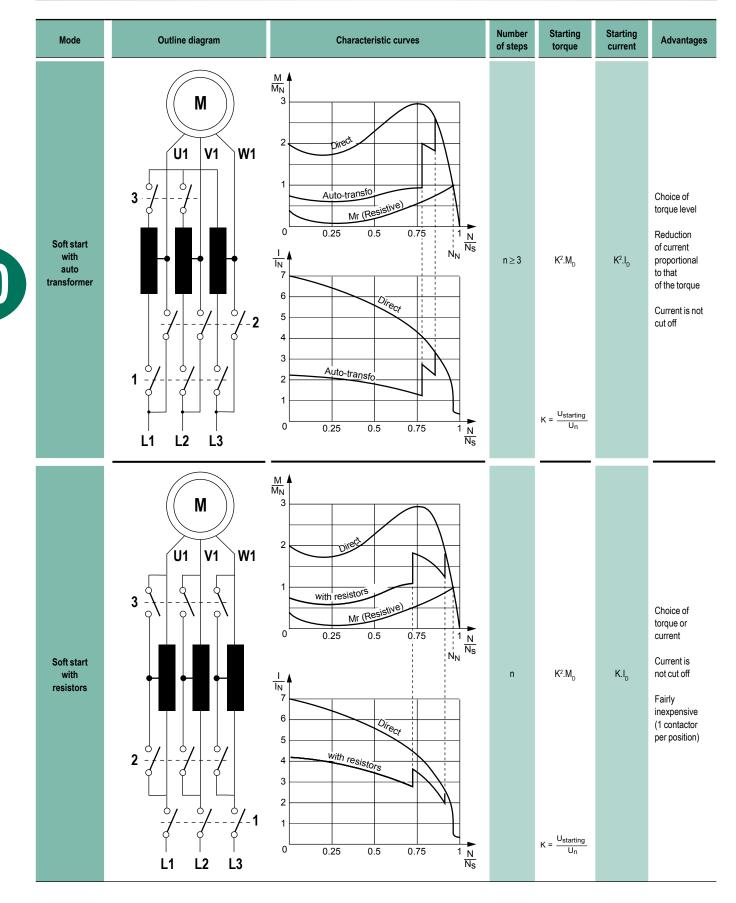
DIGISTART

D8 - Starting methods for cage induction motors



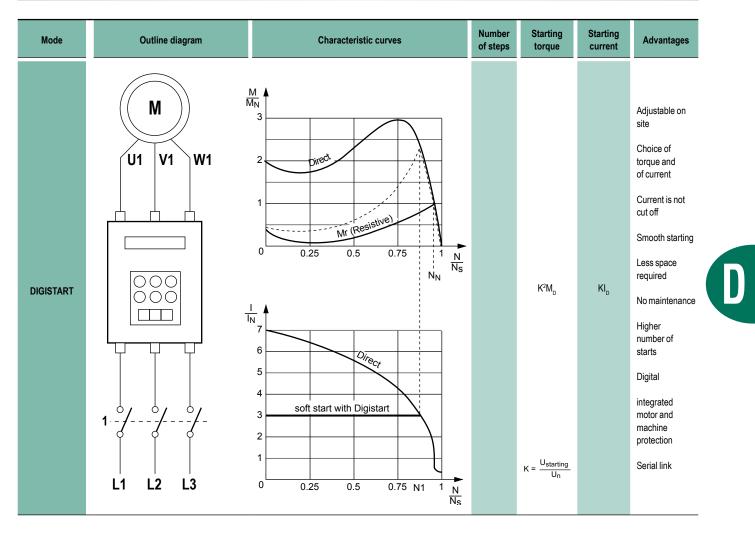


D8 - Starting methods for cage induction motors





D8 - Starting methods for cage induction motors





D9 - Braking methods

General information

The braking torque is equal to the torque produced by the motor increased by the resistive torque of the driven machine.

$$C_f = C_m + C$$

C_f= braking torque

C_m= motor torque

C_r = resistive torque

Braking time, i.e. the time required for an induction motor to change from speed N to stop, is calculated by the formula:

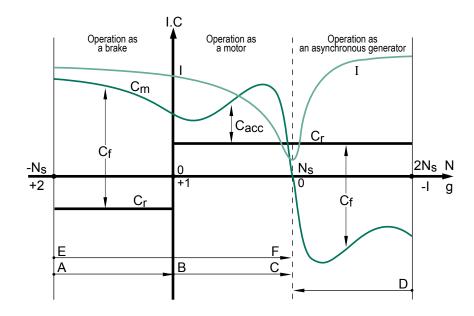
$$\mathsf{T}_{\mathsf{f}} = \frac{\Pi \cdot \mathsf{J} \cdot \mathsf{N}}{\mathbf{30} \cdot \mathsf{C}_{\mathsf{f}}(\mathsf{av})}$$

 $T_f(in s) = braking time$

J (in kgm²) = moment of inertia

N (in min⁻¹) = speed of rotation C_e (av) (in N.m) = average braking torque

during the time period



Curves I = f(N), $C_m = f(N)$, $C_r = f(N)$, in the motor starting and braking zones.

- = current absorbed
- C = torque value
- C_f = braking torque
- C_r = resistive torque
- C_m = motor torque
- N = speed of rotation

- g = slip
- N_s = synchronous speed
- AB = reverse-current braking
- BC = starting, acceleration
- DC = braking as asynchronous generator
- EF = reverse

Reverse-current braking

This method of braking is obtained by reversing two of the phases.

In general, an isolator disconnects the motor from the supply at the time the speed changes to N=0.

In cage induction motors, the average braking torque is generally greater than the starting torque.

Braking torque varies in different types of machine, as it depends on the rotor cage construction.

This method of braking involves a large amount of absorbed current, more or less constant and slightly higher than the starting current.

Thermal stresses during braking are three times higher than during acceleration.

Accurate calculations are required for repetitive braking.

Note: The direction of rotation of a motor is changed by reverse-current braking and restarting.

Thermically, one reversal is the equivalent of 4 starts. Care must therefore be taken when choosing a machine.

D.C. injection braking

Operating stability can be a problem when reverse-current braking is used, due to the flattening out of the braking torque curve in the speed interval $(O, -N_s)$.

There is no such problem with D.C. injection braking: this can be used on both cage induction and slipring motors.

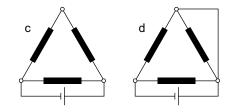
With this braking method, the induction motor is connected to the mains and braking occurs when the A.C. voltage is cut off and D.C. voltage is applied to the stator.

There are four different ways of connecting the windings up to direct current.

The D.C. applied to the stator is usually supplied by a rectifier plugged into the mains.

Thermal stresses are approximately three times lower than for reverse-current braking.

The shape of the braking torque curve in the speed interval $(0, -N_s)$ is similar to that of the curve Cm = f (N) and is obtained by changing the abscissa variable to $N_r = N_s - N$.



Motor winding connections for direct current



The braking current is calculated using the formula:

$$I_{f} = k1_{i} \times I_{d} \sqrt{\frac{C_{f} - C_{fe}}{k_{2} - Cd}}$$

The values of k1 for each of the four connections are:

k1 _a = 1.225	k1 _c =2.12
k1, = 1.41	k1_= 2.45

The braking torque can be found by the formula:

$$C_{f} = \frac{\Pi \cdot J \cdot N}{30 \cdot T_{f}}$$

In the formulae above:

l _f (in A)	= braking current					
l _d (in A)	= starting current in the phase					
	$= \frac{1}{\sqrt{3}} I_{d} \text{ given in catalogue} \\ \text{(for } \Delta \text{ connection)}$					
C _f (in N.m)	= average braking torque in the interval (N $_{\rm s}$, N)					
$\rm C_{fe}$ (in N.m)	= external braking torque					
C_{d} (in N.m)	= starting torque					
J (en kgm ²)	= total moment of inertia on the drive shaft					
N (in min ⁻¹)	= speed of rotation					
T _f (in s)	= braking time					
k1 _i	 numerical factors for connections a, b, c and d (see diagram) 					
k2	= numerical factors taking into account the average braking torque (k2 = 1.7)					

The direct current to be applied to the windings is calculated by:

 $U_{f} = k3_{i} \cdot k4 \cdot I_{f} \cdot R_{1}$

k3 values for the four diagrams are as follows:

k3 = 2	
k3 = 1.5	
k3 = 0.66	3
k3 = 0.5	
U _f (in V)	= voltage for braking
l _f (in A)	= direct current for braking
R_1 (en Ω)	= stator phase resistance at 20° C
k3 _i	 numerical factors for connections a, b, c and d (see diagrams)
k4	= numerical factor taking into account the motor temperature

rise of the motor (k4 = 1.3)

Mechanical braking

Electromechanical brakes (D.C. or A.C field excitation) can be fitted at the rear of the motor.

D9 - Braking methods

For further details, see our «Brake motors» catalogue.

Regenerative braking

This is the braking method de applied to multi-speed motors when changing down to lower speeds. This procedure cannot be used to stop the motor.

Thermal stresses are approximately equal to those occurring when motors with Dahlander connections are started at the lower rated speed (speed ratio 1 : 2).

With the motor at the lower speed, working as a generator, it develops very high braking torque in the speed interval $(2N_s, N_s)$.

The maximum braking torque is slightly higher than the starting torque of the motor at the lower speed.

Deceleration brakes

For safety reasons, deceleration brakes are fitted at the rear of motors used on hazardous machines (for example, where cutting tools may come into contact with the operator).

The range of brakes is determined by the braking torques:

2.5 - 4 - 8 - 16 - 32 - 60 Nm

The appropriate brake is selected in the factory according to the number of poles of the motor, the driven inertia, the number of brakings per hour and the required braking time.







D10 - Operation as an asynchronous generator

D10.1 - GENERAL

The motor operates as an asynchronous generator each time the load becomes a driving load and the rotor speed exceeds the synchronous speed ($N_{\rm s}$).

This can be induced either voluntarily, as in the case of electric power stations (water or wind power, etc) or involuntarily, caused by factors linked to the application (downward movement of crane hooks or blocks, inclined conveyors, etc).

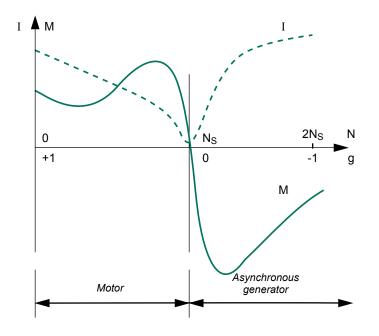
D10.2 - OPERATING CHARACTERISTICS

The diagram opposite shows the various operations of an asynchronous machine in relation to its slip (g) or its speed (N).

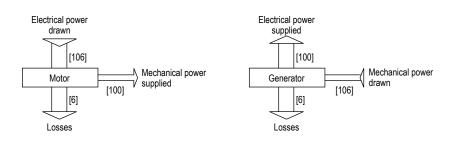
Example: let us consider an induction motor of 45 kW, 4 poles, 50 Hz at 400V. As a rough estimate, its characteristics as an asynchronous generator can be deduced from its rated characteristics as a motor, by applying the rules of symmetry.

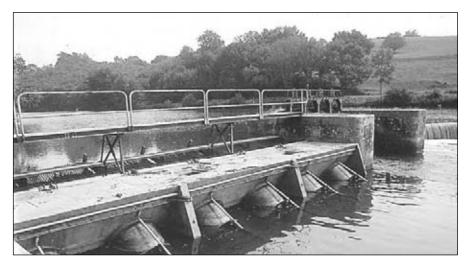
If more precise values are required, the manufacturer should be consulted.

In practice, it can be checked that the same machine, operating as a motor and as a generator with the same slip, has approximately the same losses in both cases, and therefore virtually the same efficiency. It can be deduced from this that the rated electrical power supplied by the asynchronous generator will be virtually the same as the motor output power.



Characteristics	Motor	GA
Synchronous speed(min ^{.1})	1500	1500
Rated speed(min ⁻¹)	1465	1535
Rated torque(m.N)	+ 287	- 287
Rated current at 400V(A)	87 A (absorbed)	87 A (supplied)







D10 - Operation as an asynchronous generator



D10.3 - CONNECTION TO A POWERFUL MAINS SUPPLY

It is assumed that the machine stator is connected to a powerful electrical mains supply (usually the national grid), ie. a mains supply provided by a generator which regulates the power to at least twice that of the asynchronous generator.

Under these conditions, the mains supply imposes its own voltage and frequency on the asynchronous generator. Furthermore, it supplies it automatically with the reactive energy necessary for all its operating conditions.

D10.3.1 - Connection -Disconnection

Before connecting the asynchronous generator to the mains supply, it is necessary to ensure that the direction of phase rotation of the asynchronous generator and the mains supply are in the same order.

• To connect an asynchronous generator to the mains supply, it should be accelerated gradually until it reaches its synchronous speed Ns. At this speed, the machine torque is zero and the current is minimal.

This is an important advantage of asynchronous generators: as the rotor is not polarised until the stator is powered up, it is not necessary to synchronise the mains supply and the machine when they are connected. However, there is a phenomenon affecting the connection of asynchronous generators which, in some cases, can be a nuisance: the rotor of the asynchronous generator, although not energised, still has some residual magnetism.

On connection, when the magnetic flux created by the mains supply and that caused by the residual magnetism of the rotor are not in phase, the stator experiences a very brief current peak (one or two half-waves), combined with an instantaneous overtorque of the same duration.

It is advisable to use connecting stator resistances to limit this phenomenon.

• Disconnecting the asynchronous generator from the mains supply does not pose any particular problem.

As soon as the machine is disconnected, it becomes electrically inert since it is no longer energised by the mains supply. It no longer brakes the driving machine, which should therefore be stopped to avoid reaching overspeed.

D10.3.1.1 - Reactive power compensation

To limit the current in the lines and the transformer, the asynchronous generator can be compensated by restoring the power factor of the installation to the unit, using a bank of capacitors.

In this case, the capacitors are only inserted at the terminals of the asynchronous generator once it has been connected, to avoid self-energisation of the machine due to the residual magnetism during speed pickup. For a 3-phase low voltage asynchronous generator, 3-phase or single-phase capacitors in delta connection are used.

D10.3.1.2 - Electrical protection and safety

There are two protection and safety categories:

- those which relate to the mains

- those which relate to the set and its generator

The major mains protection devices monitor:

- maximum-minimum voltage
- maximum-minimum frequency

- minimum power or energy feedback (operating as a motor)
- generator connection fault
- The protection devices for the set are:
- stop on detection of racing start
- lubrication faults

- thermal magnetic protection of the generator, usually with probes in the winding.

D10.4 - POWER SUPPLY FOR AN ISOLATED NETWORK

This concerns the supply of a consuming network which does not have another generator of sufficient power to impose its voltage and frequency on the asynchronous generator.

D10.4.1 - Reactive power compensation

In the most common case, reactive energy must be supplied:

- to the asynchronous generator
- to the user loads which consume it

To supply both of these consumption types with reactive energy, use a reactive energy source of suitable power connected in parallel on the circuit. This is usually a bank of capacitors with one or more stages which may be fixed, manually adjusted (using notches) or automatically adjusted. Synchronous capacitors are now rarely used.

Example: in an isolated network with power consumption of 50 kW where $\cos \phi = 0.9$ (and $\tan \phi = 0.49$), supplied by an asynchronous generator with $\cos \phi$ of 0.8 at 50 kW (and $\tan \phi = 0.75$), it is necessary to use a bank of capacitors which supplies:

(50 x 0.49) + (50 x 0.75) = 62 kvar



D10 - Operation as an asynchronous generator



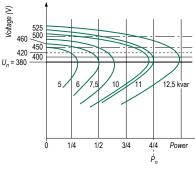
D10.4.2 - Characteristic curves

At rated frequency, an asynchronous generator supplies a voltage which depends on the active power supplied and the value of the energisation capacitors.

For each asynchronous generator, it is possible to plot a network of curves such as those shown below.

In conclusion, to maintain a constant voltage, the reactive power must be adapted to the active power required.

Adjusting the load and the capacitors does not present any special difficulties. The table below shows how these parameters should be modified.



Example of a13 kW and 6-pole machine

Direction of adjustment for load and capacitors

Prot	olem	Action	
Frequency	Voltage	Action	
Too high	Too high	Increase the active load or reduce the speed or mechanical power	
Too high	Too low	Increase the capacitor bank capacity	
Too low	Too high	Decrease the capacitor bank capacity	
Too low	Too low	Reduce the active load or increase the speed	

D10.4.3 - Regulation

When the power consumed by the user or the power supplied by the driving machine vary but the frequency and voltage are to be maintained within narrow limits, a regulation device must be provided. This device is designed to maintain the correct electrical characteristics by adjusting one or more parameters:

- active power supplied (driving machine)

- active power consumed (loads on the circuit in use)

- reactive power supplied (usually capacitors).

D10.4.4 - Control and protection

The installation comprises an electrical measuring, control and protection enclosure. The only special devices are:

- time delay on connection of the load circuit to avoid de-energisation of the machine on starting

- control of the energisation capacitors, manually or automatically as required

The rest of the electrical equipment is completely standard.

D10.5 - PERFORMANCE OF MOTORS USED AS AG

- Preference should be given to 4 - 6 or 8 pole versions for power ratings above 5.5 kW depending on the speeds of the driven machines.

- For small generators ($P \le 4$ kW), the most common application uses 2 poles.

- For standard motors, the no-load voltages of asynchronous generators are very high and the voltage drop for the rated power is around 15% (power ratings below the rated power should not be used).

- Remember that asynchronous generators consume the reactive power required for their energisation and supply active power to the mains (isolated or non-isolated) and that the reactive power of the loads should be compensated.



E1 - Selection data: single speed

2 poles - 3000 min ⁻¹	. 88 - 89
4 poles - 1500 min ⁻¹	90 -91
6 poles - 1000 min ⁻¹	. 92 -93
8 poles - 750 min ⁻¹	. 94 -95

E2 - Selection data: two-speed

Centrifugal applications

2 / 4 poles - 3000 / 1500 min ⁻¹	. 96
4 / 6 poles - 1500 / 1000 min ⁻¹ (2 separate windings)	97
4 / 6 poles - 1500 / 1000 min ⁻¹ (1 PAM winding)	98
4 / 8 poles - 1500 / 750 min ⁻¹	. 99
6 / 12 poles - 1000 / 500 min ⁻¹	100

General table of two-speed motors

Centrifugal applications	101
General applications	



E1 - Selection data: Single-speed



IP 55 - S1 Cl. F - ∆T 80 K



					MAI	NS SI	JPPL	Y A 23	30/Y	400 V	or	0 V .	50 Hz				
	Rated power at 50 Hz	Rated speed	Rated torque	Rated current		Power factor			Efficiency		Starting current/ Rated current	Starting torque/ Rated torque	Max. torque./ Rated torque	Rated apparent power	Torque* curve	Moment of inertia	Weight
Туре	P _N kW	N _N min ⁻¹	C _N N.m	I _{N (400V)} A	50 %	Cos φ 75 %	100 %	50 %	η 75 %	100 %	I_D/I_N	M_D/M_N	$M_{_M}/M_{_N}$	kVA _N	N°	J kg.m ²	IM B3 kg
LS 56 L	0.09	2860	0.3	0.44	0.40	0.45	0.55	37	45	54	4.9	5.5	5.6	0.30	1	0.00015	3.8
LS 56 L	0.12	2820	0.4	0.50	0.45	0.55	0.60	45	54	58	4.6	4.1	4.2	0.34	1	0.00015	3.8
LS 63 M	0.18	2790	0.6	0.52	0.55	0.65	0.75	59	66	67	5	3.4	3	0.36	1	0.00019	4.8
LS 63 M	0.25	2800	0.8	0.71	0.55	0.65	0.75	59	67	68	5.4	3.4	3.1	0.49	1	0.00025	6
LS 71 L	0.37	2800	1.3	0.98	0.60	0.70	0.80	63	67	68	5.2	3.2	3.8	0.68	1	0.00035	6.4
LS 71 L	0.55	2800	1.9	1.32	0.55	0.70	0.80	71	75	75	6	3.2	3.1	0.92	1	0.00045	7.3
LS 71 L	0.75	2780	2.5	1.70	0.65	0.75	0.85	73	75	75	6	3.4	3	1.18	1	0.00060	8.3
LS 80 L	0.75	2840	2.5	1.64	0.68	0.80	0.87	74	76.5	76	5.9	2.4	2.2	1.13	1	0.00070	8.2
LS 80 L	1.1	2837	3.7	2.4	0.65	0.77	0.84	76.6	78.5	78	5.8	2.7	2.4	1.7	6	0.00090	9.7
LS 80 L	1.5	2859	5	3.2	0.62	0.76	0.83	78	80.4	80.3	7	3.2	2.8	2.2	5	0.0011	11.3
LS 90 S	1.5	2870	5	3.4	0.58	0.72	0.81	75.1	78.9	79.6	8	3.9	4	2.3	5	0.0014	12
LS 90 L	1.8	2865	6	3.6	0.69	0.80	0.86	81.7	83.4	83.1	8	3.6	3.6	2.5	5	0.0017	14
LS 90 L	2.2	2862	7.4	4.3	0.73	0.83	0.88	82.9	84	83.6	7.7	3.7	3.3	3	5	0.0021	16
LS 100 L	3	2868	10	6.3	0.59	0.73	0.81	80.8	83.8	83.9	7.5	3.8	3.9	4.3	5	0.0022	20
LS 112 M	4	2877	13.5	7.9	0.65	0.78	0.85	84.4	86.1	86	7.8	2.9	2.9	5.5	5	0.0029	24.4
LS 112 MG	5.5	2916	18.1	10.5	0.71	0.81	0.88	85.6	87.2	86.6	9	3.1	3.5	7.2	5	0.0076	33
LS 132 S	5.5	2916	18.1	10.5	0.71	0.81	0.88	85.6	87.2	86.6	9	3.1	3.5	7.2	5	0.0076	34.4
LS 132 S	7.5	2905	24.5	14.7	0.63	0.78	0.85	84.5	86.4	86.5	8.7	3.4	3.6	10.2	5	0.0088	39
LS 132 M	9	2910	29.6	17.3	0.71	0.80	0.85	87.5	88.4	88.1	8.6	2.5	3.5	12	5	0.016	49
LS 132 M	11	2944	36	20.7	0.69	0.81	0.86	87.7	89.4	89.4	7.5	2.7	3.4	14.3	5	0.018	54
LS 160 MP	11	2944	36	20.7	0.69	0.81	0.86	87.7	89.4	89.4	7.5	2.7	3.4	14.3	5	0.019	62
LS 160 MP	15	2935	48.8	28.4	0.71	0.79	0.85	85.1	90.1	90	8.1	3	3.5	19.7	5	0.023	72
LS 160 L	18.5	2934	60.2	33.7	0.75	0.83	0.87	90.4	91.2	91	8	3	3.3	23.4	4	0.044	88
LS 180 MT	22	2938	71.5	39.9	0.76	0.84	0.87	91.2	91.8	91.5	8.1	3.1	3.1	27.6	4	0.052	99
LS 200 LT	30	2946	97.2	52.1	0.82	0.87	0.9	92.1	92.7	92.4	8.6	2.7	3.4	36.1	4	0.089	154
LS 200 L	37	2950	120	64.6	0.82	0.87	0.89	92.2	93	92.9	7.4	2.6	3	44.8	4	0.120	180
LS 225 MT	45	2950	146	77.4	0.82	0.87	0.9	93.1	93.4	93.3	7.5	2.8	3.1	53.6	4	0.140	200
LS 250 MZ	55	2956	178	95.2	0.8	0.86	0.89	93.1	93.7	93.7	8.3	3.1	3.4	66	4	0.173	235
LS 280 SC	75	2968	241	127	0.82	0.87	0.9	93.8	94.4	94.4	8.5	2.6	3.4	88.3	4	0.39	330
LS 280 MC	90	2968	290	152	0.83	0.88	0.9	94.1	94.7	94.7	8.4	2.6	3.3	105.6	4	0.47	375
LS 315 SP	110	2976	353	190	0.8	0.86	0.88	93.2	94.3	94.8	7.8	2.8	2.9	131.9	4	1.43	645
LS 315 MP	132	2976	424	225	0.82	0.87	0.89	93.4	94.6	95	7.6	2.8	2.9	156.1	4	1.67	715
LS 315 MR	160	2976	513	270	0.84	0.88	0.9	93.6	94.8	95.1	7.6	2.9	3.1	186.9	4	1.97	820
LS 315 MR •	200	2982	640	349	0.82	0.86	0.87	94.3	94.9	95	9.3	3.8	3.9	242	4	1.97	845

Class F temperature rise

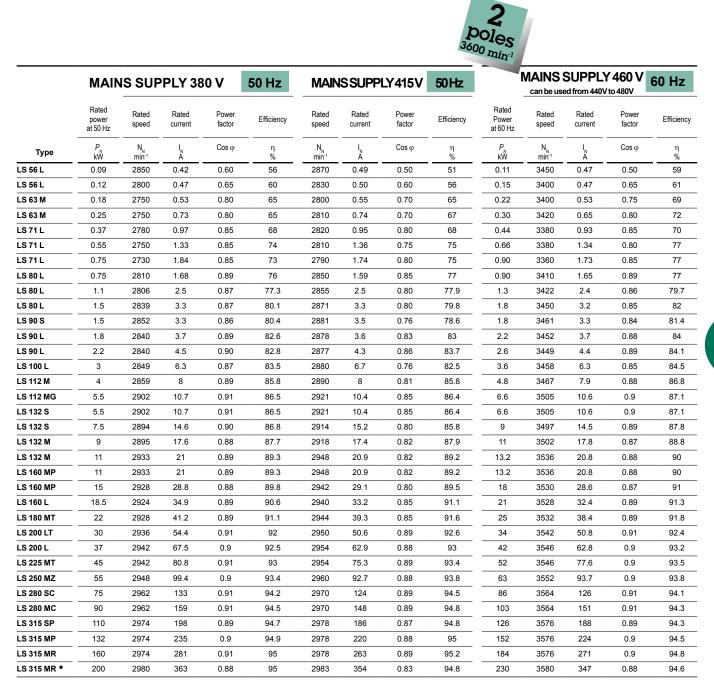
* Torque curve

Noise level

section D4.4 - page 61



E1 - Selection data: Single-speed



Class F temperature rise

Note: For mains supplies with different voltages, see section D2.2.4.

E



E1 - Selection data: Single-speed



E

IP 55 - S1 CI. F - ∆T 80 K



					MAI	NS SI	JPPĽ	Y 🛆 23	30 / Y 4	400 V	or Δ 40	0 V (50 Hz				
	Rated power at 50 Hz	Rated speed	Rated torque	Rated current		Power factor			Efficiency		Starting current/ Rated current	Starting torque/ Rated torque	Max. torque/ Rated torque	Apparent rated power	Torque* curve	Moment of inertia	Weight
Туре	P _N kW	N _N min ⁻¹	C _N N.m	I _{N (400V)} A	50 %	Cos φ 75 %	100 %	50 %	η 75 %	100 %	I_D/I_N	M_D/M_N	$M_{_M}/M_{_N}$	kVA _N	N°	J kg.m ²	IM B3 kg
LS 56 L	0.09	1400	0.6	0.39	0.42	0.52	0.60	42.8	49.6	55	3.2	2.8	2.8	0.27	2	0.00025	4
LS 63 M	0.12	1380	0.8	0.44	0.47	0.58	0.70	46.8	54	56	3.2	2.5	2.4	0.31	2	0.00035	4.8
LS 63 M	0.18	1390	1.2	0.64	0.44	0.55	0.65	51	58	62	3.7	2.7	2.7	0.45	2	0.00048	5
LS 71 L	0.25	1425	1.7	0.80	0.45	0.56	0.65	60	67	69	4.6	2.7	2.9	0.56	2	0.00068	6.4
LS 71 L	0.37	1420	2.5	1.06	0.47	0.59	0.70	66	72	72	4.9	2.4	2.8	0.73	2	0.00085	7.3
LS 71 L	0.55	1400	3.8	1.62	0.49	0.62	0.70	65	70	70	4.8	2.3	2.5	1.12	2	0.0011	8.3
LS 80 L	0.55	1410	3.8	1.42	0.55	0.68	0.76	62	69.3	73.4	4.5	2	2.3	1	7	0.0013	8.2
LS 80 L	0.75	1400	5.1	2.01	0.59	0.71	0.77	66	70	70	4.5	2	2.2	1.4	7	0.0018	9.3
LS 80 L	0.9	1425	6	2.44	0.54	0.67	0.73	70	73	73	5.8	3	3	1.6	6	0.0024	10.9
LS 90 S	1.1	1429	7.4	2.5	0.64	0.77	0.84	77.1	78.4	76.8	4.8	1.6	2	1.7	7	0.0026	11.5
LS 90 L	1.5	1428	10	3.4	0.60	0.74	0.82	77.5	79.4	78.5	5.3	1.8	2.3	2.3	7	0.0032	13.5
LS 90 L	1.8	1438	12	4	0.61	0.75	0.82	79	80.8	80.1	6	2.1	3.2	2.7	4	0.0037	15.2
LS 100 L	2.2	1436	14.7	4.8	0.59	0.73	0.81	79.8	81.5	81	5.9	2.1	2.5	3.4	7	0.0043	20
LS 100 L	3	1437	20.1	6.5	0.59	0.72	0.81	80.8	82.6	82.6	6	2.5	2.8	4.5	6	0.0055	22.5
LS 112 M	4	1438	26.8	8.3	0.57	0.76	0.83	83.4	84.2	84.2	7.1	2.5	3	5.7	6	0.0067	24.9
LS 132 S	5.5	1447	36.7	11.1	0.67	0.79	0.83	85.8	86.4	85.7	6.3	2.4	2.8	7.7	6	0.014	36.5
LS 132 M	7.5	1451	49.4	15.2	0.61	0.74	0.82	84.9	86.4	87	7	2.4	2.9	10.5	6	0.019	54.7
LS 132 M	9	1455	59.3	18.1	0.62	0.74	0.82	86.2	87.6	87.7	6.9	2.2	3.1	12.5	4	0.023	59.9
LS 160 MP	11	1454	72.2	21	0.67	0.79	0.86	87.4	88.6	88.4	7.7	2.3	3.2	14.5	1	0.030	70
LS 160 LR	15	1453	98	28.8	0.69	0.78	0.84	88.4	89.8	89.4	7.5	2.9	3.6	20	1	0.036	86
LS 180 MT	18.5	1456	121	35.2	0.67	0.79	0.84	90.3	90.8	90.3	7.6	2.7	3.2	24.4	1	0.085	100
LS 180 LR	22	1456	144	41.7	0.68	0.79	0.84	90.9	91.2	90.7	7.9	3	3.3	28.9	1	0.096	112
LS 200 LT	30	1460	196	56.3	0.69	0.8	0.84	91.5	92	91.5	6.6	2.9	2.9	39	2	0.151	165
LS 225 ST	37	1468	241	68.7	0.7	0.8	0.84	92.9	93.1	92.5	6.3	2.7	2.6	47.6	2	0.24	205
LS 225 MR	45	1468	293	83.3	0.7	0.8	0.84	93	93.3	92.8	6.3	2.7	2.6	57.7	2	0.29	235
LS 250 ME	55	1478	355	101	0.71	0.8	0.84	93.2	93.8	93.6	7	2.7	2.8	70	3	0.63	320
LS 280 SC	75	1478	485	137	0.71	0.8	0.84	93.8	94.4	94.2	7.2	2.8	2.9	94.8	3	0.83	380
LS 280 MD	90	1478	581	164	0.71	0.8	0.84	93.8	94.5	94.4	7.6	3	3	113.5	3	1.03	450
LS 315 SP	110	1484	708	197	0.74	0.82	0.85	93.9	94.7	94.8	7	2.7	2.7	136.5	3	2.32	670
LS 315 MP	132	1484	849	236	0.74	0.82	0.85	94.1	95	95	7.6	2.9	3	163.5	3	2.79	750
LS 315 MR	160	1484	1030	286	0.74	0.82	0.85	94.1	95	95	7.7	2.9	3	198.1	3	3.27	845
LS 315 MR •	200	1486	1285	359	0.69	0.79	0.84	95.1	95.8	95.8	8.1	3.1	3.4	248.5	3	3.27	860

• Class F temperature rise

* Torque curve

section D4.4 - page 61



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E1 - Selection data: Single-speed



	MAIN	NS SUF	PPLY 38	30 V	50 Hz	MAINS	SUPPL	(415V	50 Hz		can be use	SUPPL ed from 440		60 Hz
	Rated power at 50 Hz	Rated speed	Rated current	Power factor	Efficiency	Rated speed	Rated current	Power factor	Efficiency	Rated power at 60 Hz	Rated speed	Rated current	Power factor	Efficiency
Туре	P _N kŴ	N _N min ⁻¹	I _N	Cos φ	η %	N _N min ⁻¹	I _N A	Cos φ	η %	P _N kŴ	N _N min ⁻¹	I N	$\text{Cos}\phi$	η %
LS 56 L	0.09	1380	0.38	0.65	56	1410	0.40	0.60	52	0.11	1700	0.36	0.60	62
LS 63 M	0.12	1365	0.47	0.70	56	1390	0.46	0.65	56	0.15	1680	0.46	0.70	59
LS 63 M	0.18	1375	0.68	0.65	62	1400	0.68	0.60	61	0.22	1690	0.64	0.65	65
LS 71 L	0.25	1425	0.78	0.70	70	1430	0.84	0.60	69	0.30	1720	0.76	0.70	71
LS 71 L	0.37	1410	1.10	0.70	73	1430	1.10	0.65	72	0.44	1720	1.06	0.70	75
LS 71 L	0.55	1385	1.59	0.75	70	1410	1.56	0.70	70	0.66	1700	1.51	0.75	73
LS 80 L	0.55	1396	1.43	0.80	73	1415	1.41	0.74	72.7	0.66	1725	1.4	0.78	77.3
LS 80 L	0.75	1380	2.06	0.80	69	1410	2.01	0.74	70	0.90	1700	2.01	0.77	73
LS 80 L	0.9	1415	2.43	0.77	73	1435	2.48	0.70	72	1.1	1710	2.39	0.77	75
LS 90 S	1.1	1416	2.5	0.87	75.5	1437	2.4	0.82	77.2	1.3	1726	2.4	0.85	78.9
LS 90 L	1.5	1415	3.4	0.86	77.6	1436	3.4	0.79	78.4	1.8	1722	3.3	0.84	80.4
LS 90 L	1.8	1427	4	0.85	79.4	1443	4	0.79	80.1	2.2	1733	4	0.84	81.9
LS 100 L	2.2	1426	4.9	0.84	80.2	1442	4.9	0.78	80.6	2.7	1731	4.8	0.82	82.6
LS 100 L	3	1427	6.6	0.84	81.7	1443	6.6	0.77	81.9	3.6	1731	6.5	0.83	83.7
LS 112 M	4	1430	8.6	0.85	83	1448	8.2	0.81	83.6	4.8	1740	8.4	0.84	85.3
LS 132 S	5.5	1438	11.5	0.87	84.3	1450	11.3	0.80	84.6	6.6	1748	11.1	0.83	86.2
LS 132 M	7.5	1445	15.8	0.85	85	1455	15	0.82	85	9	1750	15.5	0.85	86
LS 132 M	9	1440	18.5	0.86	86	1455	18.2	0.80	86	11	1750	18.9	0.84	87
LS 160 MP	11	1446	21.5	0.89	87.8	1458	20.9	0.83	88.2	13.2	1754	20.8	0.85	89.2
LS 160 LR	15	1446	29.8	0.87	88.3	1458	29.9	0.79	88.3	17	1762	29.4	0.82	89.5
LS 180 MT	18.5	1450	35.9	0.87	90	1460	34.7	0.82	90.5	21	1754	33.6	0.86	91.1
LS 180 LR	22	1450	43	0.86	90.4	1460	41.1	0.82	90.9	25	1754	39.9	0.86	91.5
LS 200 LT	30	1454	58.2	0.86	91.1	1464	55.6	0.82	91.6	34	1758	54.5	0.85	92.1
LS 225 ST	37	1462	71.8	0.85	92.1	1470	67.8	0.82	92.6	42	1764	66.7	0.85	93
LS 225 MR	45	1462	87.1	0.85	92.3	1470	82.2	0.82	92.9	52	1764	82.4	0.85	93.2
LS 250 ME	55	1476	105	0.85	93.2	1480	99.6	0.82	93.7	63	1778	99.3	0.85	93.7
LS 280 SC	75	1476	143	0.85	93.9	1480	135	0.82	94.3	86	1778	135	0.85	94.3
LS 280 MD	90	1476	171	0.85	94.1	1480	162	0.82	94.5	103	1778	161	0.85	94.5
LS 315 SP	110	1482	205	0.86	94.6	1486	192	0.84	94.9	126	1784	196	0.85	94.9
LS 315 MP	132	1482	246	0.86	94.9	1486	230	0.84	95.1	152	1784	233	0.86	95.1
LS 315 MR	160	1482	298	0.86	94.9	1486	279	0.84	95.1	184	1784	282	0.86	95.1
LS 315 MR •	200	1484	365	0.87	95.8	1487	354	0.82	95.8	230	1784	350	0.86	95.9
-														

• Class F temperature rise

Note: For mains supplies with different voltages, see section D2.2.4.



E1 - Selection data: Single-speed



IP 55 - S1 CI. F - ∆T 80 K

					MAI	NS S	UPPL	Y ∆ 23	30/Y4	400 V	or ∆ 40	0 V 5	60 Hz				
	Rated power at 50 Hz	Rated speed	Rated torque	Rated current		Power factor			Efficiency		Starting current/ Rated current	Starting torque/ Rated torque	Max. torque/ Rated torque	Rated apparent power	Torque* curve	Moment of inertia	Weight
Туре	P _N kW	N _N min ⁻¹	C _N N.m	I _{N (400V)} A	50 %	Cos φ 75 %	100 %	50 %	η 75%	100 %	I_D/I_N	M_D/M_N	$M_{_M}/M_{_N}$	kVA _N	N°	J kg.m ²	IM B3 kg
LS 63 M	0.09	860	0.9	0.46	0.63	0.70	0.80	26	32	35	2.1	1.8	1.8	0.32	3	0.0006	5.5
LS 71 L	0.12	920	1.3	0.64	0.40	0.48	0.55	36	45	49	2.9	2.5	2.6	0.45	3	0.0007	6.5
LS 71 L	0.18	895	1.8	0.81	0.43	0.53	0.62	43	50	52	2.7	1.9	2	0.56	3	0.0011	7.6
LS 71 L	0.25	840	2.6	1	0.48	0.59	0.70	47	52	50	2.5	1.7	1.7	0.71	3	0.0013	7.9
LS 80 L	0.25	955	2.5	0.85	0.48	0.64	0.67	56	63	63.1	3.9	1.6	1.8	0.59	8	0.0024	8.4
LS 80 L	0.37	950	3.7	1.1	0.57	0.67	0.72	59	61	66	4.3	1.7	2.2	0.76	8	0.0032	9.7
LS 80 L	0.55	950	5.5	1.8	0.47	0.60	0.64	55	63	68	4.9	2.1	2.6	1.2	7	0.0042	11
LS 90 S	0.75	930	7.7	2.1	0.54	0.66	0.77	60	65	68.5	4.2	2.4	2.6	1.4	7	0.0039	13.5
LS 90 L	1.1	915	11.5	3	0.55	0.67	0.76	66	70	70	4.7	2.4	2.5	2.1	6	0.0048	15.2
LS 100 L	1.5	905	15.8	4.2	0.52	0.62	0.74	65	69	69	4.5	2.5	2.7	2.9	6	0.0058	20
LS 112 M	2.2	905	23.2	5.8	0.53	0.66	0.76	68	72	72	5.6	2.8	2.7	4	6	0.0087	24.2
LS 132 S	3	957	30.3	6.8	0.59	0.71	0.78	75	78	81.1	6	2	2.6	4.7	7	0.018	38.3
LS 132 M	4	961	39.6	9.3	0.56	0.66	0.75	78	83	83.6	5.9	2.5	2.9	6.4	7	0.034	53.3
LS 132 M	5.5	960	54.2	13.3	0.52	0.65	0.71	80	83.5	84.1	5.5	2.5	2.8	9.2	6	0.039	59.4
LS 160 M	7.5	967	74.1	16.1	0.63	0.74	0.79	82.6	84.8	85.2	4.7	1.5	2.1	11.1	7	0.086	81
LS 160 L	11	967	109	23.3	0.64	0.75	0.79	85	86.5	86.3	4.6	1.6	2.1	16.1	7	0.116	105
LS 180 LR	15	968	148	31.9	0.61	0.71	0.78	86.1	87.3	87.1	5.4	1.8	2.6	22.1	7	0.139	110
LS 200 LT	18.5	970	182	37	0.65	0.76	0.81	88.1	89.3	89	6.4	2.4	2.8	25.7	7	0.236	160
LS 200 L	22	972	216	43.6	0.65	0.76	0.81	89	90.1	89.9	6	2	2.7	30.2	7	0.295	190
LS 225 MR	30	968	296	59.5	0.72	0.79	0.81	89.2	90.3	89.9	6	2.2	2.5	41.2	7	0.39	235
LS 250 ME	37	978	361	71.1	0.69	0.79	0.81	92.9	93.2	92.7	6.2	2.3	2.5	49.3	7	0.85	305
LS 280 SC	45	978	439	86.5	0.69	0.79	0.81	92.9	93.2	92.7	6.2	2.3	2.5	59.9	7	0.99	340
LS 280 MC	55	978	537	106	0.72	0.79	0.81	93.1	93.3	92.6	6	2.4	2.5	73.3	7	1.19	385
LS 315 SP	75	980	731	140	0.69	0.78	0.83	92.5	93.3	93.3	7.2	2.4	3	96.9	7	3.09	690
LS 315 MP	90	980	877	164	0.76	0.83	0.85	92.4	93.1	93.1	7.2	2.4	2.9	113.7	7	3.74	760
LS 315 MR	110	980	1072	200	0.76	0.83	0.85	93	93.5	93.5	7.2	2.4	2.9	138.4	7	4.36	850
LS 315 MR	132	986	1278	242	0.72	0.8	0.83	94.3	94.9	94.8	6.6	2.4	2.5	167.8	7	4.36	830

* Torque curve

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E1 - Selection data: Single-speed



	MAIN	IS SUF	PLY 38	80 V	50 Hz	MAINS	SUPPL	Y415V	50 Hz		Can be use	SSUPPL ed from 440V	Y 460 V to 480V	60 Hz
	Rated power at 50 Hz	Rated speed	Rated current	Power factor	Efficiency	Rated speed	Rated current	Power factor	Efficiency	Rated power at 60 Hz	Rated speed	Rated current	Power factor	Efficiency
Туре	P _N kW	N _N min ⁻¹	I _N	$\text{Cos}\phi$	η %	N _N min ⁻¹	I _N A	Cos φ	η %	P _N kW	N _N min ⁻¹	I _N A	$\text{Cos}\phi$	η %
LS 63 M	0.09	840	0.47	0.84	35	880	0.46	0.80	34	0.11	1060	0.44	0.70	45
LS 71 L	0.12	910	0.62	0.59	50	925	0.67	0.53	47	0.14	1120	0.60	0.55	53
LS 71 L	0.18	850	0.82	0.67	50	895	0.82	0.60	51	0.22	1100	0.79	0.60	58
LS 71 L	0.25	830	1.09	0.71	49	890	1.05	0.64	52	0.30	1080	1	0.66	57
LS 80 L	0.25	930	0.8	0.74	64	960	0.85	0.65	63	0.30	1145	0.79	0.70	68
LS 80 L	0.37	940	1.11	0.77	67	955	1.1	0.70	66	0.45	1145	1.10	0.74	70
LS 80 L	0.55	930	1.8	0.74	64	960	1.9	0.65	63	0.66	1145	1.7	0.70	68
LS 90 S	0.75	915	2	0.81	69	935	2.1	0.73	67	0.90	1125	2.1	0.76	71
LS 90 L	1.1	895	3	0.80	70	920	3.1	0.72	69	1.3	1100	2.9	0.78	73
LS 100 L	1.5	890	4.2	0.79	69	910	4.3	0.71	69	1.8	1100	4.1	0.76	72
LS 112 M	2.2	895	5.8	0.80	72	915	5.8	0.72	73	2.6	1100	5.5	0.78	76
LS 132 S	3	948	7	0.81	80.1	960	6.8	0.76	81.1	3.6	1152	6.9	0.80	82.4
LS 132 M	4	953	9.4	0.78	83.1	965	9.2	0.73	83.4	4.8	1158	9.3	0.77	84.7
LS 132 M	5.5	953	13.5	0.74	83.7	963	13.4	0.68	83.9	6.6	1155	13.3	0.72	85.3
LS 160 M	7.5	962	16.6	0.81	84.5	972	15.9	0.77	85.2	8.6	1167	16	0.79	85.2
LS 160 L	11	962	23.9	0.81	86.3	970	23	0.77	86.4	12.5	1167	23	0.79	86.3
LS 180 LR	15	970	31.1	0.83	88.4	972	29.8	0.79	88.7	17	1172	29.7	0.81	88.7
LS 200 LT	18.5	965	38.2	0.83	88.6	975	36.4	0.79	89.6	21	1170	36.6	0.81	89
LS 200 L	22	967	44.8	0.83	89.8	975	42.9	0.79	90.3	25	1172	43.1	0.81	89.9
LS 225 MR	30	965	61.3	0.83	89.6	972	57.8	0.8	90.2	34	1168	58.6	0.81	89.9
LS 250 ME	37	974	74.3	0.82	92.3	980	69.2	0.8	93	42	1174	70	0.81	93
LS 280 SC	45	974	90.3	0.82	92.3	980	84.1	0.8	93	52	1174	86.6	0.81	93
LS 280 MC	55	974	111	0.82	92.1	980	102.8	0.8	93	63	1174	104	0.82	92.8
LS 315 SP	75	978	146	0.84	93	982	138	0.81	93.4	86	1178	138	0.84	93.4
LS 315 MP	90	976	171	0.86	92.9	982	160	0.84	93.2	103	1178	161	0.86	93.3
LS 315 MR	110	976	209	0.86	93.1	982	194	0.84	93.7	126	1178	196	0.86	93.6
LS 315 MR	132	984	252	0.84	94.7	988	239	0.81	94.9	152	1186	240	0.84	94.8

Note: For mains supplies with different voltages, see section D2.2.4.



E1 - Selection data: Single-speed



IP 55 - S1 CI. F - ∆T 80 K

					MAI	NS SI	JPPL	Y ∆ 2	30/Y4	400 V	or Δ 40	0 V 4	50 Hz				
	Rated power at 50 Hz	Rated speed	Rated torque	Rated current		Power factor			Efficiency		Starting current/ Rated current	Starting torque/ Rated torque	Max. torque/ Rated torque	Rated apparent power	Torque* curve	Moment of inertia	Weight
Туре	P _N kW	N _N min ⁻¹	C _N N.m	I _{N (400V)} A	50 %	Cos φ 75 %	100 %	50 %	η 75%	100 %	I_D/I_N	M_D/M_N	M_M/M_N	kVA _N	N°	J kg.m ²	IM B3 kg
LS 71 L	0.12	650	1.7	0.72	0.40	0.45	0.55	36	42	44	2.1	1.3	1.5	0.50	3	0.0013	8
LS 80 L	0.18	705	2.4	0.79	0.45	0.54	0.63	43	48	52	2.9	1.5	1.9	0.55	8	0.0031	9.7
LS 80 L	0.25	700	3.4	0.98	0.51	0.60	0.68	45	52	54	2.8	1.7	1.9	0.68	8	0.0041	11.3
LS 90 S	0.37	685	5.2	1.20	0.52	0.63	0.72	56	62	62	3.8	1.7	1.8	0.83	8	0.0038	13.5
LS 90 L	0.55	670	7.8	1.7	0.52	0.61	0.72	59	62	63.5	3.5	1.7	1.7	1.2	8	0.0047	15.2
LS 100 L	0.75	670	10.7	2.4	0.47	0.58	0.71	55	61.5	63.5	3.5	1.8	2.2	1.7	7	0.0047	18
LS 100 L	1.1	670	15.7	3.7	0.49	0.60	0.68	58	62.5	63	3.7	2	2.2	2.6	7	0.0068	21.8
LS 112 MG	1.5	710	20.2	4.7	0.43	0.55	0.64	62.5	69	72	3.8	2	2.1	3.3	7	0.015	24
LS 132 SM	2.2	713	30.2	6.1	0.45	0.56	0.68	71	77.5	77.1	4	1.7	2	4.2	8	0.025	45.6
LS 132 M	3	712	40.7	8	0.45	0.56	0.65	79	82.9	79.8	4.3	1.9	2.2	5.5	8	0.033	53.9
LS 160 M	4	718	53.2	11	0.43	0.55	0.63	81.3	83.4	83.3	3.9	1.7	2.3	7.6	8	0.068	84
LS 160 M	5.5	716	73.4	15.1	0.43	0.55	0.63	81.8	83.5	83.3	3.9	1.7	2.3	10.5	8	0.071	89
LS 160 L	7.5	714	100	20.6	0.43	0.55	0.63	82.6	84	83.4	3.9	1.9	2.3	14.3	8	0.09	101
LS 180 L	11	720	146	25.6	0.57	0.68	0.72	84.2	86.3	86	3.8	1.4	1.9	17.8	8	0.205	140
LS 200 L	15	725	198	32.9	0.57	0.7	0.75	86.3	87.9	87.7	4.4	1.6	2.1	22.8	8	0.27	185
LS 225 ST	18.5	725	244	42.4	0.54	0.66	0.72	86.2	87.7	87.5	4.2	1.6	2.1	29.4	8	0.33	210
LS 225 MR	22	725	290	51.9	0.51	0.63	0.7	85.1	87.2	87.4	4.4	1.9	2.3	36	8	0.4	240
LS 250 ME	30	730	392	60.3	0.63	0.73	0.79	90.1	91.2	90.9	5.8	1.9	2.7	41.8	8	0.99	330
LS 280 SC	37	730	484	74.3	0.63	0.73	0.79	90.7	91.4	91	5.6	1.8	2.6	51.5	8	1.19	370
LS 280 MD	45	728	590	91.4	0.63	0.73	0.78	91.1	91.7	91.1	5.4	1.8	2.6	63.3	8	1.39	430
LS 315 SP	55	738	712	105	0.71	0.78	0.81	92.2	93.2	93.2	5.4	1.8	2.4	72.9	8	3.1	660
LS 315 MR	75	738	970	143	0.71	0.78	0.81	93.1	93.8	93.6	5.4	1.8	2.4	98.9	8	4.38	815

For motors with a greater number of poles, see the table on page 66.

* Torque cu	rve
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section D6.1 - page 71



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E

E1 - Selection data: single-speed



					50.11-				5011-		MAINS	SUPPL	Y460V	60 Hz
	MAIN	15 501	PLY 38	50 V	50 Hz	WAINS	SUPPL	Y415V	50 Hz			ed from 440		00 HZ
	Rated power at 50 Hz	Rated speed	Rated current	Power factor	Efficiency	Rated speed	Rated current	Power factor	Efficiency	Rated power at 60 Hz	Rated speed	Rated current	Power factor	Efficiency
Туре	P _N kW	N _N min ⁻¹	I _N	$\text{Cos}\phi$	η %	N _N min ⁻¹	I _N A	$\text{Cos}\phi$	η %	P _N kŴ	N _N min ⁻¹	I _N	Cos φ	η %
LS 71 L	0.12	630	0.70	0.60	43.6	670	0.70	0.50	44					
LS 80 L	0.18	700	0.77	0.66	53.5	710	0.80	0.61	51.6	0.22	860	0.77	0.62	58
LS 80 L	0.25	695	0.83	0.75	61	705	1.03	0.62	54.5	0.30	850	0.97	0.65	59.5
LS 90 S	0.37	670	1.22	0.75	61.5	690	1.20	0.69	62	0.45	835	1.20	0.71	66.5
LS 90 L	0.55	655	1.8	0.74	62	680	1.8	0.67	64	0.66	810	1.8	0.72	66.5
LS 100 L	0.75	660	2.4	0.76	62	675	2.5	0.69	61	0.90	820	2.3	0.72	68
LS 100 L	1.1	655	3.6	0.73	63	675	3.8	0.64	62	1.3	820	3.6	0.68	67
LS 112 MG	1.5	705	4.7	0.68	71	720	4.8	0.61	72	1.8	860	4.5	0.66	76
LS 132 SM	2.2	704	6.1	0.72	76.3	716	6.1	0.65	76.6	2.6	857	6	0.69	79
LS 132 M	3	705	8.1	0.71	79.3	715	8.1	0.65	79.8	3.6	870	8	0.69	81.8
LS 160 M	4	714	11.1	0.66	82.6	722	11.1	0.6	83.4	4.6	868	10.6	0.64	85.2
LS 160 M	5.5	712	15.3	0.66	82.6	720	15.3	0.6	83.4	6.3	866	14.5	0.64	85.2
LS 160 L	7.5	708	20.6	0.67	82.7	716	20.8	0.6	83.5	8.6	862	19.5	0.65	85.2
LS 180 L	11	715	26	0.75	85.6	725	25.3	0.7	86.3	12.5	870	25.3	0.72	86
LS 200 L	15	720	34.1	0.77	86.8	725	33.2	0.72	87.2	17	875	32.4	0.75	87.7
LS 225 ST	18.5	720	43.1	0.75	87	725	42.1	0.7	87.4	21	875	41.8	0.72	87.5
LS 225 MR	22	720	52.4	0.73	87.4	730	53	0.66	86.8	25	875	51.3	0.7	87.4
LS 250 ME	30	728	62.2	0.81	90.5	732	58	0.79	91.1	34	878	56.9	0.82	91.4
LS 280 SC	37	728	76.6	0.81	90.6	732	71	0.79	91.2	42	878	70.3	0.82	91.5
LS 280 MD	45	726	94.2	0.8	90.7	730	89	0.77	91.3	52	876	89	0.8	91.7
LS 315 SP	55	736	109	0.82	93.1	740	102	0.8	93.4	63	886	104	0.81	93.5
LS 315 MR	75	736	149	0.82	93.3	740	139	0.8	93.7	86	886	142	0.81	93.8

For motors with a greater number of poles, see the table on page 66.

Note: For mains supplies with different voltages, see section D2.2.4.



E2 - Selection data: two-speed

The performance data for multi-speed motors are detailed for the most widely used models, with simplified tables giving a summary of the other available standard builds, along with modified standard builds.



IP 55 - CI. F - S1 Centrifugal applications 1 winding (Dahlander)

MAINS SUPPLY 400 V 50 Hz Rated powe Starting current / Powe Starting torque / Maximum torque Moment Rated current Efficiency Rated speed Weight at 50 Hz factor Rated current Rated torque Rated torque of inertia I_N(400 V) $M_{\rm f}/M_{\rm N}$ M_{M}/M_{N} IM B3 P_N kŴ N_N min⁻ Cos φ I_D/I_N η % Туре kg.m² kg 72 0.37 2840 1.2 0.8 4.3 2 2.4 0.00085 7.3 LS 71 M 1440 0.65 70 0.075 0.3 1.9 4.6 2.5 0.55 2830 1.4 0.85 71 4.2 1.88 2.3 0.0011 8.3 LS 71 L 1430 69 0.11 0.35 0.7 4.5 1.7 2.4 1.1 2810 2.5 0.87 72 5.2 2 2.27 0.0042 10.9 1 \$ 80 1 0.25 1420 0.66 0.78 70 4.6 1.9 1.95 1.5 2810 3.7 0.86 68.5 4.2 1.77 1.99 0.0039 14 LS 90 S 0.35 1440 0.8 0.81 75.7 1.76 2.12 5.4 2.2 2840 42 0.87 74 52 1.95 2.01 0.0049 15.2 LS 90 L 0.6 1420 0.84 75.6 1.4 4.4 1.71 1.98 3 2885 6.5 0.85 78.8 6.3 2.26 2.37 0.0062 24.5 LS 100 L 0.8 1440 1.7 0.82 80.2 5.9 2.15 2.38 2915 9.4 81.6 2.25 0.015 37 4.5 0.85 6.9 2.53 LS 112 MU 1.3 1450 2.8 0.81 82.2 5.7 2.11 2.51 0.0334 6 2890 13.1 0.85 78 5.7 2.04 2.26 50 LS 132 SM 1450 0.83 81.6 1.6 3.4 5.6 1.82 2.46 9 2920 18.7 0.85 82.4 7.8 2.42 2.52 0.0385 60 LS 132 M 0.82 2.5 1450 5.2 84.6 6.7 2.03 2.78 13.5 2935 24.8 0.89 88.2 8 2.3 3.2 0.068 85 LS 160 M 3.3 1469 6.4 0.85 86.9 6.9 2.2 3.1 19 2936 34.9 0.88 89.3 7.8 2.5 3.1 0.085 97 LS 160 L 4.5 1470 0.84 89.7 8.6 7.4 2.5 3.2 24 2955 45 0.87 88.5 8.7 2.8 3.4 0.137 147 LS 180 LU 8 1470 14.5 0.89 89.5 5.8 2.3 2.3 31 2955 55.9 0.91 88 8 2.4 3 0.240 200 LS 200 L 1465 20.2 0.89 88.5 5.2 1.9 11 1.6 2.8 0.270 40 2955 71.3 0.9 90 8 3.2 228 LS 200 LU 14 1465 25.1 0.88 91.5 5.2 1.7 2.1 50 2970 87.2 92 2.6 3.5 0.633 320 0.9 8.8 LS 225 MG 17 1476 30.9 0.86 92.2 5.5 2.1 2.2 59 2970 103 0.9 92 8.8 2.6 3.5 0.73 340 LS 250 ME 1476 0.86 92.2 20 36.4 5.5 2.1 2.2 70 2970 122 0.9 92 8.8 2.6 3.5 0.83 380 LS 250 ME 0.86 24 43.7 92.2 1476 5.5 2.1 2.2 85 2970 148 0.9 92 8.8 2.6 3.5 1.03 450 LS 280 MD 30 1476 54.6 0.86 92.2 5.5 2.1 2.2 2975 0.92 2.79 750 100 168 93.3 8.5 2.5 3.3 LS 315 MP 35 1485 60.9 0.88 94.3 5.5 2.1 2.1

The top line for each type corresponds to the highest rated speed.

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Note: - For mains supplies with different voltages, see section D2.2.4. - Applies to all the two-speed motor tables.

2975

1485

198

69.6

0.92

0.88

93.3

94.3

8.5

5.5

2.5

2.1

3.3

2.1

3.27

845



LS 315 MR

E2 - Selection data: two-speed



IP 55 - CI. F - S1 Centrifugal applications 2 separate windings*

					MAINS S	UPPLY 400 V	50 Hz			
	Rated power at 50 Hz	Rated speed	Rated current	Power factor	Efficiency	Starting current / Rated current	Starting torque / Rated torque	Maximum torque / Rated torque	Moment of inertia	Weight
Туре	P _N kW	N _N min ⁻¹	I _N (400 V) A	$\text{Cos}\phi$	η %	I_D/I_N	M_D/M_N	$M_{\rm M}/M_{\rm N}$	J kg.m²	IM B3 kg
LS 71 L	0.25	1430	0.75	0.78	66	3.9	1.4	1.9	0.0011	8.3
-571L	0.09	960	0.55	0.64	40	2.3	1.2	1.9		
S 80 L	0.7	1435	2.1	0.73	67	4.5	1.8	2	0.0024	11.5
.3 00 L	0.2	945	1.05	0.72	40	2.5	1.1	1.4		
S 90 S	0.85	1430	2.2	0.78	70	5.5	2	2.4	0.0032	14
.0.00	0.25	930	0.85	0.79	55	3.5	1.2	1.6		
S 90 L	1.4	1425	3.5	0.79	73	6	2.2	2.6	0.0049	17
0.00	0.5	925	1.4	0.80	61	3.6	1.3	1.7		
S 100 L	2.4	1425	5.9	0.80	73.9	6	2.4	2.6	0.0071	25
.0 100 L	0.75	940	2.1	0.71	66.8	4.3	2.2	2.3		
S 112 MG	3.4	1460	8.7	0.72	78	6.9	2.4	2.7	0.015	30
0 112 110	1.1	965	3.4	0.75	64	4	1.3	2		
S 132 SM	4	1452	8.1	0.86	82.8	6.3	2.1	2.1	0.025	44
0 102 014	1.2	972	3	0.76	76.9	4.6	2	1.7		
S 132 M	6.3	1459	13.2	0.82	83.9	7.4	2.8	2.7	0.033	55
3 132 W	1.9	974	4.6	0.77	76.9	5.5	2.3	1.9		
S 160 M	9	1465	18.8	0.81	85.2	7	2.1	3.1	0.057	75
3 100 W	3	975	7.8	0.74	74.9	5.2	1.6	2.4		
S 160 M	11	1465	22.6	0.82	85.7	7.4	2.1	3.1	0.068	85
3 100 W	3.7	975	9.3	0.74	77.8	5.5	1.7	2.6		
S 160 L	13	1465	25.6	0.84	87.3	7.8	2.3	3.2	0.085	97
3 100 L	4.3	970	10.5	0.75	78.6	5.5	1.7	2.5		
S 160 LU	15	1465	29.3	0.84	87.9	7.5	2.4	3	0.096	109
3 100 20	5	970	12.1	0.76	78.8	5.1	1.8	2.2		
S 180 L	18.5	1460	34.1	0.88	89	5.5	2	2.3	0.123	136
3 100 L	6.5	980	14.8	0.78	81	5	2	2.2		
S 180 LU	22	1470	41.5	0.86	89	6.8	2.6	2.7	0.147	155
3 100 20	7.5	980	16.6	0.8	81.5	4.8	2	2		
S 200 L	25	1475	46.9	0.85	90.5	6.4	2.2	2.5	0.24	200
02001	8.5	985	19.3	0.77	82.5	4.8	2	2		
S 200 LU	30	1475	56	0.85	91	6	2.2	2.5	0.27	228
0 200 20	9	985	20.8	0.74	84.5	5.3	2.4	2.3		
S 225 SR	34	1475	63.8	0.84	91.6	6.3	2.3	2.6	0.29	235
	11	985	25.9	0.73	84	5.1	2.3	2.2		
S 250 ME	42	1480	77.7	0.85	91.8	6.5	2.5	2.7	0.83	380
	14	985	31.8	0.73	87	5.1	2.7	2.4		
S 250 MF	52	1480	96	0.85	92	6.5	2.5	2.7	1.03	450
	19	985	43.2	0.73	87	5.1	2.7	2.4		
S 280 SK	75	1485	134.6	0.86	93.5	7.7	2.1	2.7	1.89	610
	28	985	56.3	0.8	89.7	6.6	2.9	2.4		
S 280 MK	90	1485	161.2	0.86	93.7	7.7	2.3	2.9	2.23	665
	33	985	66.2	0.8	90	6.9	2.9	2.4		
S 315 SP	110	1485	198.9	0.85	93.9	8	2.7	2.9	2.64	750
	37	985	74.1	0.8	90.1	6.9	2.9	2.4		
S 315 MR	132	1485	244.2	0.83	94	9.2	3.1	3.3	3.27	860
C C I C IIII	44	985	88	0.8	90.2	7.1	2.9	2.4		

The top line for each type corresponds to the highest rated speed.

* LS 80 to LS 132, 1 winding (PAM), see section E2 page 98.



E2 - Selection data: two-speed



IP 55 - CI. F - S1 Centrifugal applications LS 80 L to LS 132 M: 1 winding (PAM)

MAINS SUPPLY 400 V 50 Hz

	Rated power at 50 Hz	Rated speed	Rated current	Power factor	Efficiency	Starting current / Rated current	Starting torque / Rated torque	Maximum torque / Rated torque	Moment of inertia	Weight
Туре	P _N kW	N _N min ⁻¹	I _N (400 V) A	$\text{Cos}\phi$	η %	I _D /I _N	M_D/M_N	M _M /M _N	J kg.m ²	IM B3 kg
LS 80 L	0.75	1400	1.8	0.87	67	3.8	1.1	1.5	0.0042	10.9
13 80 L	0.25	905	0.9	0.88	46	2.1	1	1.2		
LS 90 S	1.1	1420	2.6	0.79	77	6	2.5	2.5	0.0039	12.5
_3 90 3	0.37	940	1.5	0.63	57	3.3	1.4	1.8		
LS 90 L	1.5	1425	3.6	0.8	78	6.1	2.5	2.6	0.0049	15.2
13 90 L	0.55	940	2.2	0.64	57	3.3	1.4	1.9		
.S 100 L	2.2	1400	4.8	0.86	77	6.8	3.2	2.8	0.0039	21
-5 100 L	0.75	940	2.3	0.75	63	4.2	1.6	2.1		
_S 100 L	3	1410	6.7	0.84	77	6.6	3	2.7	0.0051	24.5
-5 100 L	1.1	940	3.2	0.76	65	4.4	1.4	2.1		
S 442 MC	4	1450	9	0.78	82	7	1.9	2.6	0.015	35
_S 112 MG	1.5	965	4.7	0.70	67	3.6	1.1	1.8		
_S 132 SM	5.5	1460	11.7	0.82	84	6.4	2.8	2.8	0.0334	50
-3 132 3W	1.8	975	6.2	0.62	69	4	1.7	2.2		
C 422 M	7.5	1445	15.5	0.84	83	7	2.2	2.6	0.0385	60
LS 132 M	2.5	970	7.4	0.70	70	4.4	1.4	2		

The top line for each type corresponds to the highest rated speed.



E2 - Selection data: two-speed



IP 55 - CI. F - S1 Centrifugal applications 1 winding (Dahlander)

MAINS SUPPLY 400 V 50 Hz Rated powe Powe Starting current / Starting torque / Maximum torque Moment Rated speed Efficiency Rated current Weight at 50 Hz factor Rated current Rated torque Rated torque of inertia I_N(400 V) $M_{\rm f}/M_{\rm N}$ M_{M}/M_{N} IM B3 P_N kŴ N_N min⁻ Cos φ I_D/I_N η % Type kg.m² kg 0.25 1430 0.8 0.7 65 3.5 1.3 2 0.00085 7.3 LS 71 L 0.06 640 38 1.3 0.4 0.6 1.5 1.1 0.37 1430 1.15 0.8 60 4 1.4 2.1 0.0011 8.3 LS 71 L 0.07 670 0.5 0.7 30 2.1 1.2 1.4 0.0018 9.3 1435 2.6 2.4 0.55 0.71 69 1.6 4.8 LS 80 L 0.09 715 0.6 0.48 46 2.3 2.8 2.4 0.75 1425 2.3 0.72 65 4.8 2.3 2.3 0.0024 10.9 LS 80 L 710 41 0.12 0.9 0.52 2.3 2.7 2.3 1.1 1441 3 0.78 67.5 4.1 1.1 1.5 0.0032 11.5 LS 90 S 0.18 724 11 0.53 43 5 29 15 23 1.5 1459 4.2 0.70 73.4 5.5 1.9 2.5 0.0049 15.2 LS 90 L 0.25 732 0.44 50.5 2.8 1.6 3.6 3.1 2.2 1446 5.5 0.78 73.6 5.2 1.7 2.1 0.0051 21 LS 100 L 0.37 726 2 0.50 53.7 2.4 3.2 3 1435 7.4 0.79 75 5.5 1.6 2.3 0.0071 24.4 3 LS 100 L 0.55 715 2.6 0.52 58 2.7 2.1 2.1 1455 8.7 0.80 82.9 6.7 2.1 2.6 0.015 37 LS 112 MU 0.75 0.47 730 3.5 66 3.6 2.9 3.3 0.0334 5.5 1452 11 0.87 83.3 6.4 2 2.3 55 LS 132 SM 726 3.2 0.63 78 3.7 1.1 2 1.9 7.5 1449 14.7 0.88 83.7 6.3 2 2.3 0.0385 60 LS 132 M 1.5 727 4.3 0.63 79 4.1 2 2.2 9 1462 17.9 0.84 86.4 6.4 1.9 2.8 0.057 75 LS 160 M 2.2 79.2 724 6.3 0.64 1.4 2.2 3.7 11 1464 21.6 0.84 87.5 7.2 2.1 3 0.068 85 LS 160 M 2.8 724 0.64 80.9 2.2 7.7 3.7 1.5 13 1464 25.8 0.83 87.5 6.9 2.1 2.9 0.074 89 LS 160 L 3.3 722 9.1 0.63 80.5 3.7 1.5 2.1 15 1462 29.5 0.84 87.5 6.8 2.3 2.8 0.085 97 LS 160 L 722 10.1 0.64 80.5 3.8 1.4 2 3.4 18.5 1462 36.6 0.83 87.9 72 24 3 0.096 112 LS 180 LR 0.64 4.8 722 12.1 81.5 3.6 1.4 2 22 1464 40.9 0.87 89.2 2.1 2.4 0.135 150 6 LS 180 LU 5.3 730 13.2 0.68 85.5 3.6 1.8 1.7 24 1468 45.2 0.85 90.1 2.8 2.8 0.151 165 7.1 LS 200 LT 15.4 0.65 86.6 6 730 3.7 2.1 1.8 30 1475 55.8 0.86 90.3 61 2.1 24 0 240 200 LS 200 L 735 18.6 0.63 86 1.9 1.8 7 3.8 37 1475 69.2 90.8 2.3 2.7 0.290 235 0.85 6.8 LS 225 SR 0.64 8.5 735 21.8 88 4 2.1 1.8 45 1482 83.1 0.85 92 7 2.3 3 0.633 320 LS 225 MG 738 26.3 0.66 91.3 1.8 1.8 11 4 55 1484 100.8 0.85 92.7 7.7 2.6 3.4 0.83 380 LS 250 ME 14 738 33.1 0.66 92.4 1.8 1.9 4 65 1484 118.7 0.85 7.7 2.6 3.4 0.9 430 93 LS 250 MF 16 738 37.7 0.66 92.8 4 1.8 1.9 75 1484 136.9 0.85 7.7 2.6 3.4 1.03 450 93 LS 280 SD 738 45.5 0.65 92.8 19 3.9 1.7 1.8 90 1490 163.3 0.85 93.6 8.3 2.8 3.1 2.32 655 LS 280 MK 23 742 54.8 0.64 91.3 2.3 4.8 1.9 110 1490 93.8 2.8 2.9 2.79 750 199.1 0.85 8.3 LS 315 SP 29 742 69 0.64 91.3 48 23 19 132 1490 238.5 0.85 8.3 2.8 2.9 3.27 845 94 LS 315 MR 742 0.64 91.5 2.2 35 86 4.9 160 1485 288.4 0.85 94.2 8.3 2.8 2.9 3.27 860 LS 315 MR 42 740 103 0.65 91.7 5 2.2 2

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The top line for each type corresponds to the highest rated speed.



E2 - Selection data: two-speed



IP 55 - CI. F - S1 Centrifugal applications 1 winding (Dahlander)

					MAINS SU	JPPLY 400 V	50 Hz			
	Rated power at 50 Hz	Rated speed	Rated current	Power factor	Efficiency	Starting current / Rated current	Starting torque / Rated torque	Maximum torque / Rated torque	Moment of inertia	Weight
Туре	P _N kW	N _N min ⁻¹	I _N (400 V) A	$\text{Cos}\phi$	η %	I _D /I _N	M_D/M_N	M,/M,	J kg.m²	IM B3 kg
LS 90 L	0.75	910	2.1	0.82	64	3.8	1.6	2	0.0039	15
	0.15	425	0.8	0.68	42	2.1	1.6	1.8		
LS 90 LU	1.1	915	3.2	0.77	65	4.2	2.3	2.7	0.0051	17
20 00 20	0.18	450	1.2	0.54	40	2.3	2.7	3		
LS 100 L	1.5	915	4	0.79	68	4.5	1.9	1.8	0.0071	25
	0.25	450	1.5	0.55	44	2.4	2.3	2.6		
LS 112 MU	2.2	950	5.6	0.79	71	4.5	1.4	1.9	0.0177	37
L3 112 WIO	0.37	465	2.1	0.52	50	2.1	1.1	1.6		
LS 132 SM	3	955	8	0.70	77	4.5	2.2	2	0.028	55
L3 132 3W	0.55	465	3.8	0.43	58	2.4	1.7	1.6		
LS 132 M	4	955	10.4	0.71	77	4.8	2	2.2	0.033	60
_3 132 W	0.65	465	3.1	0.45	58	2	1.53	1.36		
LS 132 MU	5.5	950	14.1	0.71	79	4.9	2.1	2.3	0.046	68
L3 132 WIO	1	450	5.4	0.45	59	1.9	1.5	1.4		
S 460 M	7.5	975	17.5	0.77	80.5	5	1.5	2.3	0.093	86
LS 160 M	1.3	485	5.5	0.51	66.6	2.4	1.3	1.6		
LS 160 LU	11	975	26.2	0.73	82.9	5.5	1.9	2.6	0.151	108
LS 160 LU	1.8	485	8	0.45	71.8	2.9	1.7	2.1		
LS 180 LU	15	975	33.4	0.76	85.4	6	2.1	2.6	0.214	146
L3 100 LU	2.5	485	10.4	0.46	75.2	2.8	1.9	1.9		
6 200 1	18.5	980	38.2	0.80	87.4	6.1	2	2.6	0.324	205
_S 200 L	3	488	11.5	0.52	72.4	2.9	1.4	1.8		
6 200 1 11	25	980	52.2	0.79	87.5	7	2.3	3	0.38	235
LS 200 LU	4.5	485	16.6	0.54	72.4	2.7	1.3	1.8		

The top line for each type corresponds to the highest rated speed.



E2 - Selection data: two-speed

General table of two-speed motors

IP 55 - CI. F - S1 Centrifugal applications

MAINS SUPPLY \(\triangle 400 V \) 50 Hz

Туре	2/4 Poles Dahlander	4/6 Poles PAM	4/6 Poles 2 windings	4/8 Poles Dahlander	6/12 Poles Dahlander								
	P _N kW	P_ kW	P kW	P_ kW	P _N kW								
LS 71 M	0.37/0.075	-	-	0.25/0.06	-								
LS 71 M	0.55/0.11	-	-	0.37 / 0.07	-								
LS 80 L	-	-	-	0.55/0.09	-								
LS 80 L	1.1/0.25	0.75/0.25	0.7/0.2	0.75/0.12	-								
LS 90 S	1.5/0.35	-	0.85/0.25	1.1/0.18	-								
LS 90 SL	-	1.1/0.37	-	-	-								
LS 90 L	2.2/0.6	1.5/0.55	1.4 / 0.5	1.5/0.25	0.75/0.15								
LS 90 LU	-	-	-	-	1.1/0.18								
LS 100 L	-	2.2/0.75	2.4 / 0.75	2.2/0.37	1.5 / 0.25								
LS 100 L	3/0.8	3/1.1	-	3 / 0.55	-								
LS 112 MG	-	-	3.4 / 1.1	-	-								
LS 112 MU	4.5/1.3	4/1.5	-	4/0.75	2.2/0.37								
LS 132 SM	6/1.6	5.5/1.8	4/1.2	5.5/1.1	3 / 0.55								
LS 132 M	9/2.5	7.5/2.5	6.3/1.9	7.5/1.5	4 / 0.65								
LS 132 MU	-	-	-	-	5.5/1								
LS 160 M	-	-	9/3	9/2.2	7.5/1.3								
LS 160 M	13.5 / 3.3	-	11 / 3.7	11 / 2.8	-								
LS 160 L	19/4.5	-	13 / 4.3	13 / 3.3	-								
LS 160 L	-	-	-	15 / 3.8	-								
LS 160 LU	-	-	15/5	-	11 / 1.8								
LS 180 L	-	-	18.5 / 6.5	18.5 / 4.8	-								
LS 180 LU	24 / 8	-	22/7.5	22 / 5.3	15/2.5								
LS 200 LT	-	-	-	24 / 6	-								
LS 200 L	31 / 11	-	25 / 8.5	30 / 7	18.5/3								
LS 200 LU	40 / 14	-	30 / 9	-	25/4.5								
LS 225 SR	-	-	34 / 11	37 / 8.5	-								
LS 225 MG	50/17	-	-	45 / 11	-								
LS 250 ME	59/20	-	42/14	55 / 14	-								
LS 250 ME	70/24	-	-	-	-								
LS 250 MF	-	-	52/19	65/16	-								
LS 280 SD	-	-	-	75/19	-								
LS 280 SK	-	-	75/28	-	-								
LS 280 MD	85/30		-	-									
LS 280 MK	-	-	90/33	90/23									
LS 315 SP	-	-	110/37	110 / 29	-								
LS 315 MP	-	-	-	132 / 35	-								
LS 315 MR	100 / 35	-	132 / 44	160 / 42	-								

The specific electrical characteristics for these motors are available on request.

The characteristics tables detail intermediate powers which are not described in the above table.



E2 - Selection data: two-speed

General table of two-speed motors

IP 55 - CI. F - S1 General applications

MAINS SUPPLY \(\triangle 400 V \) 50 Hz

Туре	2/4 Poles Dahlander	2/4 Poles 2 windings	2/6 Poles 2 windings	2/8 Poles 2 windings	4/6 Poles 2 windings	4/8 Poles Dahlander
	P _N kW	P _N kW	P _N kW	P _N kW	P _N kW	P _N kW
LS 71 M	-	-	-	0.18/0.045	0.12/0.09	-
LS 71 M			-	0.25 / 0.06	0.18/0.12	
LS 71 M	0.37 / 0.25		-	0.37 / 0.09	-	0.25/0.12
LS 71 M	0.55 / 0.37		-	0.55 / 0.18	-	0.37 / 0.18
LS 71 L		0.37/0.09	0.25/0.08	-	-	-
LS 80 L	1.1/0.75	-	0.55/0.18	0.55/0.12	0.45 / 0.3	0.55 / 0.22
LS 90 S	1.5 / 1.1	0.75/0.37	0.75/0.25	0.75/0.18	0.7/0.45	0.75/0.4
LS 90 L	2.2 / 1.5		1.5/0.5	-	1.1/0.75	1.2/0.6
LS 90 LU	-	-	-	1.5 / 0.37	-	-
LS 100 L	3/2.6	2.2/1.1	2.2/0.75	2.2/0.55	1.8/1.2	1.7 / 0.9
LS 112 MG	4.5/3.7	3.3/1.7	-	3/0.75	2.8/1.8	2.8 / 1.5
LS 112 MU	5.5/4		3/1	-	3/2	3 / 1.8
LS 132 SM	6/4.5	3.7 / 1.85	4 / 1.3	4 / 1	4/2.8	5/2.85
LS 132 M	9/6.9	6/3	6.5/2.2	5.5 / 1.6	5.5/3.7	7.6/4
LS 160 M	13.5 / 10.3	-	-	-	5.9/3.9	8.1/4.5
LS 160 L	18.5 / 14		-	-	8.1/5.2	11/6
LS 180 LR	21 / 16		-	-	12/7.7	-
LS 180 L	-	-	-	-	14 / 9	14.5/9
LS 180 LU	25 / 19	-	-	-	-	16.5 / 11
LS 200 LT			-	-	-	18.5 / 12.5
LS 200 L	33/25		-	-	17 / 11.5	-
LS 200 L			-	-	21/14	22 / 15
LS 225 MR	37 / 26.5		-	-	24 / 16	-
LS 225 MG	44 / 33			-	28/18.5	28 / 19.5
LS 250 ME	52 / 40.5		-	-	33/22	-
LS 250 MF	-	-	-	-	39/22.5	40 / 26
LS 250 MF	-	-	-	-	45/30	50 / 33
LS 280 SC	62.5 / 51.5	-	-	-	-	-
LS 280 SD					-	55 / 37
LS 280 MD	81 / 66	-	-	-	-	-
LS 280 MK	-	-	-	-	55 / 40	66 / 45
LS 315 SP	-	-	-	-	62.5/42	80 / 50
LS 315 MR	95 / 78	-	-	-	78/51.5	95 / 60

The specific electrical characteristics for these motors are available on request.



	PAGES
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F5 - Foot and face mounted IM B34 (IM 2101)	108

F6 - Face mounted IM B14 (IM 3601)

The dimensions in the tables are valid for all operating positions defined on page 27.

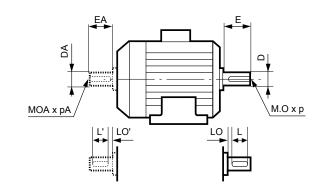


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F1 - Dimensions of shaft extensions

Dimensions in millimetres







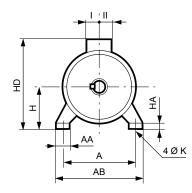
								Ма	in shaft	extensi	ons									
Туре				4,6	and 8 po	oles				2 and 2/4 poles										
	F	GD	D	G	E	0	р	L	LO	F	GD	D	G	E	0	р	L	LO		
LS 56 M	3	3	9j6	7	20	4	10	16	3	3	3	9j6	7	20	4	10	16	3		
LS 63 M	4	4	11j6	8,5	23	4	10	18	3,5	4	4	11j6	8,5	23	4	10	18	3,5		
LS 71 L	5	5	14j6	11	30	5	15	25	3,5	5	5	14j6	11	30	5	15	25	3,5		
LS 80 L	6	6	19j6	15,5	40	6	16	30	6	6	6	19j6	15,5	40	6	16	30	6		
LS 90 S/L/LU/SL	8	7	24j6	20	50	8	19	40	6	8	7	24j6	20	50	8	19	40	6		
LS 100 L	8	7	28j6	24	60	10	22	50	6	8	7	28j6	24	60	10	22	50	6		
LS 112 M/MG/MU	8	7	28j6	24	60	10	22	50	6	8	7	28j6	24	60	10	22	50	6		
LS 132 S/M/SM	10	8	38k6	33	80	12	28	63	10	10	8	38k6	33	80	12	28	63	10		
LS 160 M/L/LU/MP/LR	12	8	42k6	37	110	16	36	100	6	12	8	42k6	37	110	16	36	100	6		
LS 180 MT/LR/L/LU	14	9	48k6	42,5	110	16	36	98	12	14	9	48k6	42,5	110	16	36	98	12		
LS 200 LT/L/LU	16	10	55m6	49	110	20	42	97	13	16	10	55m6	49	110	20	42	97	13		
LS 225 ST/MT/MR/SR/MG	18	11	60m6	53	140	20	42	126	14	16	10	55m6	49	110	20	42	97	13		
LS 250 MZ/ME/MF	18	11	65m6	58	140	20	42	126	14	18	11	60m6	53	140	20	42	126	14		
LS 280 SC/SD/MC/MD	20	12	75m6	67,5	140	20	42	125	15	18	11	65m6	58	140	20	42	126	14		
LS 280 SK/MK	20	12	75m6	67,5	140	20	42	125	15	18	11	65m6	58	140	20	42	126	14		
LS 315 SP/MP/MR	22	14	80m6	71	170	20	42	155	15	18	11	65m6	58	140	20	42	126	14		

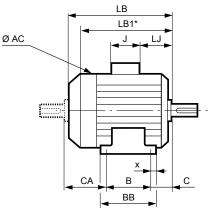
								Secon	dary sh	aft exte	nsions									
Туре				4, 6	and 8 pc	oles				2 and 2/4 poles										
	FA	GF	DA	GB	EA	OA	pА	L'	LO'	FA	GF	DA	GB	EA	OA	pА	L'	LO'		
LS 56 M	3	3	9j6	7	20	4	10	16	3	3	3	9j6	7	20	4	10	16	3		
LS 63 M	4	4	11j6	8,5	23	4	10	18	3,5	4	4	11j6	8,5	23	4	10	18	3,5		
LS 71 L	5	5	14j6	11	30	5	15	25	3,5	5	5	14j6	11	30	5	15	25	3,5		
LS 80 L	5	5	14j6	11	30	5	15	25	3,5	5	5	14j6	11	30	5	15	25	3,5		
LS 90 S/L/LU/SL	6	6	19j6	15,5	40	6	16	30	6	6	6	19j6	15,5	40	6	16	30	6		
LS 100 L	8	7	24j6	20	50	8	19	40	6	8	7	24j6	20	50	8	19	40	6		
LS 112 M/MG/MU	8	7	24j6	20	50	8	19	40	6	8	7	24j6	20	50	8	19	40	6		
LS 132 S/M/SM	8	7	28j6	24	60	10	22	50	6	8	7	28j6	24	60	10	22	50	6		
LS 160 M/L/LU/MP/LR	12	8	38k6	37	80	16	36	100	6	12	8	38k6	37	80	16	36	100	6		
LS 180 MT/LR/L/LU	14	9	48k6	42,5	110	16	36	98	12	14	9	48k6	42,5	110	16	36	98	12		
LS 200 LT/L/LU	16	10	55m6	49	110	20	42	97	13	16	10	55m6	49	110	20	42	97	13		
LS 225 ST/MT/MR/SR/MG	18	11	60m6	53	140	20	42	126	14	16	10	55m6	49	110	20	42	97	13		
LS 250 MZ/ME/MF	18	11	60m6	53	140	20	42	126	14	18	11	60m6	53	140	20	42	126	14		
LS 280 SC/SD/MC/MD	18	11	65m6	58	140	20	42	126	14	18	11	65m6	58	140	20	42	126	14		
LS 280 SK/MK	20	12	75m6	67,5	140	20	42	125	15	18	11	65m6	58	140	20	42	126	14		
LS 315 SP/MP/MR	22	14	80m6	71	170	20	42	155	15	18	11	65m6	58	140	20	42	126	14		



F2 - Foot mounted IM B3 (IM 1001)

Dimensions in millimetres





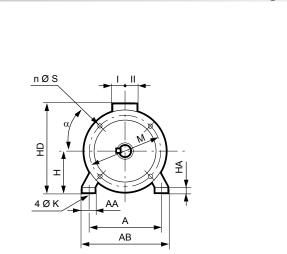
T	Main dimensions A AB B BC X AA H AC HD LB LB1* LJ J II C/																		
Туре	А	AB	В	BB	С	Х	AA	К	HA	Н	AC	HD	LB	LB1*	LJ	J	I	II	CA
LS 56 M	90	104	71	87	36	8	24	6	7	56	110	140	156	134	16	86	43	43	51
LS 63 M	100	115	80	96	40	8	26	7	9	63	124	152	172	165	26	86	43	43	55
LS 71 L	112	126	90	106	45	8	24	7	9	71	140	170	193	166	21	86	43	43	61
LS 80 L	125	157	100	120	50	10	29	9	10	80	170	203	215	177	26	86	43	43	68
LS 80 LU	125	157	100	120	50	10	29	9	10	80	170	203	267	232	26	86	43	43	120
LS 90 S	140	172	100	120	56	10	37	10	11	90	190	223	218	177	26	86	43	43	66
LS 90 L/SL	140	172	125	162	56	28	37	10	11	90	190	223	245	204	26	86	43	43	68
LS 90 LU	140	172	125	162	56	28	37	10	11	90	190	223	265	230	26	86	43	43	88
LS 100 L	160	196	140	165	63	12	40	12	13	100	200	238	290	250	26	86	43	43	93
LS 112 M	190	220	140	165	70	12	45	12	14	112	200	250	290	250	26	86	43	43	86
LS 112 MG	190	220	140	165	70	12	52	12	14	112	235	260	315	265	36	86	43	43	110
LS 112 MU	190	220	140	165	70	12	52	12	14	112	235	260	334	288	36	86	43	43	130
LS 132 S	216	250	140	170	89	16	50	12	15	132	235	280	350	306	53	86	43	43	128
LS 132 SM/M	216	250	178	208	89	16	59	12	18	132	280	307	387	327	25	110	57	73	126
LS 132 MU	216	250	178	208	89	16	59	12	18	132	280	307	410	351	25	110	57	73	148
LS 160 MP	254	294	210	294	108	20	64	14,5	25	160	315	368	468	407	44	134	92	63	154
LS 160 M	254	294	210	294	108	20	60	14,5	25	160	316	395	495	435	44	134	92	63	182
LS 160 LR	254	294	254	294	108	20	64	14,5	25	160	315	368	495	440	44	134	92	63	138
LS 160 L	254	294	254	294	108	20	60	14,5	25	160	316	395	495	435	44	134	92	63	138
LS 160 LU	254	294	254	294	108	20	60	14,5	25	160	316	395	510	450	44	134	92	63	153
LS 180 MT	279	324	241	316	121	20	79	14,5	28	180	316	428	495	435	45	205	100	95	138
LS 180 LR	279	324	279	316	121	20	79	14,5	28	180	316	428	520	450	45	205	100	95	125
LS 180 L	279	339	279	329	121	25	86	14,5	25	180	350	435	552	481	54	205	100	95	159
LS 180 LU	279	339	279	329	121	25	86	14,5	25	180	350	435	593	508	54	205	100	95	199
LS 200 LT	318	378	305	365	133	30	108	18,5	30	200	350	455	599	514	60	205	100	95	167
LS 200 L	318	388	305	375	133	35	103	18,5	36	200	390	475	621	539	68	205	100	95	194
LS 200 LU	318	388	305	375	133	35	103	18,5	36	200	390	475	669	586	68	205	100	95	244
LS 225 ST	356	431	286	386	149	50	127	18,5	36	225	390	500	627	545	74	205	100	95	203
LS 225 SR	356	431	286	386	149	50	127	18,5	36	225	390	500	676	593	74	205	100	95	253
LS 225 MT	356	431	311	386	149	50	127	18,5	36	225	390	500	627	545	74	205	100	95	178
LS 225 MR	356	431	311	386	149	50	127	18,5	36	225	390	500	676	593	74	205	100	95	228
LS 225 MG	356	420	311	375	149	30	65	18,5	30	225	479	629	810	716	68	292	148	180	360
LS 250 MZ	406	470	349	449	168	70	150	24	47	250	390	550	676	593	68	217	103	145	171
LS 250 ME	406	470	349	420	168	35	90	24	36	250	479	655	810	716	68	292	148	180	303
LS 250 MF	406	470	349	420	168	35	90	24	36	250	479	655	870	776	68	292	148	180	363
LS 280 SC	457	520	368	478	190	35	90	24	35	280	479	685	810	716	68	292	148	180	262
LS 280 SD	457	520	368	478	190	35	90	24	35	280	479	685	870	776	68	292	148	180	322
LS 280 SK	457	533	368	495	190	40	85	24	35	280	586	746	921	819	99	292	148	180	379
LS 280 MC	457	520	419	478	190	35	90	24	35	280	479	685	810	716	68	292	148	180	211
LS 280 MD	457	520	419	478	190	35	90	24	35	280	479	685	870	776	68	292	148	180	271
LS 280 MK	457	533	419	495	190	40	85	24	35	280	586	746	921	819	99	292	148	180	328
LS 315 SP	508	594	406	537	216	40	114	28	70	315	586	781	947	845	125	292	148	180	341
LS 315 MP	508	594	457	537	216	40	114	28	70	315	586	781	947	845	125	292	148	180	290
LS 315 MR	508	594	457	537	216	40	114	28	70	315	586	781	1017	915	125	292	148	180	360

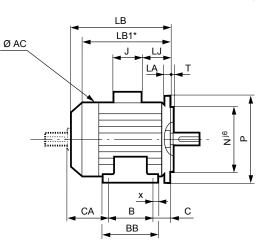
* LB1: non-ventilated motor



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F3 - Foot and flange mounted IM B35 (IM 2001)





Dimensions in millimetres

Type								-		/ain di		-			-	-	-			
	A	AB	В	BB	С	Х	AA	K	HA	Н	AC	HD	LB	LB1*	HJ	LJ	J	1	11	Sym.
LS 56 M	90	104	71	87	36	8	25	6	7	56	110	140	156	134	84	16	86	43	43	FF 100
LS 63 M	100	115	80	96	40	8	26	7	9	63	124	152	172	165	89	26	86	43	43	FF 115
LS 71 L	112	126	90	106	45	8	24	7	9	71	140	170	193	166	99	26	86	43	43	FF 130
LS 80 L	125	157	100	120	50	10	29	9	10	80	170	203	215	177	123	26	86	43	43	FF 165
LS 80 LU	125	157	100	120	50	10	29	9	10	80	170	203	267	232	123	26	86	43	43	FF 165
LS 90 S	140	172	100	120	76	10	37	10	11	90	190	223	238	197	133	46	86	43	43	FF 165
LS 90 L/SL	140	172	125	162	76	8	37	10	11	90	190	223	265	224	133	46	86	43	43	FF 165
LS 90 LU	140	172	125	162	76	28	37	10	11	90	190	223	285	250	133	46	86	43	43	FF 165
LS 100 L	160	196	140	165	63	12	40	12	13	100	200	238	290	250	138	26	86	43	43	FF 215
LS 112 M	190	220	140	165	70	12	45	12	14	112	200	250	290	250	138	26	86	43	43	FF 215
LS 112 MG	190	220	140	165	70	12	52	12	14	112	235	260	315	265	148	36	86	43	43	FF 215
LS 112 MU	190	220	140	165	70	12	52	12	14	112	235	260	334	288	148	36	86	43	43	FF 215
LS 132 S	216	250	140	170	89	16	50	12	15	132	235	280	350	306	148	53	86	43	43	FF 265
LS 132 SM/M	216	250	178	208	89	16	59	12	18	132	280	307	387	327	175	25	110	57	73	FF 265
LS 132 MU	216	250	178	208	89	16	59	12	18	132	280	307	410	351	175	25	110	57	73	FF 265
LS 160 MP	254	294	210	294	108	20	64	14,5	25	160	315	368	468	407	208	44	134	92	63	FF 300
LS 160 M	254	294	210	294	108	20	60	14,5	25	160	316	395	495	435	235	44	134	92	63	FF 300
LS 160 LR	254	294	254	294	108	20	64	14,5	25	160	315	368	495	440	208	44	134	92	63	FF 300
LS 160 L	254	294	254	294	108	20	60	14,5	25	160	316	395	495	435	235	44	134	92	63	FF 300
LS 160 LU	254	294	254	294	108	20	60	14,5	25	160	316	395	510	450	235	44	134	92	63	FF 300
LS 180 MT	279	324	241	316	121	20	79	14,5	28	180	316	428	495	435	248	45	205	100	95	FF 300
LS 180 LR	279	324	279	316	121	20	79	14,5	28	180	316	428	520	450	248	45	205	100	95	FF 300
LS 180 L	279	339	279	329	121	25	86	14,5	25	180	350	435	552	481	255	54	205	100	95	FF 300
LS 180 LU	279	339	279	329	121	25	86	14,5	25	180	350	435	593	508	255	54	205	100	95	FF 300
LS 200 LT	318	378	305	365	133	30	108	18,5	30	200	350	455	599	514	255	60	205	100	95	FF 350
LS 200 L	318	388	305	375	133	35	103	18,5	36	200	390	475	621	539	275	68	205	100	95	FF 350
LS 200 LU	318	388	305	375	133	35	103	18,5	36	200	390	475	669	586	275	68	205	100	95	FF 350
LS 225 ST	356	431	286	386	149	50	127	18,5	36	225	390	500	627	545	275	74	205	100	95	FF 400
LS 225 SR	356	431	286	386	149	50	127	18,5	36	225	390	500	676	593	275	74	205	100	95	FF 400
LS 225 MT	356	431	311	386	149	50	127	18,5	36	225	390	500	627	545	275	74	205	100	95	FF 400
LS 225 MR	356	431	311	386	149	50	127	18,5	36	225	390	500	676	593	275	74	205	100	95	FF 400
LS 225 MG	356	420	311	375	149	30	65	18,5	30	225	479	629	810	716	405	68	292	148	180	FF 400
LS 250 MZ	406	470	349	449	168	70	150	24	47	250	390	550	676	593	300	68	217	103	145	FF 500
LS 250 ME	406	470	349	420	168	35	90	24	36	250	479	655	810	716	405	68	292	148	180	FF 500
LS 250 MF	406	470	349	420	168	35	90	24	36	250	479	655	870	776	405	68	292	148	180	FF 500
LS 280 SC	457	520	368	478	190	35	90	24	35	280	479	685	810	716	405	68	292	148	180	FF 500
LS 280 SD	457	520	368	478	190	35	90	24	35	280	479	685	870	776	405	68	292	148	180	FF 500
LS 280 SK	457	533	368	495	190	40	85	24	35	280	586	746	921	819	466	99	292	148	180	FF 500
LS 280 MC	457	520	419	478	190	35	90	24	35	280	479	685	810	716	405	68	292	148	180	FF 500
LS 280 MD	457	520	419	478	190	35	90 95	24	35	280	479 500	685	870	776	405	68 00	292	148	180	FF 500
LS 280 MK		533	419	495	190	40	85	24	35	280	586	746	921	819	466	99	292	148	180	FF 500
LS 315 SP	508	594	406	537	216	40	114	28	70	315	586	781	947	845	466	125	292	148	180	FF 600
LS 315 MP	508	594	457	537	216	40	114	28	70	315	586	781	947	845	466	125	292	148	180	FF 600
LS 315 MR	508	594	457	537	216	40	114	28	70	315	586	781	1017	915	466	125	292	148	180	FF 600

* LB1: non-ventilated motor

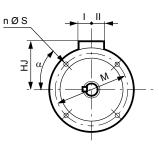
Dimension CA and shaft extension dimensions are identical to those for foot mounted motors (page 104).

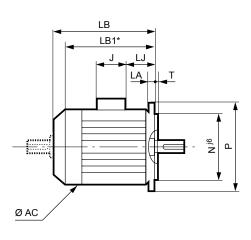


3-phase TEFV induction motors LS aluminium alloy frame Dimensions

F4 - Flange mounted IM B5 (IM 3001)

Dimensions in millimetres





IEC	Flange dimensions												
symbol	М	Ν	Р	Т	n	α	S	LA					
FF 100	100	80	120	2,5	4	45	7	5					
FF 115	115	95	140	3	4	45	10	10					
FF 130	130	110	160	3,5	4	45	10	10					
FF 165	165	130	200	3,5	4	45	12	10					
FF 165	165	130	200	3,5	4	45	12	10					
FF 165	165	130	200	3,5	4	45	12	10					
FF 165	165	130	200	3,5	4	45	12	10					
FF 165	165	130	200	3,5	4	45	12	10					
FF 215	215	180	250	4	4	45	14,5	12					
FF 215	215	180	250	4	4	45	14,5	12					
FF 215	215	180	250	4	4	45	14,5	12					
FF 215	215	180	250	4	4	45	14,5	12					
FF 265	265	230	300	4	4	45	14,5	14					
FF 265	265	230	300	4	4	45	14,5	14					
FF 265	265	230	300	4	4	45	14,5	14					
FF 300	300	250	350	5	4	45	18,5	14					
FF 300	300	250	350	5	4	45	18,5	14					
FF 300	300	250	350	5	4	45	18,5	14					
FF 300	300	250	350	5	4	45	18,5	14					
FF 300	300	250	350	5	4	45	18,5	14					
FF 300	300	250	350	5	4	45	18,5	14					
FF 300	300	250	350	5	4	45	18,5	14					
FF 300	300	250	350	5	4	45	18,5	14					
FF 300	300	250	350	5	4	45	18,5	14					
FF 350	350	300	400	5	4	45	18,5	15					
FF 350	350	300	400	5	4	45	18,5	15					
FF 350	350	300	400	5	4	45	18,5	15					
FF 400	400	350	450	5	8	22,5	18,5	16					
FF 400	400	350	450	5	8	22,5	18,5	16					
FF 400	400	350	450	5	8	22,5	18,5	16					
FF 400	400	350	450	5	8	22,5	18,5	16					
FF 400	400	350	450	5	8	22,5	18,5	16					
FF 500	500	450	550	5	8	22,5	18,5	18					
FF 500	500	450	550	5	8	22,5	18,5	18					
FF 500	500	450	550	5	8	22,5	18,5	18					
FF 500	500	450	550	5	8	22,5	18,5	18					
FF 500	500	450	550	5	8	22,5	18,5	18					
FF 500	500	450	550	5	8	22,5	18,5	18					
FF 500	500	450	550	5	8	22,5	18,5	18					
FF 500	500	450	550	5	8	22,5	18,5	18					
FF 500	500	450	550	5	8	22,5	18,5	18					
FF 600	600	550	660	6	8	22,5	24	22					
FF 600	600	550	660	6	8	22,5	24	22					
FF 600	600	550	660	6	8	22,5	24	22					

			M	ain din	nensior	ıs		
Туре	AC	LB	LB1*	HJ	LJ	J	I	Ш
LS 56 M	110	156	134	84	16	86	43	43
LS 63 M	124	172	165	89	26	96	43	43
LS 71 L	140	193	166	99	26	86	43	43
LS 80 L	170	215	177	123	26	86	43	43
LS 80 LU	170	267	232	123	26	86	43	43
LS 90 S	190	238	197	133	46	86	43	43
LS 90 L/SL	190	265	224	133	46	86	43	43
LS 90 LU	190	285	250	133	46	86	43	43
LS 100 L	200	290	250	138	26	86	43	43
LS 112 M	200	290	250	138	26	86	43	43
LS 112 MG	235	315	265	148	36	86	43	43
LS 112 MU	235	334	288	148	36	86	43	43
LS 132 S	235	350	306	148	53	86	43	43
LS 132 SM/M	280	387	327	175	25	110	57	73
LS 132 MU	280	410	351	175	25	110	57	73
LS 160 MP	315	468	407	208	44	134	92	63
LS 160 M	316	495	435	235	44	134	92	63
LS 160 LR	315	495	440	208	44	134	92	63
LS 160 L	316	495	435	235	44	134	92	63
LS 160 LU	316	510	450	235	44	134	92	63
LS 180 MT	316	495	435	248	45	205	100	95
LS 180 LR	316	520	450	248	45	205	100	95
LS 180 L	350	552	481	255	54	205	100	95
LS 180 LU	350	593	508	255	54	205	100	95
LS 200 LT	350	599	514	255	60	205	100	95
LS 200 L	390	621	539	275	68	205	100	95
LS 200 LU	390	669	586	275	68	205	100	95
LS 225 ST	390	627	545	275	74	205	100	95
LS 225 SR	390	676	593	275	74	205	100	95
LS 225 MT	390	627	545	275	74	205	100	95
LS 225 MR	390	676	593	275	74	205	100	95
LS 225 MG	479	810	716	405	68	292	148	180
LS 250 MZ**	390	676	593	300	68	217	103	145
LS 250 ME**	479	810	716	405	68	292	148	180
LS 250 MF**	479	870	776	405	68	292	148	180
LS 280 SC**	479	810	716	405	68	292	148	180
LS 280 SD**	479	870	776	405	68	292	148	180
LS 280 SK**	586	921	819	466	99	292	148	180
LS 280 MC**	479	810	716	405	68	292	148	180
LS 280 MD**	479	870	776	405	68	292	148	180
LS 280 MK**	586	921	819	466	99	292	148	180
LS 315 SP**	586	947	845	466	125	292	148	180
LS 315 MP**	586	947	845	466	125	292	148	180
LS 315 MR**	586	1017	915	466	125	292	148	180

* LB1: non-ventilated motor ** For IM 3001 types of use for frame sizes \geq 250 mm, please consult Leroy Somer.

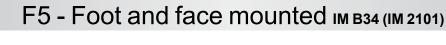
Dimension CA and shaft extension dimensions are identical to those for foot mounted motors (page 104).

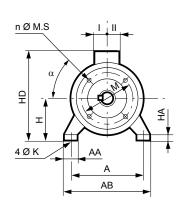


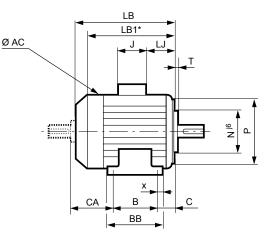
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IM 3011 use

3-phase TEFV induction motors LS aluminium alloy frame Dimensions







Dimensions in millimetres

Туре									Ν	lain di	nensio	ons								
Type	А	AB	В	BB	С	Х	AA	К	HA	Н	AC	HD	LB	LB1*	HJ	LJ	J	I	Ш	Sym.
LS 56 M	90	104	71	87	36	8	25	6	7	56	110	140	156	134	84	16	86	43	43	FT 65
LS 63 M	100	115	80	96	40	8	26	7	9	63	124	152	172	165	89	26	86	43	43	FT 75
LS 71 L	112	126	90	106	45	8	24	7	9	71	140	170	193	166	99	26	86	43	43	FT 85
LS 80 L	125	157	100	120	50	10	29	9	10	80	170	203	215	177	123	26	86	43	43	FT 100
LS 80 LU	125	157	100	120	50	10	29	9	10	80	170	203	267	232	123	26	86	43	43	FT 100
LS 90 S	140	172	100	120	56	10	37	10	11	90	190	223	218	177	133	26	86	43	43	FT 115
LS 90 L/SL	140	172	125	162	56	28	37	10	11	90	190	223	245	204	133	26	86	43	43	FT 115
LS 90 LU	140	172	125	162	56	28	37	10	11	90	190	223	265	230	133	26	86	43	43	FT 115
LS 100 L	160	196	140	165	63	12	40	12	13	100	200	238	290	250	138	26	86	43	43	FT 130
LS 112 M	190	220	140	165	70	12	45	12	14	112	200	250	290	250	138	26	86	43	43	FT 130
LS 112 MG	190	220	140	165	70	12	52	12	14	112	235	260	315	265	148	36	86	43	43	FT 130
LS 112 MU	190	220	140	165	70	12	52	12	14	112	235	260	334	288	148	36	86	43	43	FT 130
LS 132 S	216	250	140	170	89	16	50	12	15	132	235	280	350	306	148	53	86	43	43	FT 215
LS 132 SM/M	216	250	178	208	89	16	59	12	18	132	280	307	387	327	175	25	110	57	73	FT 215
LS 132 MU	216	250	178	208	89	16	59	12	18	132	280	307	410	351	175	25	110	57	73	FT 215
LS 160 MP	254	294	210	250	108	20	112	14	25	315	312	468	468	407	175	70	110	57	73	FT 215
LS 160 LR	254	294	254	294	108	20	112	14	25	315	312	495	468	440	175	70	110	57	73	FT 215

* LB1: non-ventilated motor

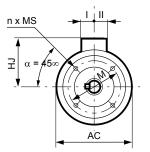
Dimension CA and shaft extension dimensions are identical to those for foot mounted motors (page 104).

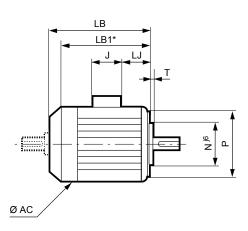


3-phase TEFV induction motors LS aluminium alloy frame Dimensions

F6 - Face mounted IM B14 (IM 3601)

Dimensions in millimetres





IEC		I	Flange di	mensions	5	
symbol	М	Ν	Р	Т	n	MS
FT 65	65	50	80	2,5	4	M5
FT 75	75	60	90	2,5	4	M5
FT 85	85	70	105	2,5	4	M6
FT 100	100	80	120	3	4	M6
FT 100	100	80	120	3	4	M6
FT 115	115	95	140	3	4	M8
FT 115	115	95	140	3	4	M8
FT 115	115	95	140	3	4	M8
FT 130	130	110	160	3,5	4	M8
FT 130	130	110	160	3,5	4	M8
FT 130	130	110	160	3,5	4	M8
FT 130	130	110	160	3,5	4	M8
FT 215	215	180	250	4	4	M12
FT 215	215	180	250	4	4	M12
FT 215	215	180	250	4	4	M12
FT 215	215	180	250	4	4	M12
FT 215	215	180	250	4	4	M12

* LB1: non-ventilated motor

Turne			М	ain din	nensio	ns		
Туре	AC	LB	LB1*	HJ	LJ	J	I	П
LS 56 M	110	156	134	84	16	86	43	43
LS 63 M	124	172	165	89	26	86	43	43
LS 71 L	140	193	166	99	26	86	43	43
LS 80 L	170	215	177	123	26	86	43	43
LS 80 LU	170	267	232	123	26	86	43	43
LS 90 S	190	218	177	133	26	86	43	43
LS 90 L/SL	190	245	204	133	26	86	43	43
LS 90 LU	190	265	230	133	26	86	43	43
LS 100 L	200	290	250	138	26	86	43	43
LS 112 M	200	290	250	138	26	86	43	43
LS 112 MG	235	315	265	148	36	86	43	43
LS 112 MU	235	334	288	148	36	86	43	43
LS 132 S	235	350	306	148	53	86	43	43
LS 132 SM/M	280	387	327	175	25	110	57	73
LS 132 MU	280	410	351	175	25	110	57	73
LS 160 MP	312	468	407	208	70	110	57	73
LS 160 LR	312	468	440	208	70	110	57	73

F

Dimension CA and shaft extension dimensions are identical to those for foot mounted motors (page 104).



G1 - Non-standard flanges

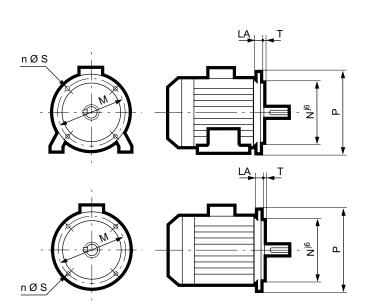
Optionally, LEROY-SOMER motors can be fitted with flanges and faceplates that are larger or smaller than standard. This means that motors can be adapted to all types of situation without the need for costly and timeconsuming modifications.

The tables below give flange and faceplate dimensions and flange/motor compatibility. The bearing and shaft extension for each frame size remain standard.

MAIN FLANGE DIMENSIONS

Flange mounted (FF)



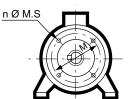


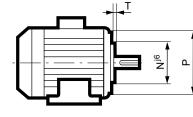
IEC	Flange dimensions												
symbol	м	N	Р	т	n	s	LA						
FF 100	100	80	120	2.5	4	7	5						
FF 115	115	95	140	3	4	10	10						
FF 130	130	110	160	3.5	4	10	10						
FF 165	165	130	200	3.5	4	12	10						
FF 215	215	180	250	4	4	15	12						
FF 265	265	230	300	4	4	15	14						
FF 300	300	250	350	5	4	18.5	14						
FF 350	350	300	400	5	4	18.5	15						
FF 400	400	350	450	5	8	18.5	16						
FF 500	500	450	550	5	8	18.5	18						
FF 600*	600	550	660	6	8	24	22						

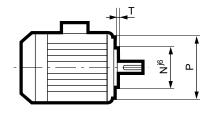
lerance Njs

Face mounted (FT)

Dimensions in millimetres







IEC		Faceplate dimensions											
symbol	м	N	Р	т	n	M.S							
FT 65	65	50	80	2.5	4	M5							
FT 75	75	60	90	2.5	4	M5							
FT 85	85	70	105	2.5	4	M6							
FT 100	100	80	120	3	4	M6							
FT 115	115	95	140	3	4	M8							
FT 130	130	110	160	3.5	4	M8							
FT 165	165	130	200	3.5	4	M10							
FT 215	215	180	250	4	4	M12							
FT 265	265	230	300	4	4	M12							



nØM.S

G1 - Non-standard flanges

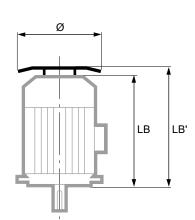
				F	lange	moun	ted (FI	=)						Face r	nount	ed (FT)			
Flange type Motor type	FF 100	FF 115	FF 130	FF 165	FF 215	FF 265	FF 300	FF 350	FF 400	FF 500	FF 600	FT 65	FT 75	FT 85	FT 100	FT 115	FT 130	FT 165	FT 215	FT 265
LS 56	•											•	*	*	*					
LS 63	0	•	*									*	•	*	*	*				
LS 71	0	0	•	O								*	*	•	*	*	*			
LS 80		0	0	•	*									*	•	*	*	*		
LS 90		*	*	•	*										*	•	*	0		
LS 90 (Foot)		0	0	о	<u> </u>										*	•	*	<u> </u>		
LS 100		0	0	0	•											*	•	*	*	
LS 112 M		<u> </u>	0	0	•											*	•	*	*	
LS 112 MG			0	0	•	*										*	•	*	*	
LS 132 S				0	*	•											*	*	•	*
LS 132 SM/M/MU				0	0	•	0											*	•	*
LS 160 MP/L/LR					*	*	•	*											•	*
LS 180							•	*												
LS 200							*	•	*											
LS 225									•	*										
LS 250									*	•										
LS 280										•	*									
LS 315										*	•									
 Standard 	O Moo	lified be	earing lo	ocation	3	≮ Adap	table wi	thout m	odificat	ion		: non	-standa	ard						

G2 - Drip covers

Dimensions in millimetres

Drip cover for operation in vertical position, shaft end facing down

	,	
Туре	LB'	Ø
80	LB + 20	145
90	LB + 20	185
100	LB + 20	185
112 M	LB + 20	185
112 MG	LB + 25	210
132 S	LB + 25	210
132 SM and M	LB + 30	240
160 MP-LR	LB + 30	240
160 M-L-LU	LB + 36.5	265
180 MT-LR	LB + 36.5	265
180 L/LU	LB + 36.5	305
200 LT	LB + 36.5	305
200 L-LU	LB + 36.5	350
225 ST-MT-MR	LB + 36.5	350
225 MG	LB + 55	420
250 MZ	LB + 36.5	350
250 ME-MF	LB + 55	420
280 SC/SD/MC/MD	LB + 55	420
280 SK-MK	LB + 76.5	505
315 SP-MP-MR	LB + 76.5	505





G3.1 - LS MOTORS WITH OPTIONAL FEATURES

The integration of LS motors within a process often requires accessories to make operation easier:

- **D.C. tachometers** recommended for slip compensation.

- A.C. tachometers for speed measurement.

- forced ventilation for motors used at high or low speeds.

I B4

G3 - Options

- **holding brakes** for maintaining the rotor in the stop position without needing to leave the motor switched on.

- **emergency stop brakes** to immobilise loads in case of failure of the motor torque control or loss of power supply.

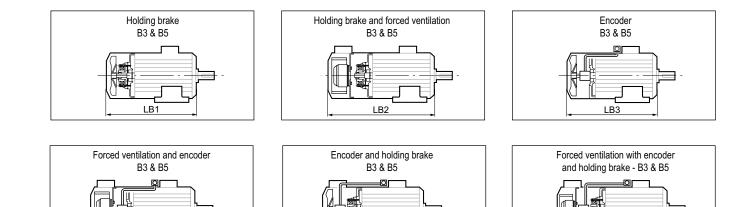
- **encoders** which provide digital information for accurate speed maintenance and position control.

These options can be used singly or in combination as shown in the table opposite.

Notes:

- Without forced ventilation, there is a possibility of overspeed with class «S» balancing.
- The motor temperature is monitored by probes built into the windings.

LB6



LB5





G3 - Options

G3.2 - DIMENSIONS OF LS MOTORS WITH OPTIONAL FEATURES

Dimensions in millimetres

_			Main dimer	nsions LBn		
Туре	LB1	LB2	LB3	LB4	LB5	LB6
LS 80 L	251	340	295	351	359	415
LS 90 S	276	335	•	0	•	0
	302	362	328	383	375	430
LS 100 L	354	395	376	431	440	495
LS 112 M	354	395	376	431	440	495
LS 112 MG	380	455	396	443	459	497
LS 132 S	400	445	o	0	0	0
LS 132 SM	447	482	461	499	535	573
LS 132 MU	0	o	486	524	560	598
LS 160 M	-	-	549	687	-	-
LS 160 L	-	-	549	687	-	-
LS 160 LU	-	-	564	702	-	-
LS 180 MT	-	-	549	687	-	-
LS 180 LR	-	-	564	702	-	-
LS 180 L	-	-	602	741	-	-
LS 180 LU	-	-	629	769	-	-
LS 200 LT	-	-	635	775	-	-
LS 200 L	-	-	674	802	-	-
LS 200 LU	-	-	723	847	-	-
LS 225 ST	-	-	681	808	-	-
LS 225 SR	-	-	730	854	-	-
LS 225 MR	-	-	730	854	-	-
LS 225 MG	-	-	860	1012	-	-
LS 250 MZ	-	-	730	-	-	-
LS 250 ME	-	-	860	1012	-	-
LS 280 SC	-	-	860	1012	-	
LS 280 MD	-	-	920	1072	-	-
LS 280 MK	-	-	965	1075	-	-
LS 315 SP/MP	-	-	991	1101	-	-
LS 315 MR	-	-	1061	1171	-	-

- : not available

O : please consult Leroy-Somer

* For B5, add 20 mm

Description of options

The dimensions and characteristics of the various options described are available in the LS MV motor catalogues.



G4 - Safety

The elimination of risk for operators of all types of equipment is one of the priority areas in workplace safety.

Companies can do their best by perfecting their processes and procedures to make them safer and by introducing a safety element into their training courses, but none of this is any good if there is no suitably safe equipment on the market. Progress has been made in this area. Manufacturers, users, standards institutions and government departments have all played a part in improving safety in the workplace.

Leroy Somer has developed with certain customers complete motor packages incorporating a variety of safety features. Typically, some of the main options that have been used are:

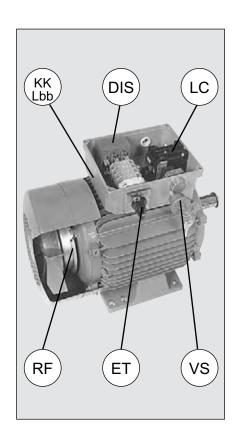
Symbol	Safety options	Details
RF	Decelerator - Electromechanical brake	5 types: 5 decelerating torques RF 3 - C = 3 mN RF 5 - C = 5 mN RF 32 - C = 32 mN RF 10 - C = 10 mN RF 16 - C = 16 mN
DF	Decelerator/brake electrically released when machine stopped	Reversing switch prevents motor starting when brake is not applied.
РТО	Overload protection	Bimetal temperature probe in series with the contactor coil.
DIS	Protection against jamming and short-circuits	Isolating switch with fixed setting for each motor (0.35 to 7.5 kW).
TL	Red indicator light	Shows machine is switched on.
LC	Supply and protection switch: - protects against overload (used with PTO) - prevents uncontrolled starts	Single voltage power switch: 2 standard types - 230V: LC 220 Other voltages on request - 400V: LC 380
VS	Key lock to prevent machine starting	LC is controlled by: - a pushbutton for starting - a mushroom head button with VS emergency stop option
ET	Star-delta starter	Starter switch with timer, downstream of LC.
А	Load ammeter	2 coloured zones on meter: - green: continuous duty - red: overload - intermittent duty



G4 - Safety

Na	Main option	Additional		References*	
No.	combinations	combinable options	Sbb	Mbb	Lbb
	- Decelerator - brake: RF	PTO	•		
1	- 4 types: RF3, RF5, RF10, RF16	DF	•		
	- D.O.L. starting: LC	Α		•	
	- 1 supply voltage: LC 220	PTO		•	
2	or LC 380				
-	- Control on right: LC/d	VS		•	
	- Control on left: LC/g	TL		•	•
		DIS			•
	- Star-delta starting:	PTO			•
3	LC ET				
3 (2 + ET)	- Control on right: LC ET/d	VS			•
(2+1)	- Control on left: LC ET/g	A or DIS			•
		TL			•
	- Decelerator - brake + D.O.L.	PTO			•
4	starting : RF LC				
4 (1 + 2)	- Control on right: RF LC/d	VS			•
(1+2)	- Control on left: RF LC/g	DF or A or DIS			•
		TL			•
	- Decelerator - brake + Star-delta	PTO			•
5	starting : RF LC ET				
5 (1 + 3)	- Control on right: RF LC ET/d	VS			•
(1+3)	- Control on left: RF LC ET/g	DF or A or DIS			•
		TL			٠

* Dimensions (see following page).

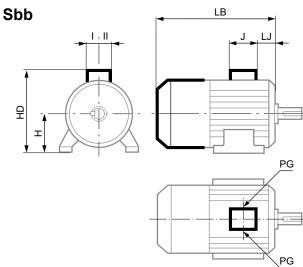


G



G4 - Safety

DEVICES FOR MOTORS WITH OPTIONAL SAFETY FEATURES



LB RF

PG

LB

LJ

PG

Control

- Terminal box with cable gland on right or left (as seen from drive end)

	MOTOR TYPES							
Ref.	LS 80	LS 90S	LS 90L	LS 100	LS 112 M MG	LS 132 S	LS 132 M	
LB	251	276	302	354	354 380	400	447	
J	137	137	137	137	137	137	160	
LJ	25	25	25	32	35	53	25	
HD	224	244	244	259	280	300	313	
н	80	90	90	100	112	132	132	
1	51.5	51.5	51.5	51.5	51.5	51.5	55	
Ш	51.5	51.5	51.5	51.5	51.5	51.5	55.5	

Dimensions in millimetres

- Reversible terminal box with cable gland on fan cover side (as seen from drive end)

MOTOR TYPES							
Ref.	LS 80	LS 90S	LS 90L	LS 100	LS 112 M MG	LS 132 S	LS 132 M
LB	214	218	245	290	290 315	350	-
LB RF	251	276	302	354	354 380	400	-
J	109	109	109	109	109	109	-
LJ	17.5	17.5	17.5	24.5	27.5	45.5	-
HD	247	267	267	282	303	323	-
н	80	90	90	100	112	132	-
I.	143	143	143	143	143	143	-
	51	51	51	51	51	51	-

1 terminal box with cable gland on right, controls on left
1 terminal box with cable gland on left, controls on right (as seen from drive end)

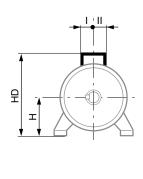
	MOTOR TYPES							
Ref.	LS 80	LS 90S	LS 90L	LS 100	LS 112 M MG	LS 132 S	LS 132 M	
LB	214	218	245	290	290 315	350	387	
LB RF	251	276	302	354	354 380	400	447	
J	194	194	194	194	194	194	194	
LJ	17.5	17.5	17.5	24.5	27.5	45.5	24	
HD	247	266	266	281	302	322	334	
н	80	90	90	100	112	132	132	
1	78.5	78.5	78.5	78.5	78.5	78.5	78.5	
	78.5	78.5	78.5	78.5	78.5	78.5	78.5	

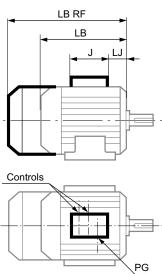
Lbb

Mbb

дН

Т







H1 - Voltage drop along cables (standard NFC 15 100)

Voltage drops are calculated using the formula:

$$u = b \left(\rho_{\uparrow} \frac{L}{S} \cos \varphi + \lambda L \sin \varphi \right) I_{s}$$

where *u* = voltage drop

b = factor equal to 1 for three-phase circuits, and equal to 2 for single-phase circuits

Note: Three-phase circuits with a neutral that is completely out of balance (loss of two phases) are treated as single-phase circuits.

 ρ_{τ} = resistivity of the conductors in normal duty taken as being equal to the resistivity atthe normal duty temperature, ie. 1.25 times the resistivity at 20 °C, giving 0.0225 $\Omega mm^2/m$ for copper and 0.036 $\Omega mm^2/m$ for aluminium.

L = length of cabling conduits in metres

S = cross-section of conductors in mm²

 $\cos \phi$ = Power Factor: if the exact figure is not available, the PF is taken as being 0.8 (sin ϕ = 0.6)

 λ = linear reactance of conductors, taken as being equal to 0.08 m Ω / m if the exact figure is not available

Maximum power for D.O.L. motors The table opposite shows maximum kW ratings for D.O.L. motors connected to the

Minimising motor starting problems For the installation to remain in good working order, it is necessary to avoid any significant temperature rise in the cabling conduits, while making sure that the protection devices

Operating problems in other equipment

connected to the same supply are due to the

voltage drop caused by the current demand

on starting, which can be many times greater

than the current absorbed by the motor at full

 $I_s = current in use, in amps$

mains supply.

load

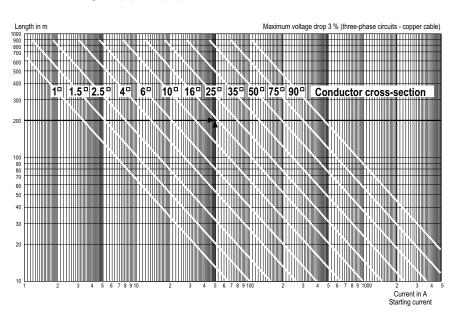
do not interrupt starting.

The higher the current, the greater the voltage drop will be. The voltage drop should therefore be calculated for the starting current to see if this is suitable for the application. If the most important criterion is the starting torque (or starting time), the voltage drop should be limited to 3% maximum* (the equivalent of a loss of torque of around 6 to 8%).

* the relative voltage drop (as a %) equals:

 $\Delta u = 100 \frac{u}{U_0}$

 U_o = voltage between phase and neutral



Maximum power for D.O.L. motors (kW)

Type of motor	Single-phase 230 (220) V	Three-phase (380/400V)	
Type of premises		full power D.O.L.	other starting methods
Residential areas	1.4	5.5	11
Other premises Overhead power lines Underground power lines	3 5.5	11 22	22 45

Other premises includes the service sector, the industrial sector, general housing services, the agricultural sector, etc.

For motors driving a high inertia machine, motors with long starting times, brake motors or change of direction by current reversal, the electricity supply company must carry out all the necessary checks before installation.



H2 - Earthing impedance

French government decree 62.1454 of 14 November 1962 concerning the protection of operatives in workplaces in which electrical currents are used, requires that when the neutral is connected to the earth by a limiting impedance, the rms value of the fault current multiplied by the resistance of the earth terminal of the mass in which the fault occurs must not exceed:

- 24 V in highly conductive workplaces

- 50 V in other cases

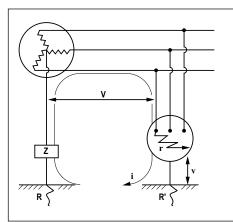
(Ref. standard UTE C 12.100 - page 12, Article 32)

This may be written:

v = R'iand V = (Z + R + R' + r)iwhence $Z = R' \frac{V}{v} - (R + R' + r)$

and consequently:

$$Z \ge R' \frac{V}{v_L} - (R + R' + r)$$



- V : simple voltage
- Z : limiting impedance
- ${\sf R}\,$: resistance of neutral earth
- R' : resistance of the earth of the mass where the fault occurs
- r : internal fault resistance
- i : fault current
- v : potential of the mass in relation to the earth
- v_L : maximum value imposed for that potential

Example 1

Highly conductive premises where:

- $R = 3\Omega$
- R' = 20 Ω
- = 10 Ω
- V = 220 V
- $Z \ge 20 \text{ x } \frac{220}{24} (3 + 20 + 10) = 150 \Omega$

Example 2

Other cases: R = 6Ω R' = 10Ω r = 0Ω V = 380 V $Z \ge 10 x \frac{380}{50} - (6 + 10 + 0) = 60 \Omega$





H3 - Packaging weights and dimensions

	ROAD TRANSPORT					
Frame size		IM B3	IM B5 - IM V1			
	Tare (kg)	Dimensions in mm (L x W x H)	Tare (kg)	Dimensions in mm (L x W x H		
		Cardboard boxes				
56	0.3	230 x 120 x 170	0.3	230 x 120 x 170		
63	0.3	230 x 120 x 170	0.3	230 x 120 x 170		
71	0.4	305 x 155 x 170	0.4	305 x 155 x 170		
80	0.7	330 x 205 x 255	0.7	330 x 205 x 255		
90	0.85	375 x 215 x 285	0.85	375 x 215 x 285		
100	1.25	420 x 270 x 320	1.25	420 x 270 x 320		
112	1.25	420 x 270 x 320	1.25	420 x 270 x 320		
132	2.9	560 x 320 x 375	2.9	560 x 320 x 375		
160	8	710 x 500 x 570	8	710 x 500 x 570		
		Open pallet box or laths				
160	17	740 x 480 x 610	18	740 x 480 x 610		
180	17	740 x 480 x 610	18	740 x 480 x 610		
200	38	890 x 570 x 710	35	890 x 570 x 710		
225	56		48	1000 x 870 x 720		
		Pallets				
250	18	1000 x 600	22	1000 x 600		
280	20	1200 x 700	24	1200 x 700		
315	20	1200 x 700	24	1200 x 700		

	SEA TRANSPORT					
Frame size		IM B3	IM B5 - IM V1			
	Tare (kg)	Dimensions in mm (L x W x H)	Tare (kg)	Dimensions in mm (L x W x H)		
		Plywood crates				
56	on request		on request			
63	on request		on request			
71	on request		on request			
80	on request		on request			
90	on request		on request			
100	17	740 x 480 x 610	18	740 x 480 x 610		
112	17	740 x 480 x 610	18	740 x 480 x 610		
132	17	740 x 480 x 610	18	740 x 480 x 610		
160	17	740 x 480 x 610	18	740 x 480 x 610		
160	17	740 x 480 x 610	18	740 x 480 x 610		
180	17	740 x 480 x 610	18	740 x 480 x 610		
200	48	910 x 620 x 750	50	910 x 620 x 750		
225	55	960 x 750 x 830	57	960 x 750 x 830		
250	77	77 1120 x 750 x 890		1120 x 750 x 890		
280	86	1270 x 720 x 970	90	1270 x 720 x 970		
315	86	1270 x 720 x 970	90	1270 x 720 x 970		

- These values are given for individual packages

- Frame sizes up to 132 grouped in cardboard containers on a standard 1200 x 800 pallet



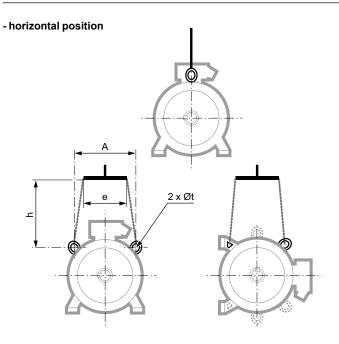
H4 - Position of lifting rings

Position of lifting rings for lifting the motor only (not connected to the machine)

Labour regulations in France stipulate that all loads over 25 kg must be fitted with lifting devices to facilitate handling.

The positions of the lifting rings and the

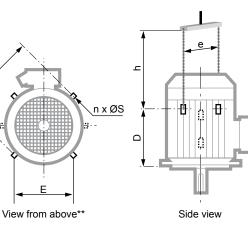
minimum dimensions of the loading bars are given below in order to help with preparation for handling the motors. If these precautions are not followed, there is a risk of warping or crushing some equipment such as the terminal box, protective cover or drip cover. IMPORTANT: motors intended for use in the vertical position may be delivered in the horizontal position on a pallet. When the motor is pivoted, the shaft must under no circumstances be allowed to touch the ground, as the bearings may be irreparably damaged.



Time	Horizontal position					
Туре	Α	e min	h min	Øt		
112 MG/MU	120	200	150	9		
132	160	200	150	9		
160	200	160	110	14		
180 MR	200	160	110	14 14		
180 L	200	260 260	150			
200	270		165 150	14		
225 ST/MT	270	260		14		
225 MG	400	400	500	30		
250 ME/MF			500	30		
280 SC/MC/MD			500	30		
280 SK/MK	360	380	500	30		
315 SP/MP/MR	360	380	500	17		

- vertical position





Turne	Vertical position						
Туре	С	Е	D	n**	øs	e min*	h min
160	320	200	230	2	14	320	350
180 MR	320	200	230	2	14	320	270
180 L-LU	390	265	290	2	14	390	320
200 L-LU	410	300	295	2	14	410	450
225 ST/MT/MR	410	300	295	2	14	410	450
225 MG	500	400	502	4	30	500	500
250 MZ	410	300	295	2	14	410	450
250 ME/MF	500	400	502	4	30	500	500
280 SC/SD/MC/MD	500	400	502	4	30	500	500
280 SK/MK	630	-	570	2	30	630	550
315 SP/MP/MR	630	-	570	2	30	630	550

* : if the motor is fitted with a drip cover, allow an additional 50 to 100 mm to avoid damaging it when the load is swung.

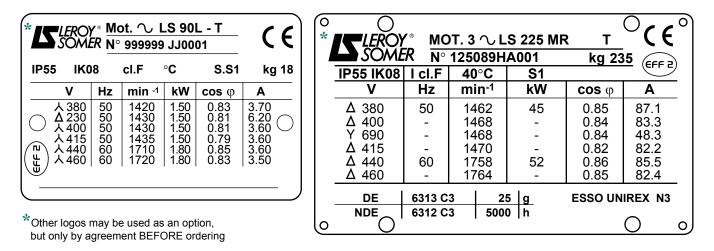
** : if n = 2, the lifting rings form an angle of 90° with respect to the terminal box axis

if n = 4, this angle becomes 45°



H5 - Identification, exploded views and parts list

H5.1 - NAMEPLATES



Definition of symbols used on nameplates



LEGAL MARK OF CONFORMITY OF PRODUCT TO THE REQUIREMENTS OF EUROPEAN DIRECTIVES.

MOT 3 ~	: Three-phase A.C. motor
LS	: Range
132	: Frame size
Μ	: Housing symbol
т	: Impregnation index

Motor no.

- 125089 : Serial number Н : Year of production Α : Month of production 001 : Batch number (EFF 2)
 - : Efficiency indicator

l cl. F	: Insulation class F
40°C	: Contractual
	ambient operating
	temperature
S%	: Duty - Duty (operating)
	factor
c/h	: Number of cycles per hour
kg	: Weight
V	: Supply voltage
Hz	: Supply frequency
min₁	: Revolutions per
	minute (rpm)
kW	: Rated output power
cos φ	: Power factor
Α	: Rated current

IP55 IK08: Index of protection

- : Delta connection Δ
- Y : Star connection

Please quote when ordering spare parts

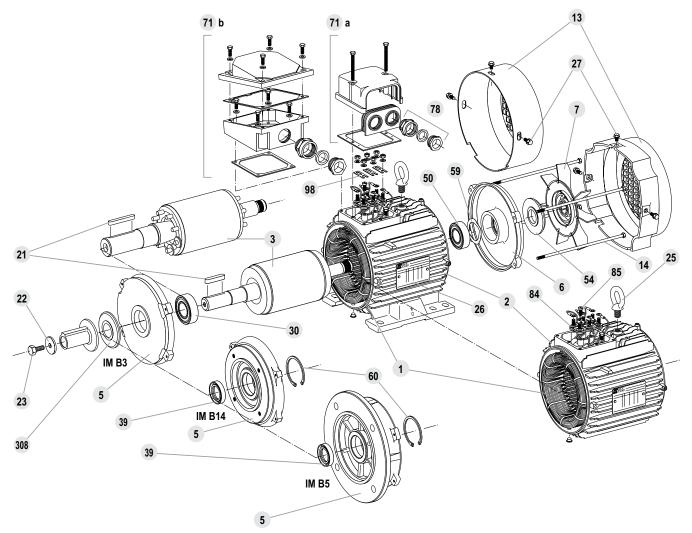
Bearings

DE	: Drive end bearing
NDE	: Non drive end bearing
g	: Amount of grease at each regreasing (in g)
h	: Regreasing interval (in hours)
ESSO	UNIREX N3 : Type of grease



H5 - Identification, exploded views and parts list

H5.2 - FRAME SIZE: 56 to 132

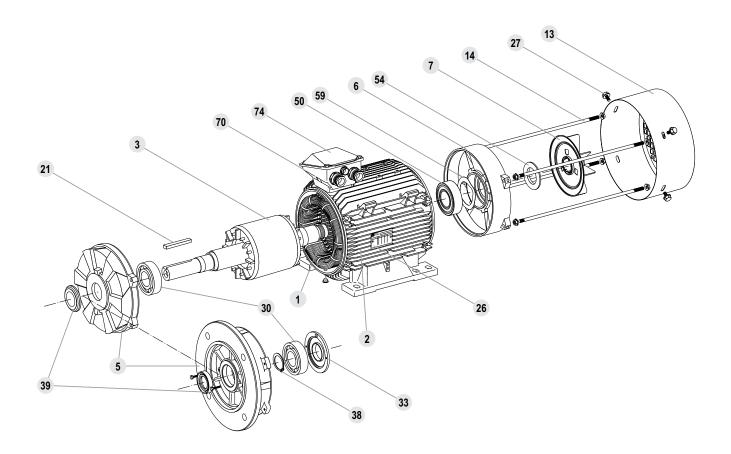


Frame size: 56 to 132						
No,	Description	No,	Description	No,	Description	
1	Wound stator	22	Shaft extension washer	59	Preloading (wavy) washer	
2	Frame	23	Shaft extension screw	60	Circlip	
3	Rotor	25	Lifting ring	71a	Plastic terminal box (up to frame 112)	
5	DE shield	26	Nameplate	71b	Metal terminal box	
6	NDE shield	27	Fan cover screw	78	Cable gland	
7	Fan	30	Drive end bearing	84	Terminal block	
13	Fan cover	39	Drive end seal	85	Set screw	
14	Tie rods	50	Non drive end bearing	98	Connectors	
21	Shaft extension key	54	Non drive end seal	308	Labyrinth seal	



H5 - Identification, exploded views and parts list

H5.3 - FRAME SIZE: 160 and 180

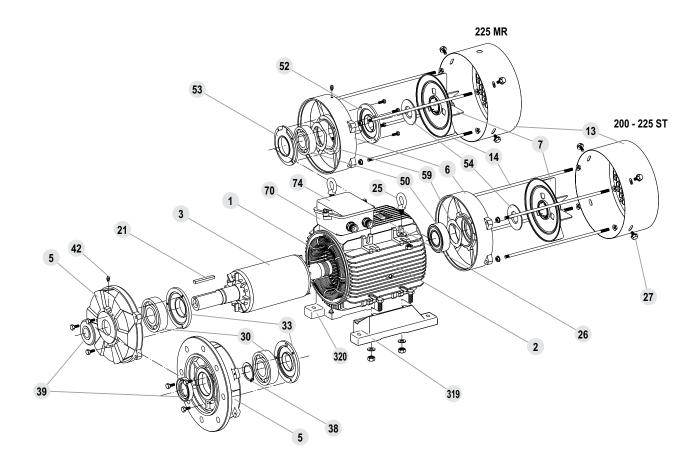


Frame size: 160 and 180						
No.	Description	No.	Description	No.	Description	
1	Wound stator	14	Tie rods	39	Drive end seal	
2	Frame	21	Key	50	Non drive end bearing	
3	Rotor	26	Nameplate	54	Non drive end seal	
5	DE shield	27	Fan cover screw	59	Preloading (wavy) washer	
6	NDE shield	30	Drive end bearing	70	Terminal box	
7	Fan	33	Inner DE bearing retainer	74	Terminal box lid	
13	Fan cover	38	Drive end bearing circlip			



H5 - Identification, exploded views and parts list

H5.4 - FRAME SIZE: 200 and 225

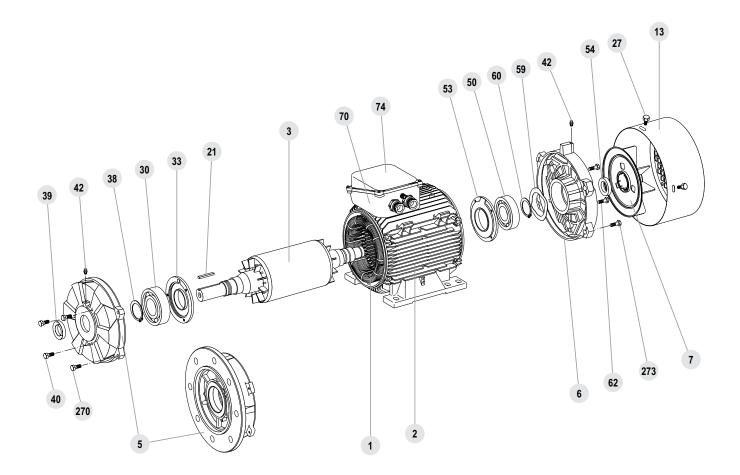


Frame size: 200 and 225						
No.	Description	No.	Description	No.	Description	
1	Wound stator	25	Lifting ring	52	Outer NDE bearing retainer	
2	Frame	26	Nameplate	53	Inner NDE bearing retainer	
3	Rotor	27	Fan cover screw	54	Non drive end seal	
5	DE shield	30	Drive end bearing	59	Preloading (wavy) washer	
6	NDE shield	33	Inner DE bearing retainer	70	Terminal box	
7	Fan	38	Drive end bearing circlip	74	Terminal box lid	
13	Fan cover	39	Drive end seal	319	Right foot	
14	Tie rods	42	Grease nipples (optional for 200 frame)	320	Left foot	
21	Key	50	Non drive end bearing			



H5 - Identification, exploded views and parts list

H5.5 - FRAME SIZE: 250 and 280



Frame size: 250 and 280						
No.	Description	No.	Description	No.	Description	
1	Wound stator	30	Drive end bearing	59	Preloading (wavy) washer	
2	Frame	33	DE internal cover	60	Non drive end bearing circlip	
3	Rotor	38	Drive end bearing circlip	62	Cover fixing screw	
5	DE shield	39	Drive end seal	70	Terminal box	
6	NDE shield	40	Cover fixing screw	74	Terminal box lid	
7	Fan	42	Grease nipples	270	DE shield fixing screw	
13	Fan cover	50	Non drive end bearing	273	NDE shield fixing screw	
21	Shaft extension key	53	Inner NDE bearing retainer			
27	Fan cover screw	54	Non drive end seal			

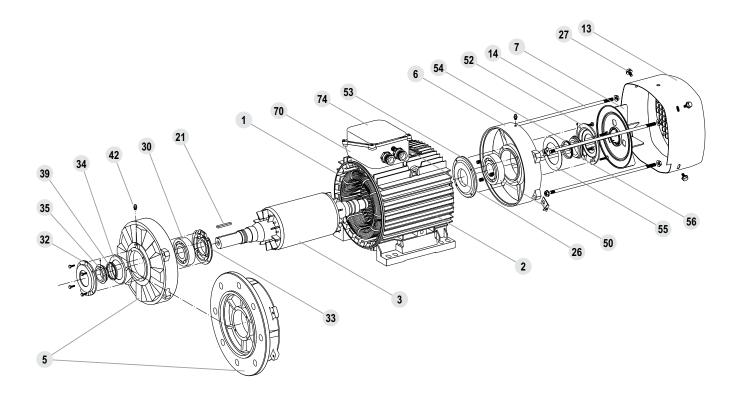
Note: The above illustration of parts does not necessarily show details, forms and volumes accurately.



Η

H5 - Identification, exploded views and parts list

H5.6 - FRAME SIZE: 315



Frame size: 315						
No.	Description	No.	Description	No.	Description	
1	Wound stator	27	Fan cover screw	52	Outer NDE bearing retainer	
2	Frame	30	Drive end bearing	53	Inner NDE bearing retainer	
3	Rotor	32	Outer DE bearing retainer	54	Non drive end seal	
5	DE shield	33	Inner DE bearing retainer	55	NDE fixed grease valve	
6	NDE shield	34	DE fixed grease valve	56	NDE mobile grease valve	
7	Fan	35	DE mobile grease valve	70	Terminal box	
13	Fan cover	39	Drive end seal	74	Terminal box lid	
14	Tie rods	42	Grease nipples			
21	Кеу	50	Non drive end bearing			



H6 - Maintenance

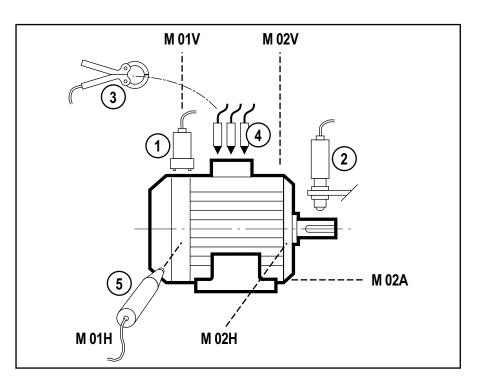
LEROY-SOMER can provide installation and maintenance information on each type of product or product range.

These documents, plus other technical information on our products can be obtained on request from LEROY-SOMER sales offices.

When asking for informative material, you should quote the complete machine reference.

LEROY-SOMER, in its continuous search for ways to help our customers, has evaluated numerous methods of preventive maintenance.

The diagram and table below give the recommended equipment to use and the ideal positions to take measurements of all parameters which can affect the operation of the machine, such as eccentricity, vibration, state of bearings, structural problems, electrical problems, etc



① Accelerometer: for measuring	
vibrations	

- ② Photo-electric cell: for measuring speed and phase (balancing)
- ③ Clamp ammeter: for measuring current (D.C. and 3-phase A.C.)
- ④ Voltage probe: A.C. and D.C. voltages
- ⑤ Infra-red probe: for measuring temperature

Measauring device Measurement points M 01V M 01H M 02V M 02H M 02A Shaft E01 E02 E03 1 Accelerometer (2) Photo-electric cell 3 Clamp ammeter (4) Voltage probe (5) Infra-red probe



GENERAL CONDITIONS OF SALE

LEROY-SOMER

I - SCOPE OF APPLICATION These General Conditions of Sale («GCS») shall apply to the sale of all products, components, software and services (referred to as «Products») proposed or sold by the Seller to the Client. Said GCS shall also apply to all quotation or offers made by the Seller, and are an integral part of all orders. «Seller» is understood to mean all companies directly or indirectly controlled by LEROY-SOMER. As a complementary measure, orders are also subject to the latest version in force of the later. Union General also subject to the latest version in force of the Inter-Union General Conditions of Sale for France of the F.I.E.C. (Fédération des Industries Electriques, Electroniques et de Communication [Federation of Electrical, Electronic and Communication Industries]), inasmuch as they are not contrary to the GCS

The acceptance of the Seller's offers or quotations, or any order, entails the acceptance without reservation of these GCS and rules out all contrary provisions shown on all other documents and, in particular, on the Client's order forms and the Client's General Conditions of Purchase.

Purchase. If the sale concerns castings, by way of derogation to Paragraph 1 above, said castings shall be subject to the latest version in force of the *Conditions Générales Contractuelles des Fonderies Européennes* [General Contractual Conditions of European Foundries]. The Products and services sold pursuant to these GCS may under no circumstances be used for applications in the nuclear field, as such sales expressly fall under technical specifications and specific contracts that the Seller reserves the right to refuse.

II - ORDERS

All orders, even those taken by the Seller's agents and representatives, and regardless of the transmission method, shall only bind the Seller after written acceptance thereby of the order.

The seller reserves the option of modifying the characteristics of its Products without notice. However, the Client shall letain the possibility of specifying the characteristics on which its commitment is contingent. In the absence of any such express stipulation, the Client may not refuse delivery of new, modified Products. The Seller may not be held liable for an unsatisfactory selection of Products if said selection results from conditions of use that are incomplete and/or mistaken, or not disclosed to the Seller by the Client. Except in the event of a stipulation to the contrary, the offers and quotations remitted by the Seller shall only be valid for thirty days as from the date on which they are drawn up. Where the Products must comply with standards, specific regulations and/or be received by control and inspection agencies, the price request must be accompanied by the technical specification, all terms and conditions of sellent.

III - PRICES

expressed exclusive of tax and may be revised without Tarif notice

notice. Prices are either deemed to be firm for the period of validity specified on the quotation, or subject to a revision formula attached to the offer and which specifies, according to the regulations, parameters pertaining to the materials, products, various services and salaries for which the indices are published in the B.O.C.C.R.F. (Bulletin Officiel de la Concurrence, de la Consommation et de la Répression des Fraudes [French Official Journal of Competition and Consumer Matters, and Anti-Fraud Measures]). Freuch Measures)). Fraud Measures)). All additional costs, in particular approval costs, specific checks, etc.,

shall be invoiced in addition

IV - DELIVERY

IV - DELIVERY Sales are governed by the latest edition in force of the INCOTERMS published by the Internal Chamber of Commerce («I.C.C. INCOTERMS»). The Products shall be dispatched according to the conditions stated on the order acknowledgement issued by the Seller for all orders of Products

Products. Except in the event of specific provisions, the prices correspond to Products that are made available in the Seller's factories, including basic

Except in the event of specific provisions, the prices correspond to Products that are made available in the Seller's factories, including basic packaging. Except in the event of a provision to the contrary, the Products shall always be transported at the risk of the addressee. In all cases, it shall be the responsibility of the addressee to make any claims to the carrier, within the delivery time and in the forms specified by law, concerning the state or number of parcels received, and to concomitantly provide the Seller with a copy of such declaration. Failure to comply with said procedure shall exempt the Seller from any liability. In any event, the Seller with the acceptance of the order, the Seller reserves the right to invoice any supplemental costs that may result therefrom. Except in the event of a contractual or statutory obligation to the contrary, ackaging shall not be returnable. In the event that a delivery of Products is delayed for a reason not attributable to the Seller, the Products stored on the Seller's premises shall be insured at the exclusive risk of the Client. Consideration for storage, costs will be invoiced at a rate of 1% (*one per cent*) of the total amount of the order, per week or partial week of storage, with no deductible or *de minimi* amount, as from the date of Products availability provided for in the Client may, at side side of products availability provided for invoice the Client in full for payment, according to the products shall invoice the Seller may, at side side reform said from said date, the Seller may, at its discretion, a either freedy dispose of the Products shall invoice the Seller as indemnities, without prejudice to any other action the Seller may, at its discretion and the products shall be into the Seller as a indemnities, without prejudice to any other action the Seller may, at its discretion and the products and and the seller may atus.

V - DELIVERY TIME

V - DELIVERY TIME The Seller shall only be bound by the delivery time mentioned on its order acknowledgement. Said delivery time shall only start to run as from the date of issuance of the order acknowledgement by the Seller, and subject to the fulfilment of the conditions provided for on the confirmation receipt, in particular receipt of the down payment for the order, notification of the opening of an operative irrevocable and confirmed documentary credit that complies in all respects to the Seller's request (*in particular regarding the amount, currency, validity and licence*), acceptance of the payment conditions accompanied by the implementation of any guarantees requested, etc. Exceeding delivery time shall not grant the Client entitlement to damages and/or penalties.

and/or penalties. Except in the event of a specific condition to the contrary, the Seller

reserves the right to make partial deliveries. Delivery times shall be interrupted by right and without the need for any judicial formalities, by any failure to pay or late payment by the Client.

VI - TESTS - QUALIFICATION

vi - IC>IC>-QUALIFICATION The Products manufactured by the Seller are checked and tested before leaving its factories. Clients may be present at said tests if specified on the order. the orde

Specific design of additional to the present at sale design specified of the order. Specific tests and/or trials, as well as approval of Products, requested by the Client, whether carried out on the Client's premises or in the Seller's factories, on site, or by control and inspection agencies, must be specified on the order and are always at Client's expense. Prototypes for Products specially developed or adapted for a Client must be qualified by the Client before serial production in order to ensure that it is compatible with the other components that make up its equipment, and that it is adapted to the intended use. Said qualification will also enable the Client to ensure that the Products comply with the technical specification. In this respect, the Client and Seller shall sign a Product Approval Form in two original, one of which shall be retained by the Client and one by the Seller.

In the event that the Client requires delivery without having firstly qualified the Products, said Products shall be delivered as they stand and shall always be deemed to be prototypes; the Client shall then be solely liable for using the Products or delivering them to its own clients. However, the Seller may also decide not to deliver the Products that have not received the Client's prior approval

VII - PAYMENT CONDITIONS

All sales shall be deemed to be completed and payable at the Seller's registered office, without any possible derogation, regardless of the payment method, where the contract was concluded and where delivery registered office, without any possible delogation, registered office, without any possible delogation, registered entry awas made. Where the Client is located out of French territory, invoices shall be payable in cash upon receipt, or by a bank draft or a bill of exchange, within 30 (thirty) days net. All early payment compared to the deadline fixed shall give right to a discount of 0.2% (*nought point two* per cent) per month, of the amount concerned of the invoice. Except in the event of provisions to the contrary, where the Client is located outside of French Territory, invoices shall be payable in cash againstremittance of shipping documents, or by inrevocable documentary credit confirmed by a first rate French bank, at Client's expense. Payment shall be understood to mean the fluds being made available on the Seller's bank account and must imperatively be made in the invoicing currency.

currency. Pursuant to French Law no. 2001-420 of 15 May 2001, failure to pay an

Pursuant to French Law no. 2001-420 of 15 May 2001, failure to pay an invoice when due shall trigger, after service of formal notice that has remained without effect, payment to the Seller of a flat-rate penalty on the due date of the receivable, which shall be applied to amount inclusive of tax of monies owed if the invoice is liable to VAT (*Value Added Tax*), and the suspension of pending orders. Said penalty is equal to the European Central Bank Rate + 7 basis points. The collection of said monies via litigation shall trigger an increase of 15% (*fifteen per cent*) of the amount claimed, with a minimum of Euros 500 exclusive of tax (*five hundred euros exclusive of tax*), with tax in addition if fue

addition if due

Moreover, subject to compliance with the statutory provisions in force, in the event of total or partial failure to pay any invoice or instalment whatsoever, regardless of the payment method used, all amounts that remain owed to the Seller (including its subsidiaries, affiliated or allied companies, whether French or foreign) for all deliveries and services, regardless of the due date originally provided for, shall immediately

pecome due. Notwithstanding any specific payment conditions provided for between the parties, the Seller reserves the right to require, in the event of a decline in the Client's credit rating, a payment incident or bankruptcy of the Client:

the payment in cash, before the Products leave the factory, for all orders - down payments to be made on all orders, - alternative or different payment guarantees

VIII - PAYABI E AND RECEIVABLE BALANCE

III - PAYABLE AND RECEIVABLE BALANCE except where prohibited by law, the Seller and the Client expressly agree balance their payables and receivables arising from their trade lations, even if all conditions defined by law for legal balancing are not action.

For the application of said clause, the Seller shall mean any company of the LEROY-SOMER Group.

IX -TRANSFER OF RISK / RESERVE OF TITLE Risk shall be transferred as soon as the Products are made available, according to the delivery conditions stipulated on the order acknowledgement. The transfer to the Client of title shall take place after payment in

The transfer to the Client of title shall take place after payment in full. In the event that the restitution of the Products delivered is claimed by the Seller, the Seller is entitled to retain any down payment as compensation. Remittance of a bill that creates an obligation to pay (*bill* of *exchange or other*) shall not constitute payment and discharge. For as long as the price has not been paid in full, the Client is required to inform the Seller, within twenty-four hours, of the sequestration, requisition or confiscation of the Products for the benefit of a third party, and to take all protective measures to make known the Seller's property right in the event of action by creditors, and to cause such right to be respected.

CONFIDENTIALITY

X - CONFIDENTIALITY Each of the parties undertakes to maintain the confidentiality of all technical, trade, financial or other information received from the other party, whether orally, in writing or by any other means of communication, when any order is negotiated and/or fulfilled. This confidentiality obligation shall apply throughout the period during which the order is fulfilled and for 5 (five) years subsequent to completion or cancellation thereof, regardless of the reasons therefor.

XI-INDUSTRIAL AND INTELLECTUAL PROPERTY

XI - INDUSTRIAL AND INTELLECTUAL PROPERTY Data, studies, results, information or software, whether patentable or not obtained by the Seller when any order is fulfilled shall remain the exclusive property of the Seller. With the exception of instruction and maintenance manuals, documents of any nature remitted to the Client shall remain the exclusive property of the Seller and must be returned to it upon request, even if the Client was invoiced for part of the cost of the study, and said documents may not be disclosed to third parties or used without the Seller's prior written agreement. agreeme

XII - CANCELLATION / TERMINATION

XII - CANCELLATION / TERMINATION The Seller serves the right to cancel or terminate immediately, at the Seller's discretion, by right and without the need for any judicial formalities, the contract in the event of failure to pay any portion whatsoever of the price, when due, or in the event of any breach of any of the Client's contractual obligations. Down payments and any amount already paid shall remain in Seller's hands in the form of indemnities, already paid share terthal the self establish the total of indertination without prejudice to the Selfer's right to claim damages. In the event that the contract is cancelled, the Products must be returned to the Selfer immediately, regardless of where the Products are located, at Client's expense and risk, under penalty of 10% (ten per cent) of the value thereof per unwark defaust. eof, per week's delay

XIII - WARRANTY

All - WARKAN I I The Seller warrants the Products against all operating defects caused by a material or manufacturing fault, for a period of twelve months as from the date on which the Products are made available, unless a different statutory provision subsequently applies, under the conditions defined

Delow. The warranty may only be triggered insofar as the Products have been stored, used and maintained in accordance with the Seller's instructions and manuals. The warranty does not apply where the defect results, in particular, from :

inadequate monitoring, maintenance or storage,

- normal wear and tear on the Products,
 - servicing or modification of the Products,
 - servicing or modification of the Products without the Seller's prior written authorisation,
 - abnormal use of the Products or use of the Products for a purpose other

than that intended, faulty installation of the Products on the premises of the Client and/or

the end user, - failure by the Client to disclose the purpose or conditions of use of the

Products failure to use genuine spare parts, force majeure or any event that is beyond the control of the Seller.



In any case, the warranty is limited to the replacement or repair of the parts or Products deemed faulty by the Seller's technical departments. If the repair is entrusted to a third party, the repair shall only be carried out once the Seller has agreed to the quotation for the repair. All Products returns must have been given the Seller's prior, written

authorisation.

The Products to be repaired must be dispatched carriage paid, to the address given by the Seller. If the Products are not accepted under warranty, their return to the Client shall be invoiced to the Client or the

This warranty shall apply to the Seller's Products that are made readily available and therefore does not cover the de-installation and reinstallation of said Products in the equipment into which it is mounted.

Repair, motification or replacement of any part or Product during the warranty period may not result in the warranty period being extended. The provisions of this article constitute the Seller's sole obligation concerning the warranty of the Products delivered.

XIV - LIABILITY

The Seller's liability is strictly limited to the obligations stipulated in these GCS and those expressly accepted by the Seller. All penalties and indemnities provided for therein constitute lump sum damages that include discharge for the Seller and are exclusive of any other penalty or indemnification

With the exception of the Seller's gross negligence and the compensation of bodily injury, the Seller's liability shall be limited, in total, to the contractual amount, exclusive of tax, of the Product(s) that give(s) right to compensation.

The Seller may under no circumstances be required to indemnify consequential, indirect and / or punitive damages that the Client may use as the basis for a claim; as a result, the Seller may not be required to indemnify, in particular, production losses, operating losses or lost profit or, in general, any damage eligible for indemnification other than bodily injury or damage to property.

The Client undertakes to hold harmless the Seller and / or its insurers from any and all claims made by its insurers and/or any third party in a contractual relation with the Client, in excess of the limit and for the exclusions listed above.

XV - SPARE PARTS AND ACCESSORIES

Spare parts and accessionies shall be supplied upon request, to the extent of their availability. Associated costs shall be invoiced in addition. The Seller reserves the right to require a minimum quantity or invoicing amount per order.

XVI - WASTE MANAGEMENT

The Products that form the purpose of the sale does not fall within the scope of the European Directive 2002/96/EC (WEEE) dated January 27°, 2003, and all related legislation of Member States of the European 2/*, 2003, and ail related legislation of Member States of the European Union that result therefrom, on the composition of electrical and electronic equipment and the disposal of waste from such equipment. In accordance with Article L 541-2 of the French Environment Code, it is the responsibility of the waste holder to ensure the disposal thereof or to cause the disposal thereof at its own expense.

XVII - FORCE MAJEURE

With the exception of the Client's obligation to pay the monies owed to the Seller in respect of an order, the Client and Seller may not be held liable for the total or partial failure to perform their contractual obligations Induction the total of partial failure to perform their contraction obligation. If such failure results from the occurrence of a force majeure. Delays or disturbances in production that totally or partially result from war (whether declared or not), terrorist act, strikes, riots, accidents, fires, floods, natural disasters, transportation delays, shortage of components or materials, governmental decision or action (including prohibition on import/export or the withdrawal of an import/export licence) shall, in particular be deemed a force majeure.

import/export or the withdrawal of an import/export licence) shall, in particular, be deemed a force majeure. If one of the parties is delayed or prevented from performing its obligations by reason of this Article for a period in excess of 180 consecutive days, each party may then terminate, by right and without any need for judicial formalities, the unperformed part of the order, by written notice to the other party, without liability. However, the Client shall be required to pay the price agreed pertaining to the Products already delivered on the date of termination.

XVIII - PROHIBITION ON UNLAWFUL PAYMENTS

The Client shall refrain from being engaged in any activity that would expose the Seller or any of its affiliates to a risk of penalties under laws and regulations of any relevant jurisdiction prohibiting improper payments, including but not limited to bribes or gifts of an obviously unreasonable amount, to any government or agency officials, to political parties or their officials or candidates for public office, or to any employee of any customer or supplier.

XIX - TRADE COMPLIANCE LAWS The Client agrees that all applicable import, export control and sanctions laws, regulations, orders and requirements, as they may be amended from time to time, including without limitation those of the European Union, the United States of America, and the jurisdictions in which the Seller and the Client are established or from which Products may be supplied, and the requirements of any licences, authorisations, general licences or Licence exerctions, requiring the tradition there of the tradition the tradition the tradition there of the tradition the tradition t Supplied, and the requirements of any necess, authorisations, general licences or licence exceptions relating thereto ("Trade Compliance Laws") will apply to its receipt and use of Products, as well as related services and technology. In no event shall the Client use, transfer, release, export or re-export the Products, related services or technology in violation of Trade Compliance Laws.

Seller shall have no obligation to supply any Products, or services unless and until that received any necessary licences or authorisations or has qualified for general licences or licence exceptions under Trade Compliance Laws. If for any reason any such licences, authorisations or approvals are

denied or revoked, or if there is a change in any Trade Compliance Laws that would prohibit Seller from fulfilling the contract, or would in the reasonable judgement of Seller otherwise expose Seller and/or Seller's Affiliate(s) to a risk of liability under Trade Compliance Laws, Seller shall be relieved without liability of all obligations under the contract.

XX - SEVERABILITY

All clauses and/or provisions of these General Conditions that are deemed or become null or void shall not cause the nullity or voidance of the contract, but solely the clause and/or provision concerned.

XXI - DISPUTES

THIS CONTRACT SHALL BE GOVERNED BY AND INTERPRETED IN

THIS CONTRACT SHALL BE GOVERNED BY AND INTERPRETED IN ACCORDANCE WITH THE LAWS OF FRANCE. ANY DISPUTE IN RELATION TO THE INTERPRETATION OR THE EXECUTION OF THIS CONTRACT NOT AMICABLY SETTLED BETWEEN THE PARTIES WITHIN A 30 DAY PERIOD, SHALL BE SETTLED BY THE COMPETENT COURT OF ANGOULÉME (FRANCE), EVEN IN THE CASE OF INTRODUCTION OF THIRD PARTIES OR THE ENVOLVEMENT OF SEVERAL DEFENDANTS. HOWEVER, THE SUPPLIER RESERVES THE EXCLUSIVE RIGHT TO BRING THE DISPUTE TO THE COMPETENT COURTS OF THE SELLER OR THE CLIENT.



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